



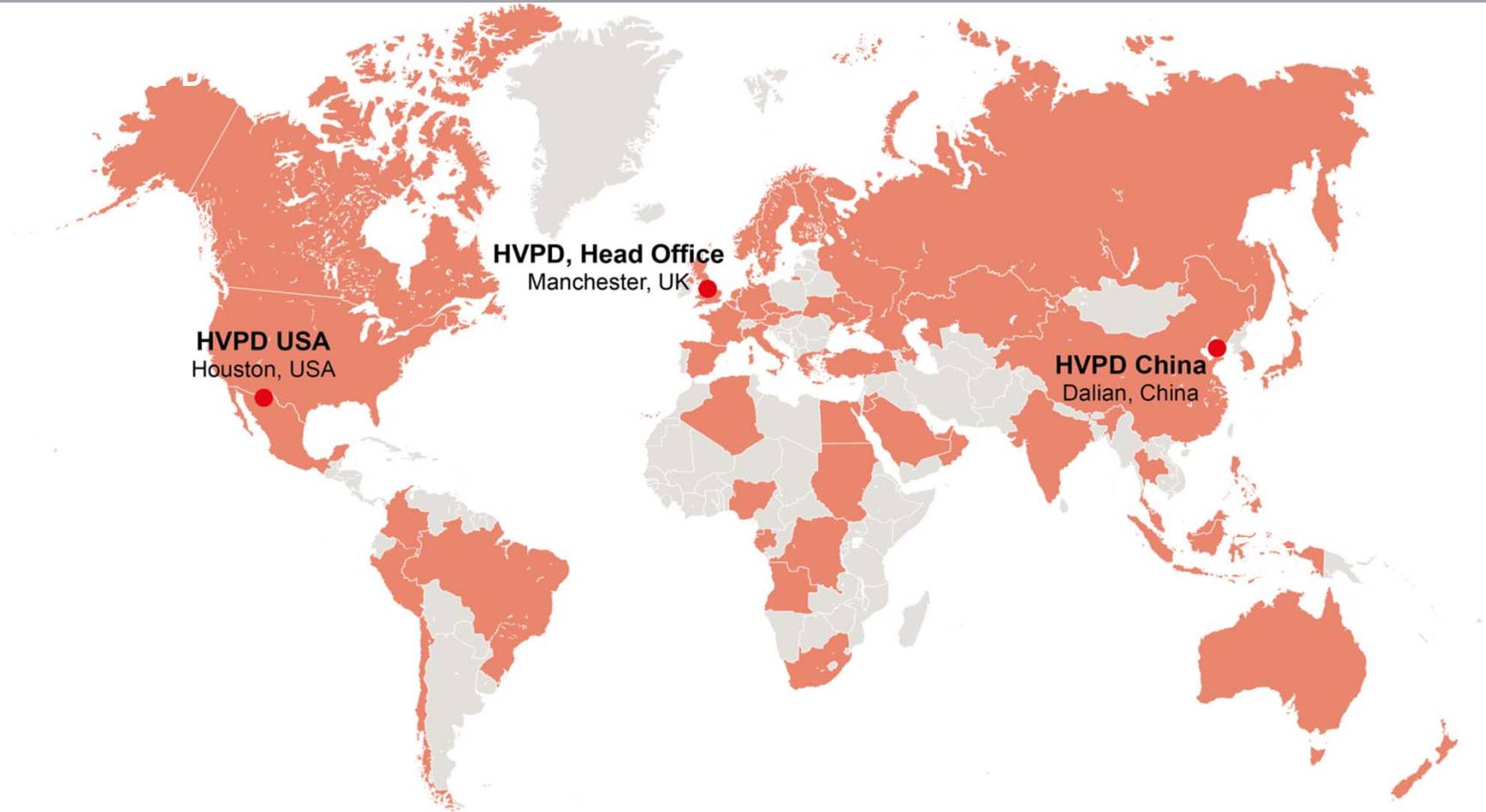
Introduction to PD

October 2014

Presented by:
Dr Lee Renforth,
Managing Director
HVPD Ltd

CONTENTS

- PD detection theory
- PD test & monitoring equipment
- Cable PD – detection & location
- Local PD in switchgear
- PD in rotating machines
- Continuous PD monitoring



- HVPD are experts in the growing industry of **on-line partial discharge (OLPD) condition monitoring** and condition based management (CBM) of high voltage networks.
- We supply portable and permanent OLPD surveying, diagnostic test and continuous monitoring solutions, and a complimentary range of on-site services, monitoring services and training.
- Over 350 customers in 100 countries trust our technology.

**500+ test and monitoring
projects completed over
the past 20 years**

OUR EXPERTISE

“Our Knowledge is Your Power”



Oil & Gas



Offshore Renewables



Transmission & Distribution



Power Generation



Shipping



What is partial discharge?

“A **localised** electrical discharge that only partially bridges the insulation between conductors and which can or can not occur adjacent to a conductor”

IEC60270 Definition



Why test for partial discharge?

PD activity is an indication of an **incipient fault** in HV insulation and is widely regarded as the best ‘**early warning**’ indicator of the deterioration of high voltage insulation.



**Power cables,
joints/splices and
terminations**



**Switchgear
(Air, Solid, Gas-insulated)**



**Power transformers
and bushings**

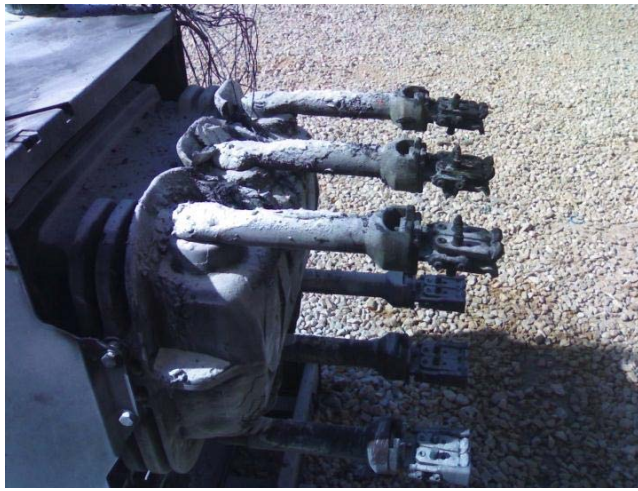


Motors and generators



CT's and VT's

- Safety – mostly with switchgear, outdoor HV plant and cable sealing ends
- Ageing population problem – life extension, delaying capital replacement
- Condition-Based Maintenance (CBM)
- Avoid unplanned outages and improve network reliability



At Manufacture

- Quality Assurance
- Type/routine tests, e.g. IEEE/IEC standards – test to less than 5 pC on the cables



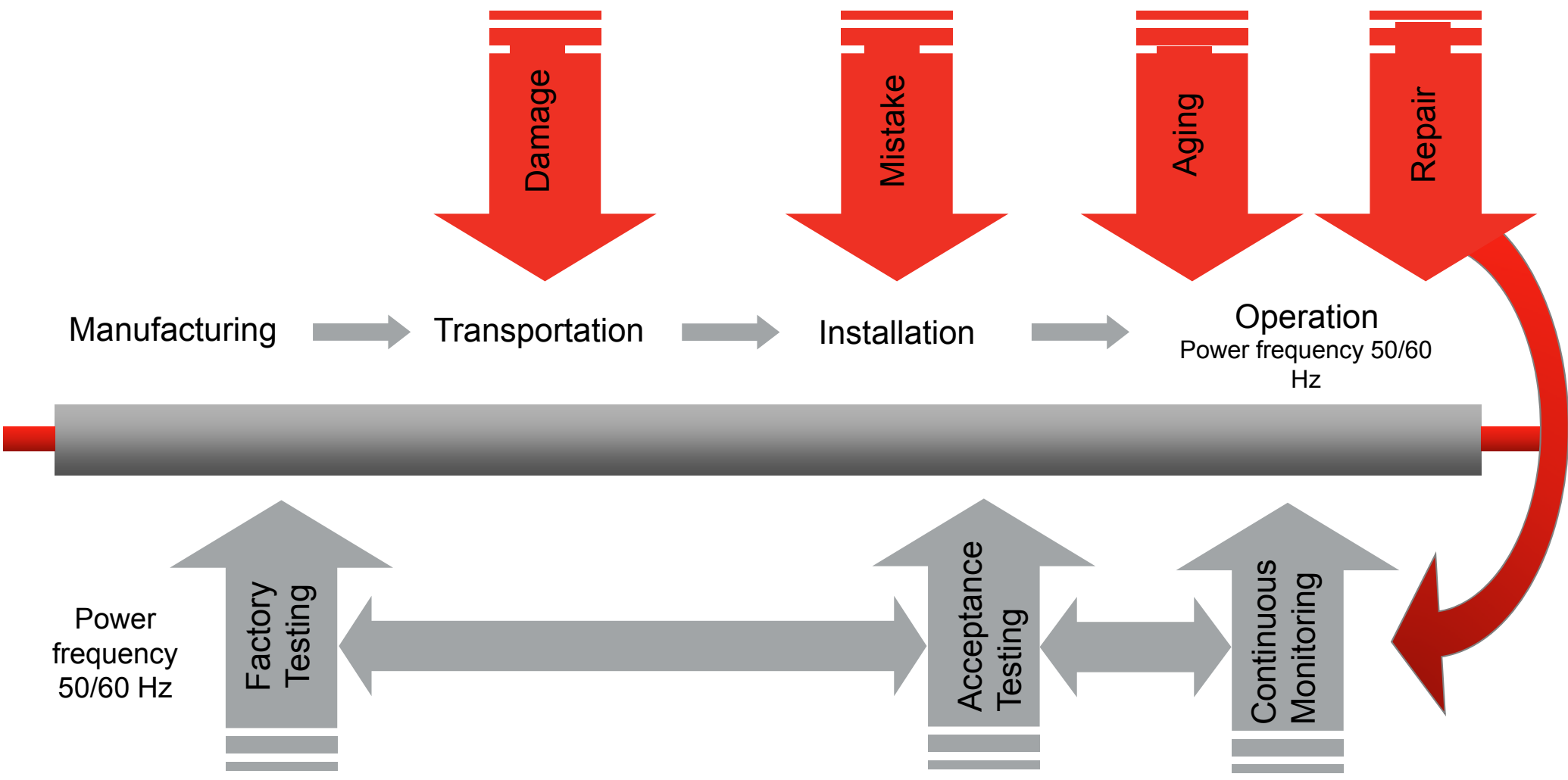
At Commissioning

- To check for transport damage
- To ensure the installation of the cable accessories have made to a good standard (these are the weak points in the cable system)

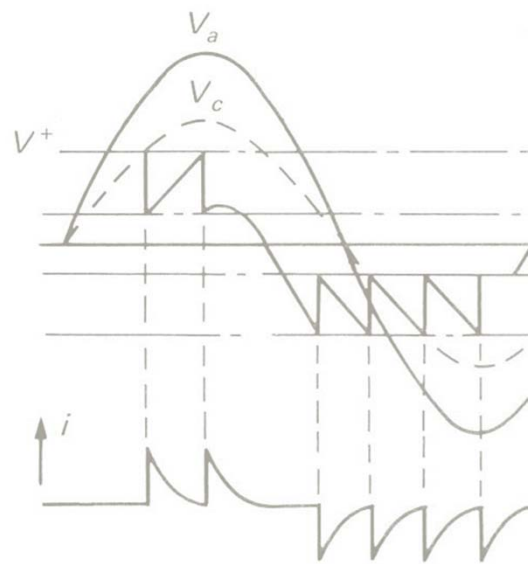




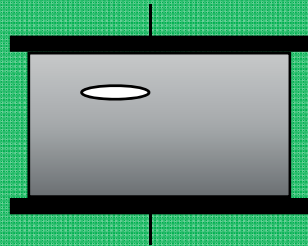
- To get baseline PD readings
- To evaluate insulation quality
- To locate PD activity sites and target repair
- To avoid costly / unplanned outages
- To support Condition-Based Management (CBM) regime



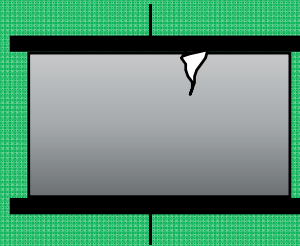
OLPD DETECTION THEORY



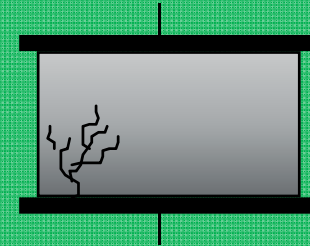
Internal



Void in insulation

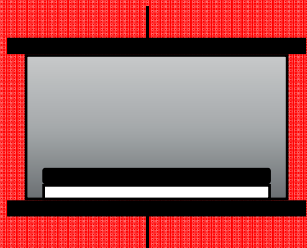


Sharp, irregular surface on conductor

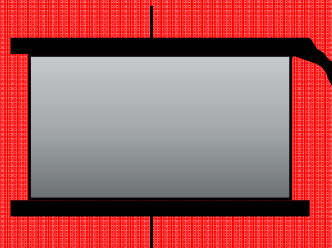


Tree growth in insulation

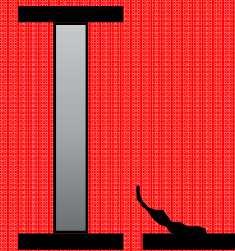
External



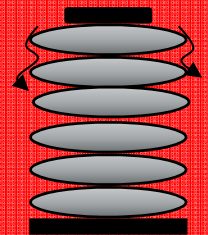
'Floating' metalwork near conductors



Corona from sharp objects at high voltage



Discharges from induced voltages onto sharp points at ground

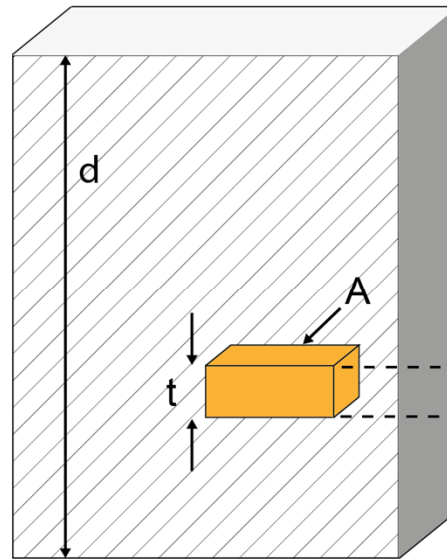


Surface discharges

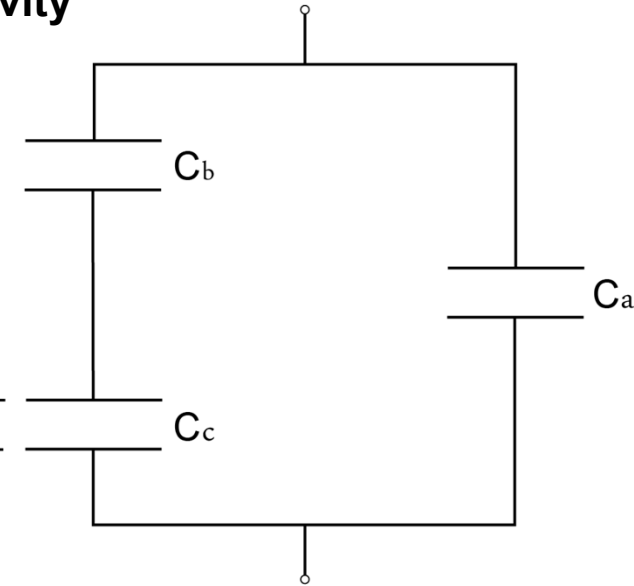
C_a = Bulk insulation capacitance

C_b = Capacitance between discharging area and electrodes

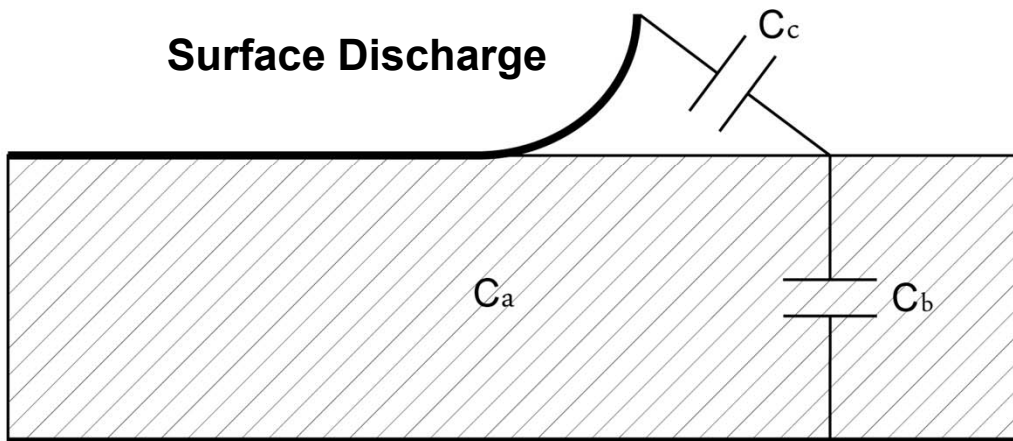
C_c = Cavity/surface area in which the PD occurs



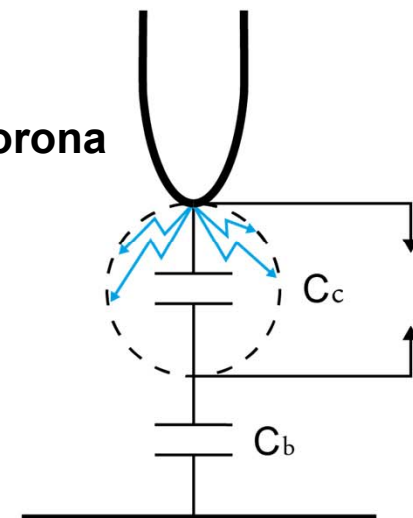
Void/cavity

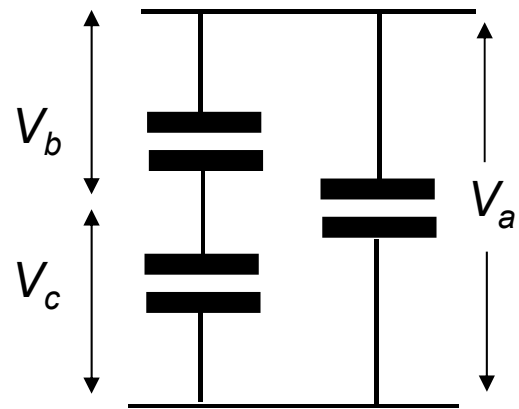


Surface Discharge

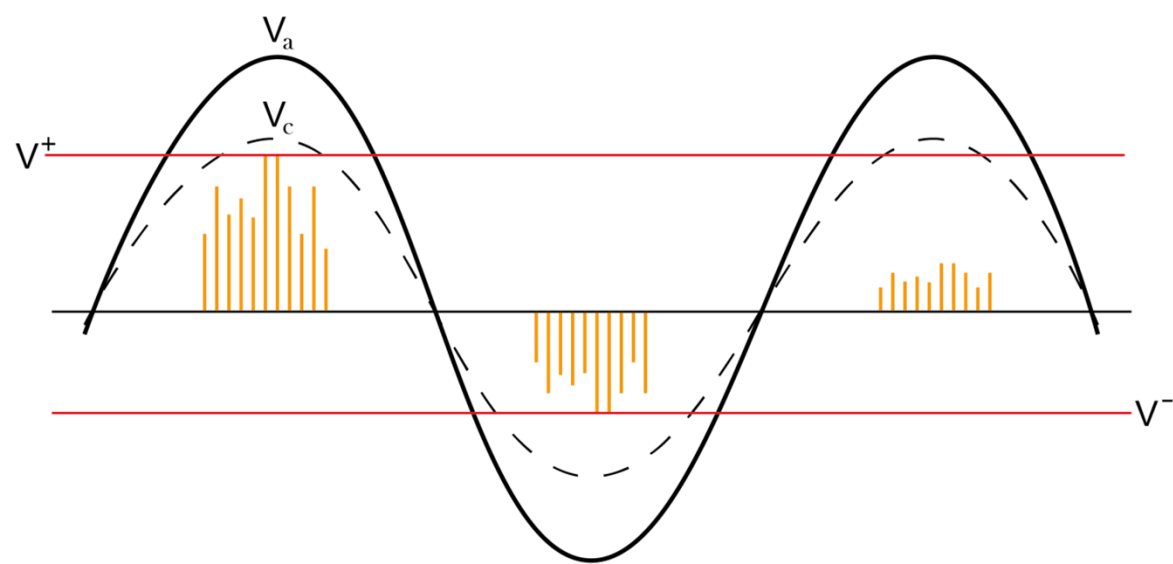


Corona





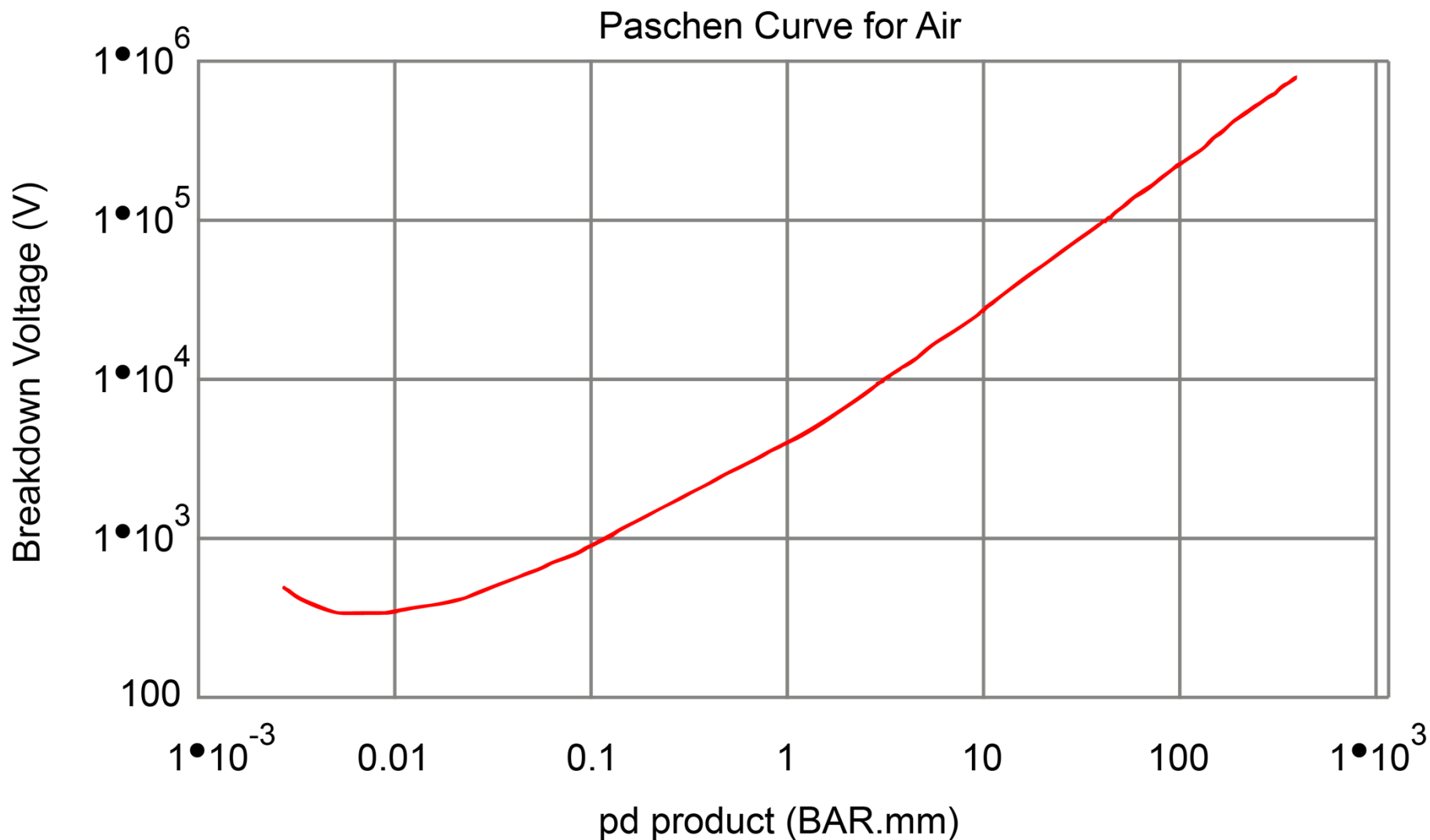
Theoretical



Actual current pulses
(stochastically occurring)



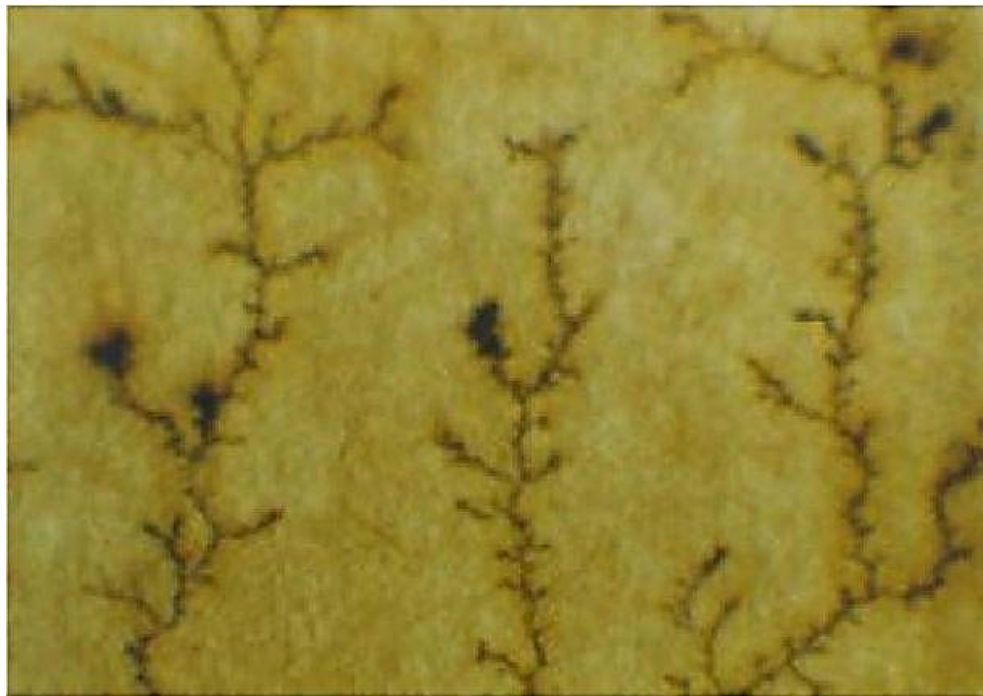
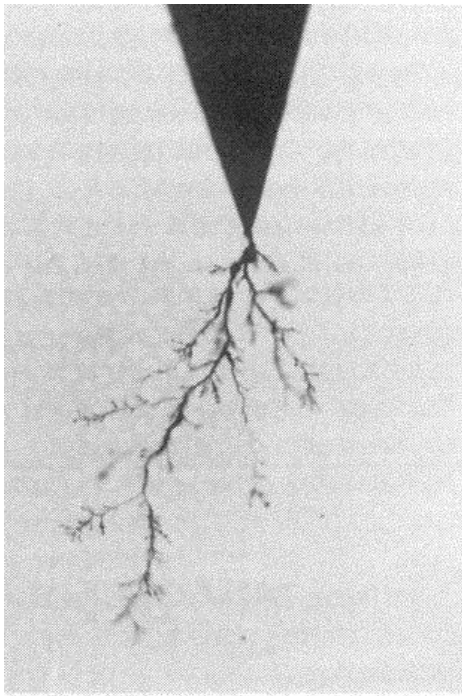
$V^+, V^- =$ PD inception voltages



From T.W. Dakin et al "Breakdown of gases in uniform fields" *Electra*, Vol 32, pp 61-82, 1974.

Internal discharges can be caused by:

- Voids, cavities, delaminations in solid or liquid insulation
- Electrical trees form from these voids







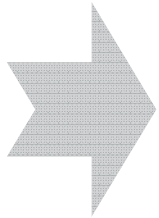
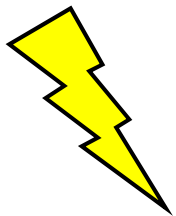






- Incepted from sharp points on HV conductors
- Also possible from sharp points on ground

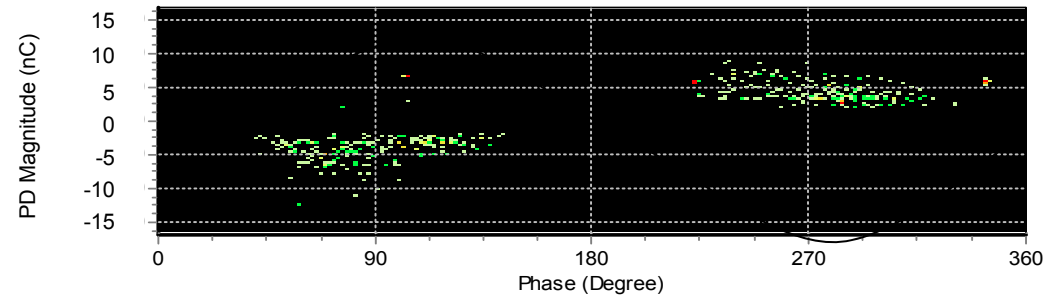


ENERGIES RELEASED**DETECTION METHODS****PD**

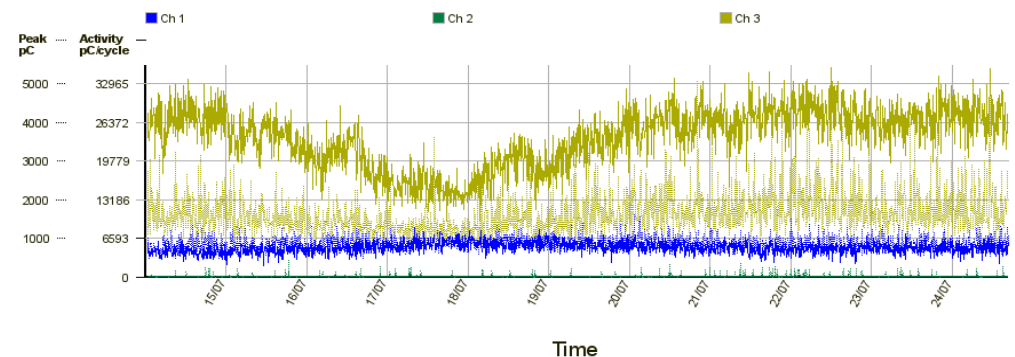
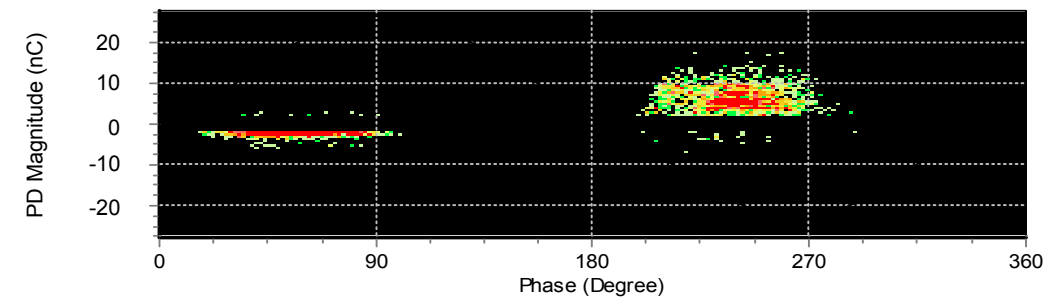
Electrical Charge	→	Capacitor/Inductive (HFCT)
Electromagnetic Wave	→	TEV, VHF/UHF Couplers
Optical	→	Low-light/UV Cameras
Acoustic Wave	→	Contact/Airborne Acoustic
Gaseous by-products	→	Dissolved Gas Analysis
Chemical by-products (such as white deposit oxides)	→	Visual inspection
Ozone	→	Smell / Ozone Detector

- PD magnitude
- PD count (number of PD pulses per power cycle)
- Cumulative PD activity
- Phase Resolved PD (PRPD) Patterns
- PD monitoring over time

Internal PD in bushing



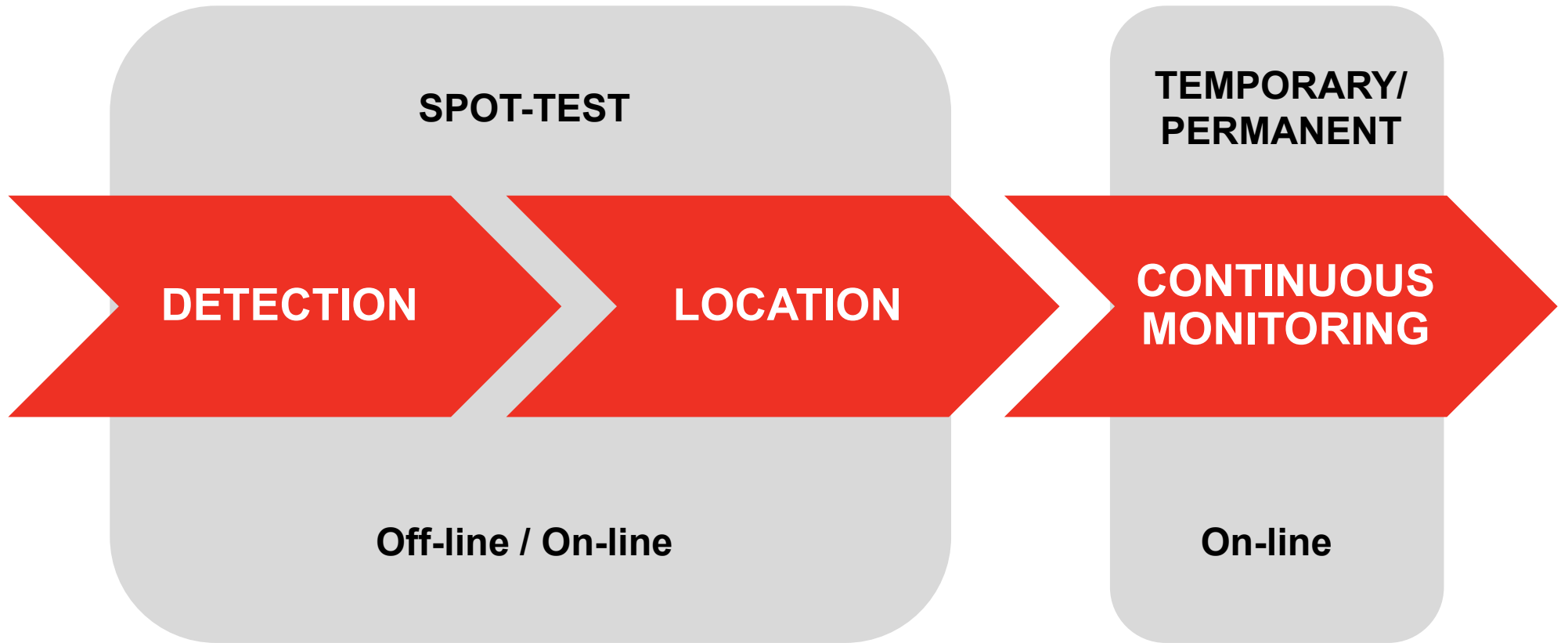
Surface discharge in termination





OLPD TEST & MONITORING EQUIPMENT





Phase 1 – Detection

- Simple equipment
- Initial indication of PD level/severity



**HVPD PDSAir™
Handheld PD Surveying Tool**

Phase 2 – Diagnostics/Location

- More advanced hardware/noise rejection
- PD diagnosis and location within the cable/plant
- Digital PD detector with PC for analysis and reporting



**HVPD Longshot™
Diagnostic OLPD Test Unit**

Phase 3 & 4 – Temporary/Permanent Monitoring

- Temporary or permanent hardware
- Trends PD over time and captures any trend to failure
- Web-based UI/SCADA alarms
- Simple and advanced options:
 - Simple hardware without diagnostic capabilities, generates alarm signals only
 - Advanced hardware with diagnostic capabilities



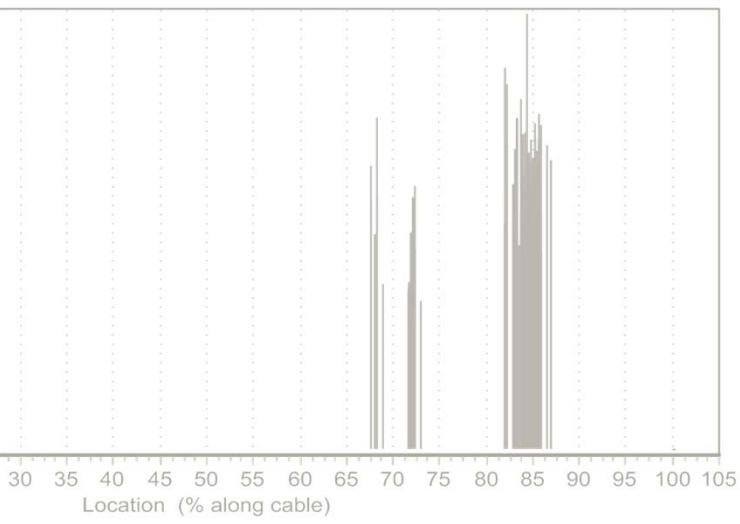
**HVPD Multi™
Portable Monitor**



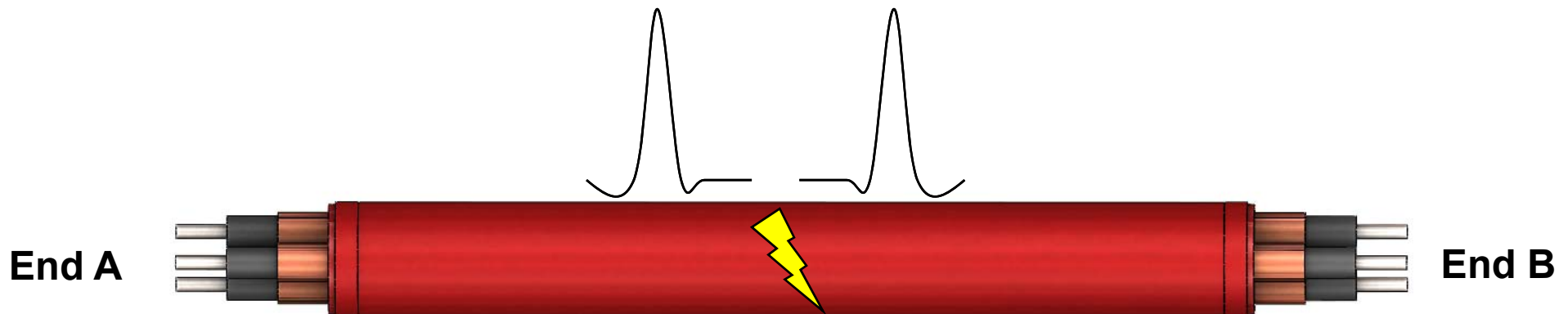
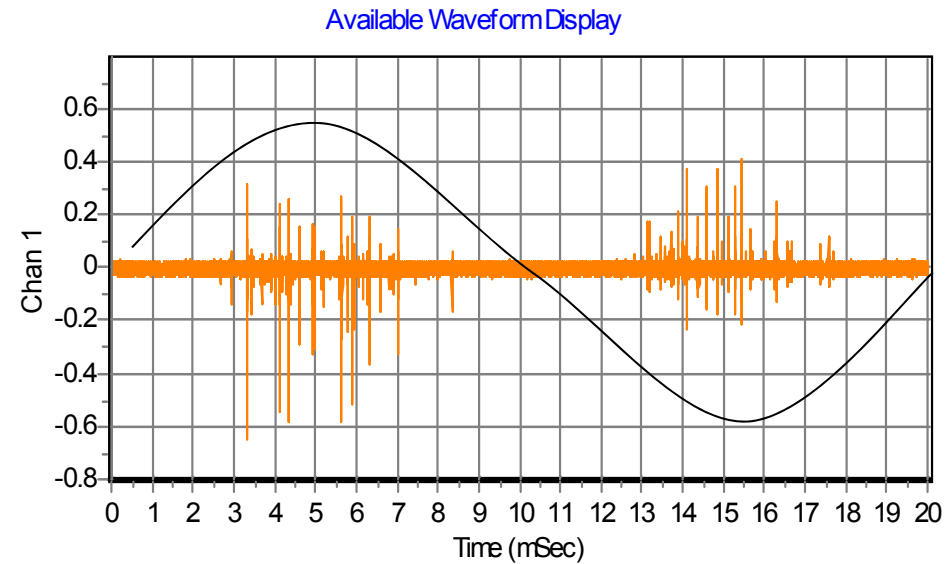
**HVPD Multi™
Permanent Monitor**



CABLE PD – DETECTION & LOCATION

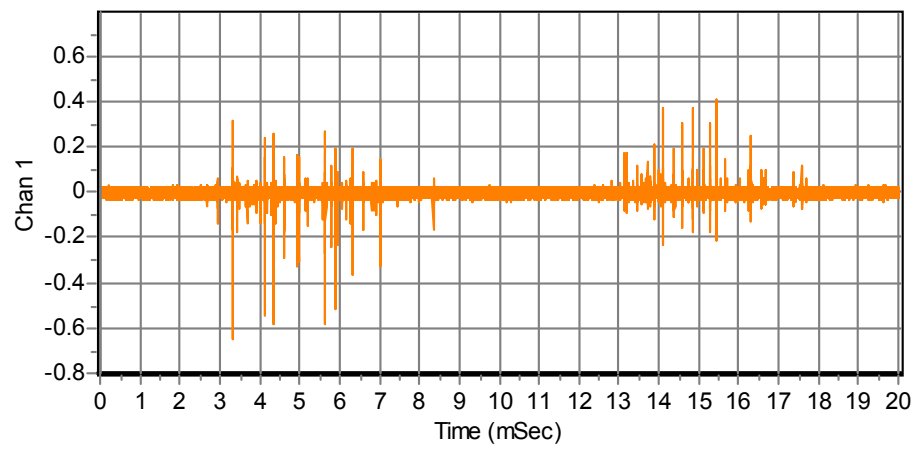


- PDs are incepted by the high voltage applied to cable.
- PD pulses are short duration impulses (ns – μ s) that propagate in both directions away from PD site between cable core and sheath.
- Signals can be detected on both the core and earth screen at terminations.



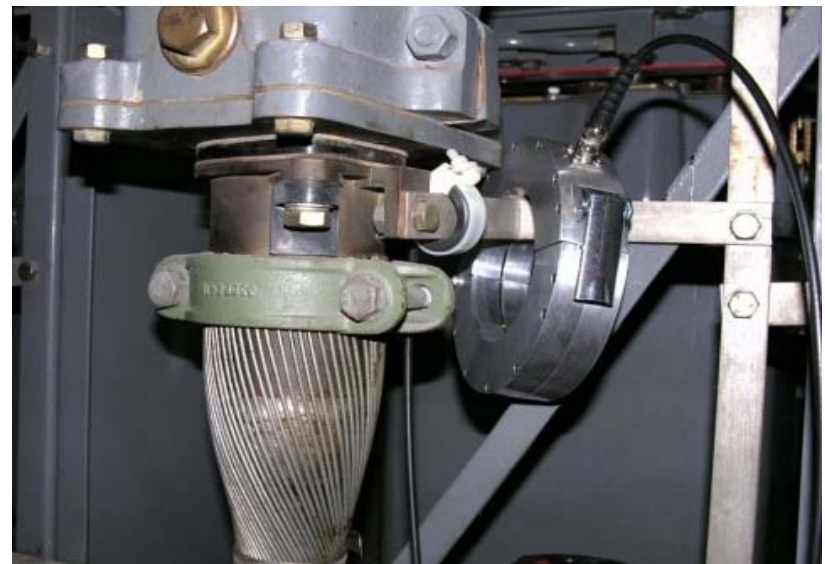
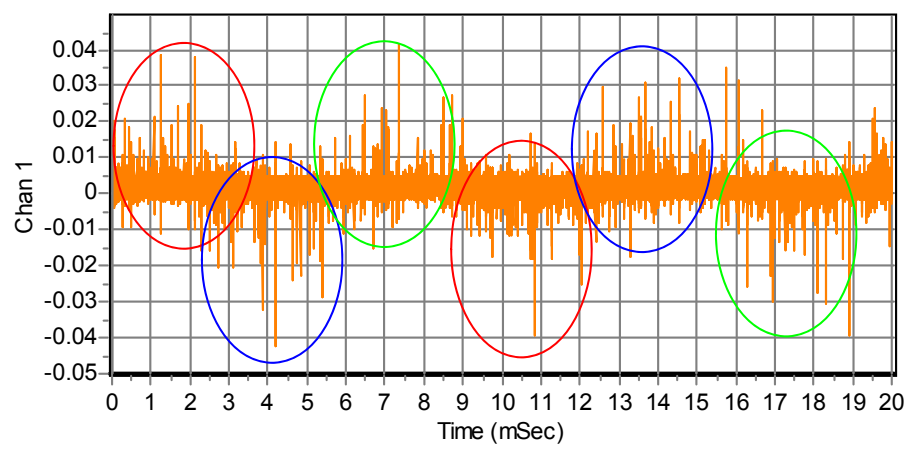
Single Core Cable

Available Waveform Display

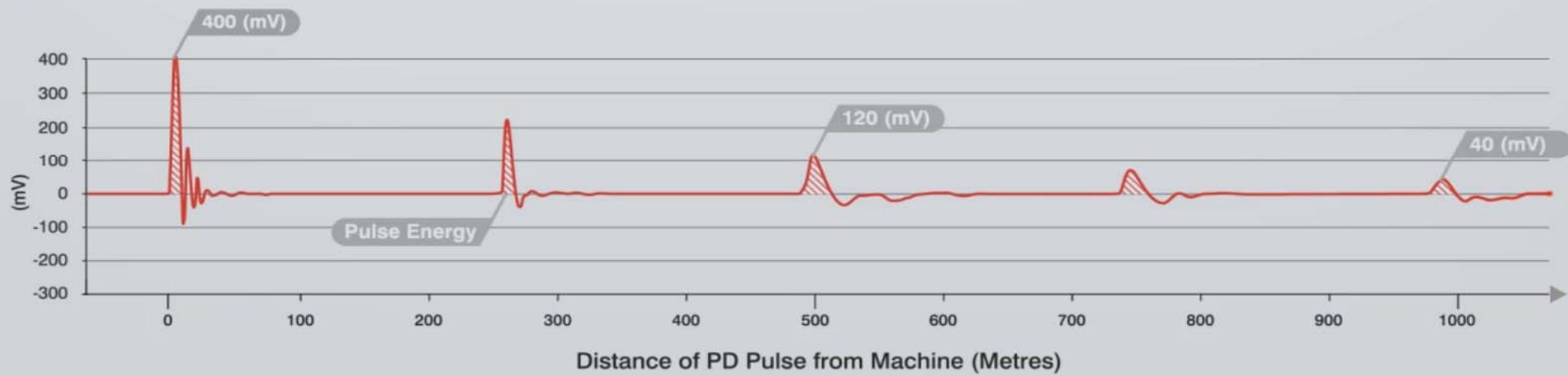


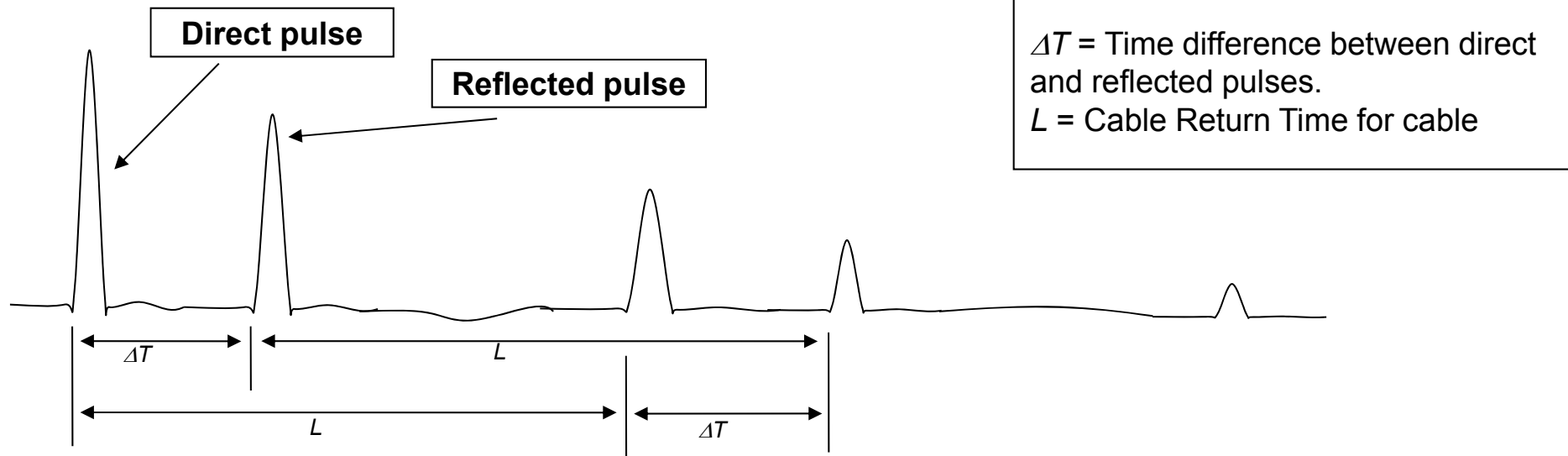
Three Core Belted Cable with HFCT on Common Screen

Available Waveform Display



PD Pulse Propagation Analysis





PD Pulse Return Speed: $V_{PD} = \text{Cable Length} / \text{Return Time}$

PD Site Location:

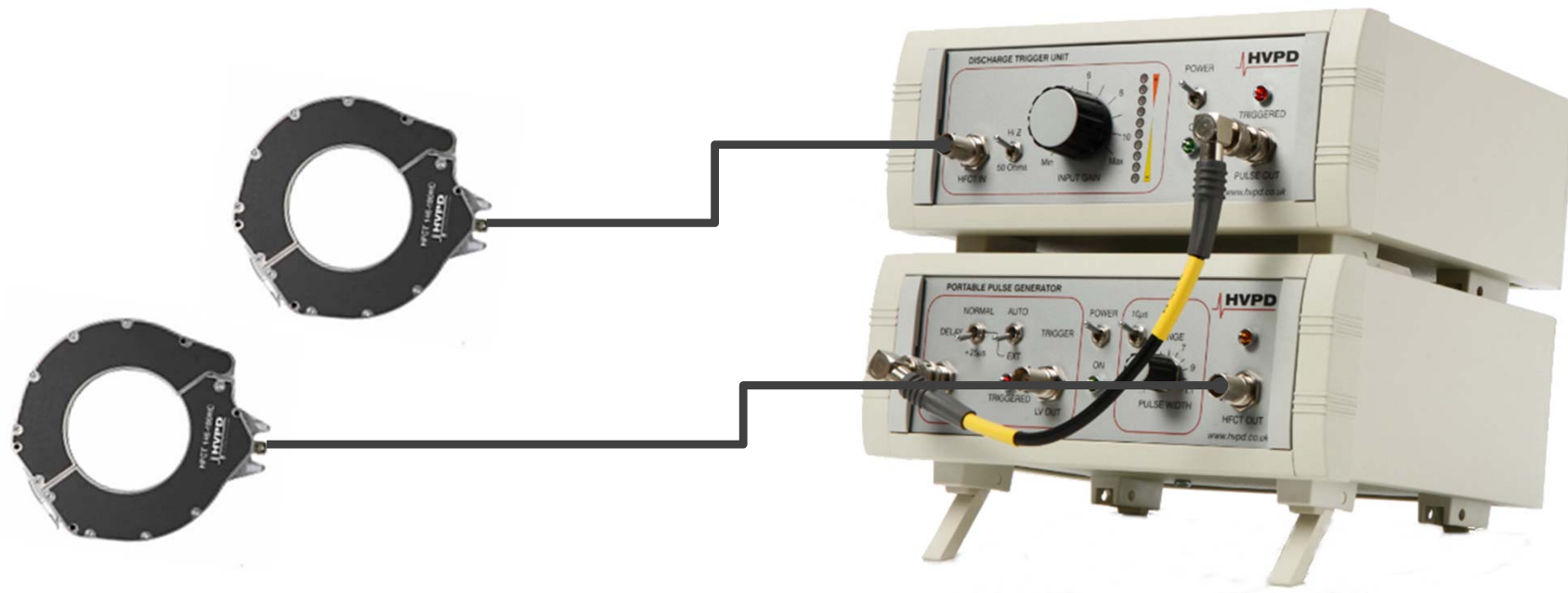
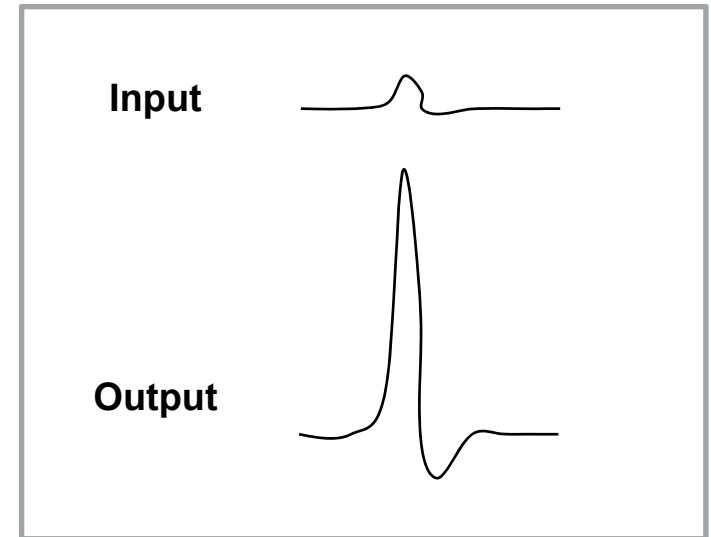
$$PD_{\%} = \left(1 - \left(\frac{\Delta T}{L} \right) \right) 100$$

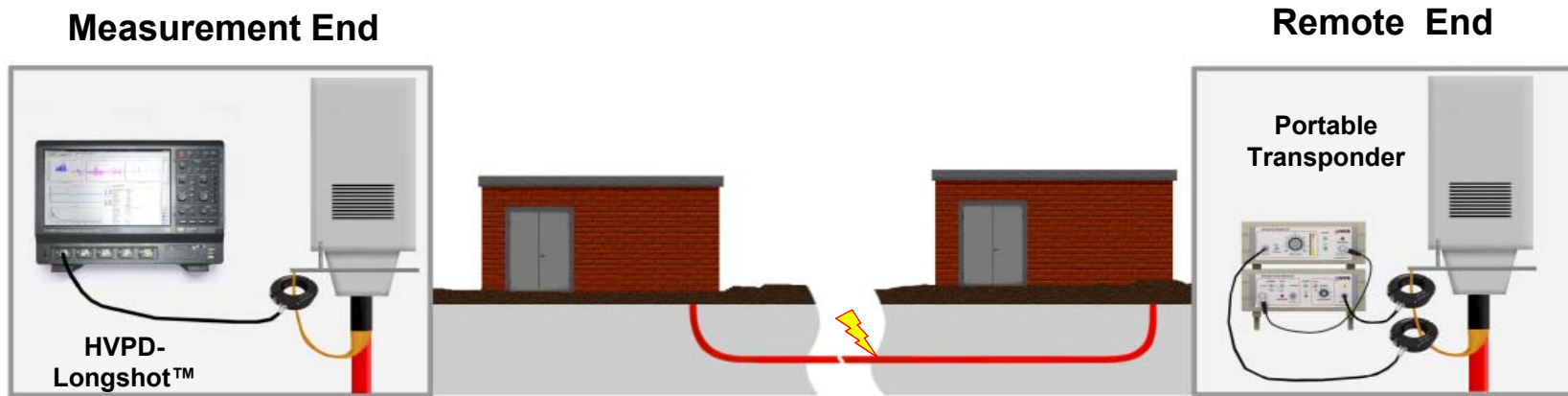
In many on-line cases reflected PD pulses are often not visible:

- Attenuation is too large to measure reflected pulses from the far end (long cables)
- Waveforms too difficult to interpret (noisy signals)
- Teed or jointed cables
- Cables with many ring main units or switches
- Cables with no change in impedance at the far end

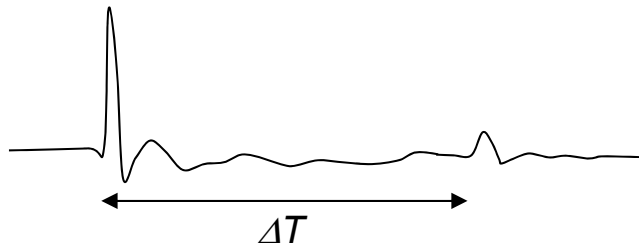


- Portable Transponder installed at remote cable end
- Compensates for lack of reflected pulse
- Detects PD pulse with Discharge Trigger Unit and re-injects large pulse back into cable with Pulse Generator
- Connects to cable with HFCTs



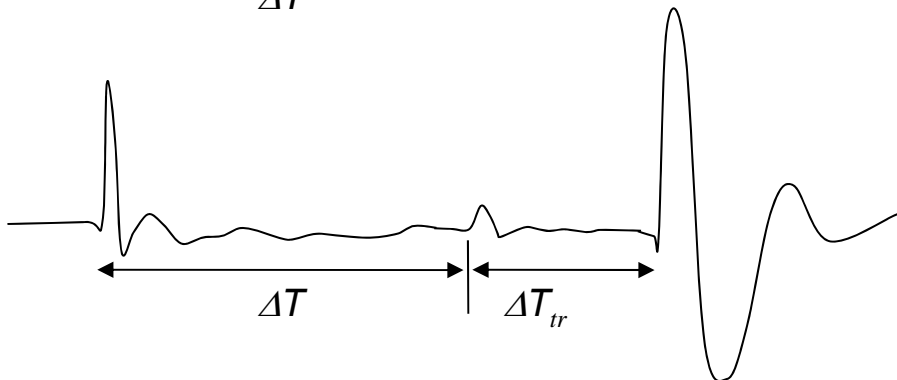


Without Transponder



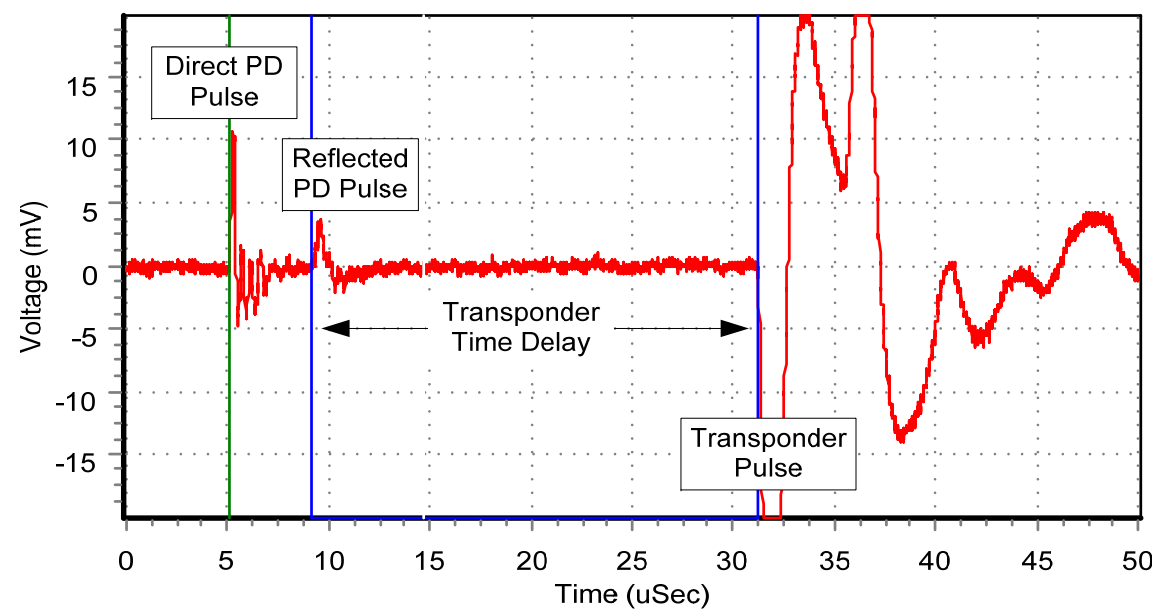
Reflection may not be clearly visible (e.g. due to noise)

With Transponder

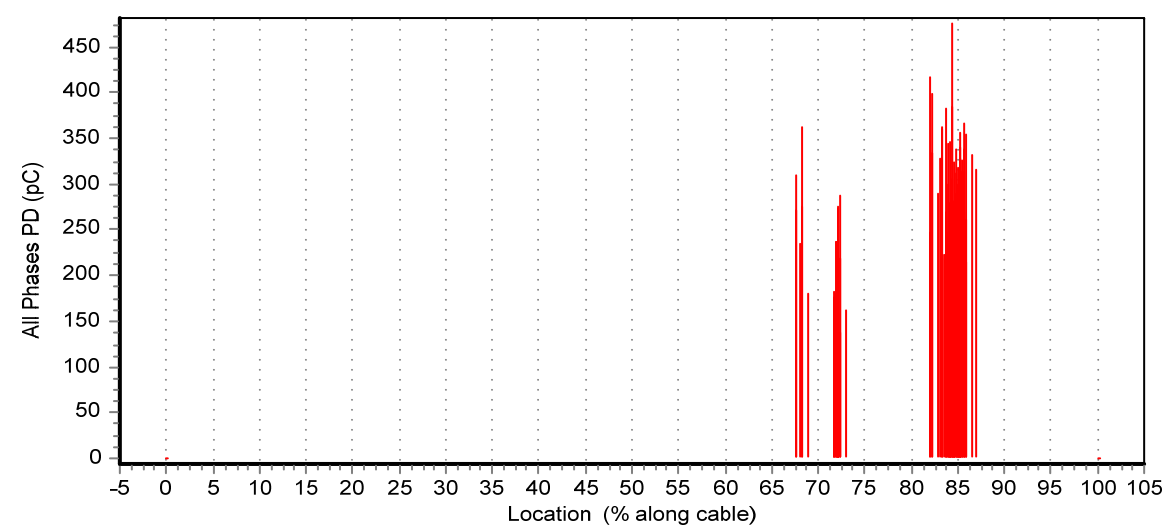


The large transponder pulse removes any confusion

ΔT = Time between direct and reflected PD pulses
 ΔT_{tr} = Transponder time delay



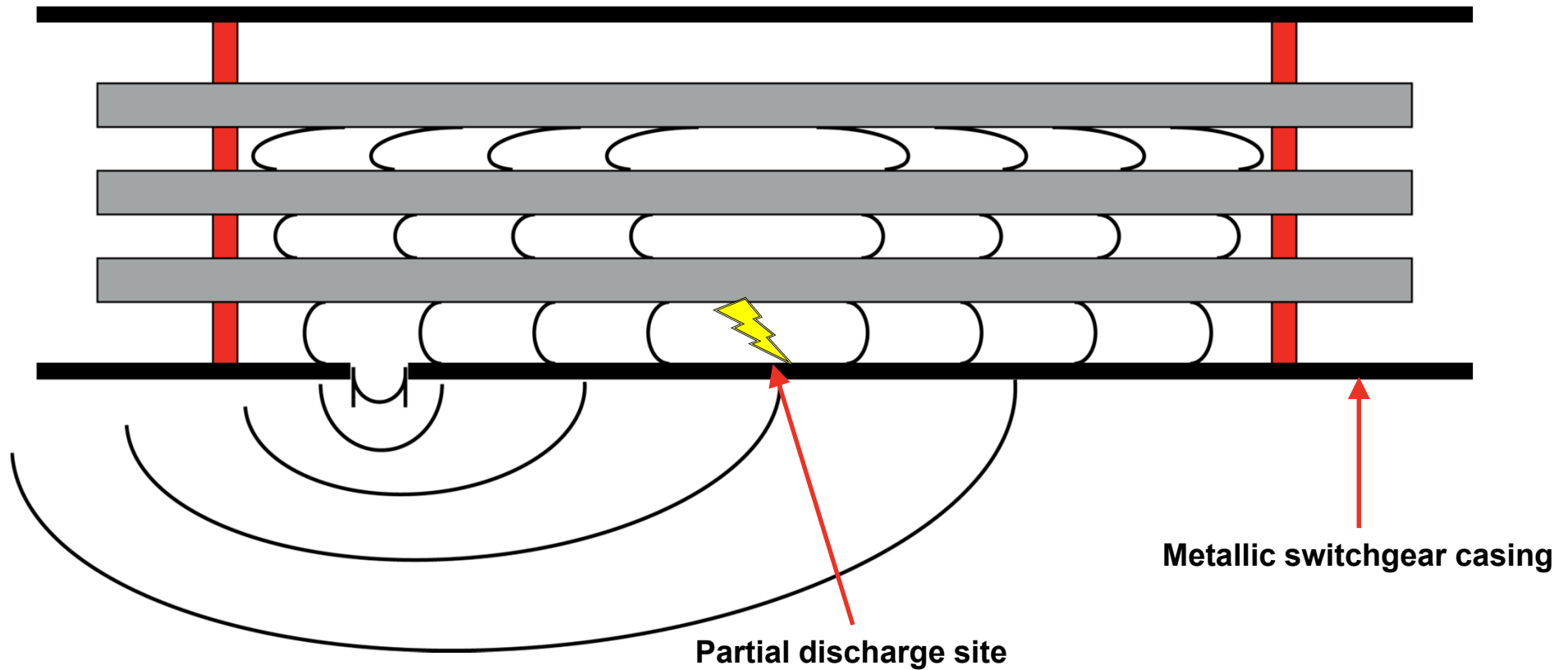
Reflectogram showing PD and transponder pulses



PD location map for all PD pulses in cable section under test

LOCAL PD IN MV SWITCHGEAR



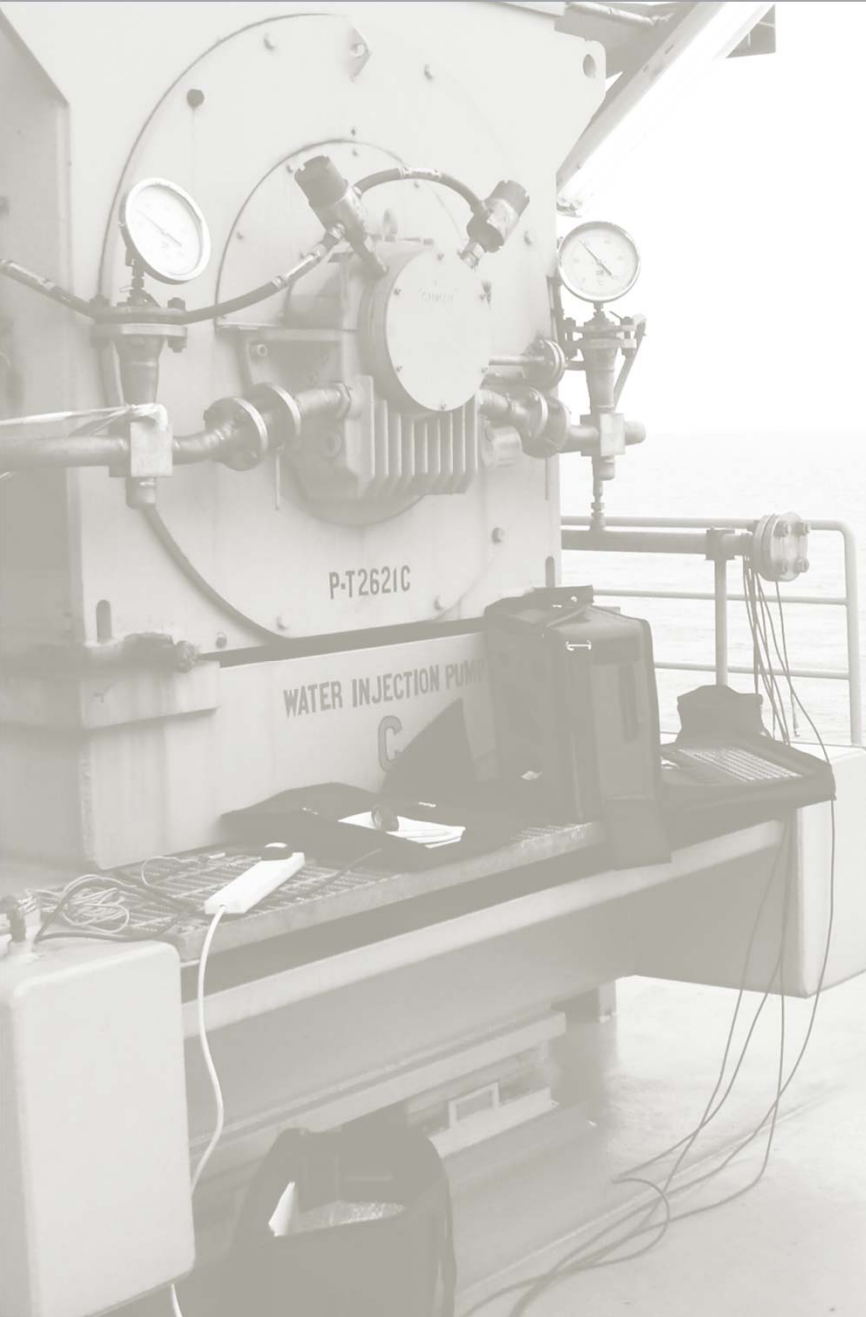


- PD site within switchgear: Phase–Earth discharge
- EM signals radiate from PD site and couple onto metal-clad housing
- Signals emerge on the outer surface at openings in metal housing



PD IN ROTATING MACHINES

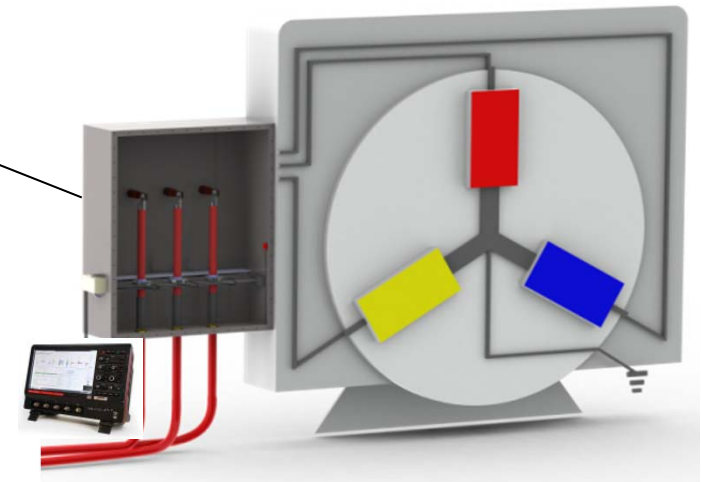




Important to identify type of PD in machine for severity:

- slot section,
- delamination,
- end windings etc.

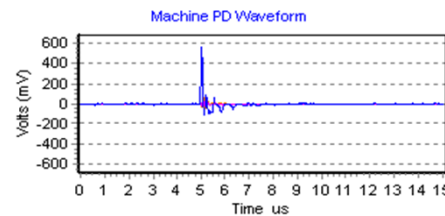
PD Sensors



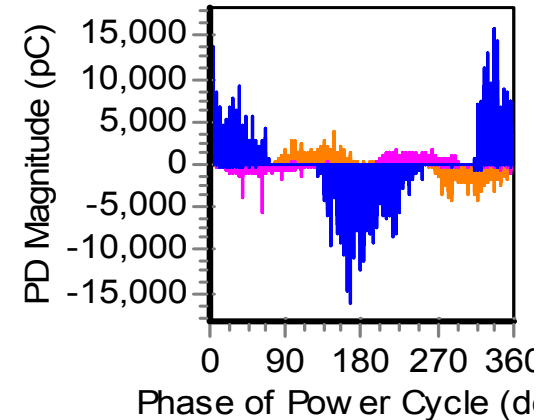
**HVPD Longshot™
Diagnostic Test Unit**

- Signals captured synchronously from sensors on each phase.
- Identification of Phase-Earth PD and Phase-Phase PD.
- Phase Resolved PD (PRPD) patterns indicate the defect type.

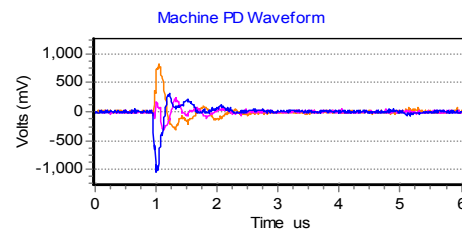
Phase-Earth PD on RYB phases



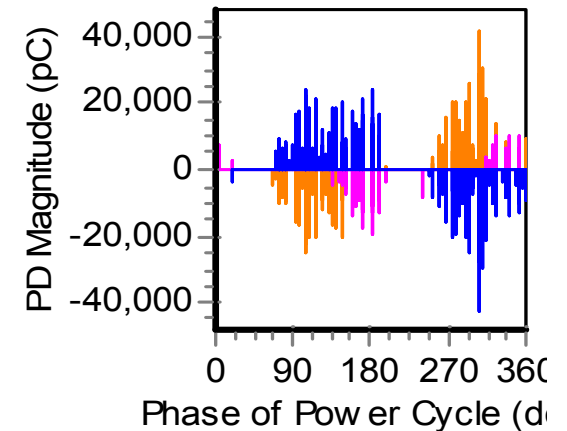
Machine PD



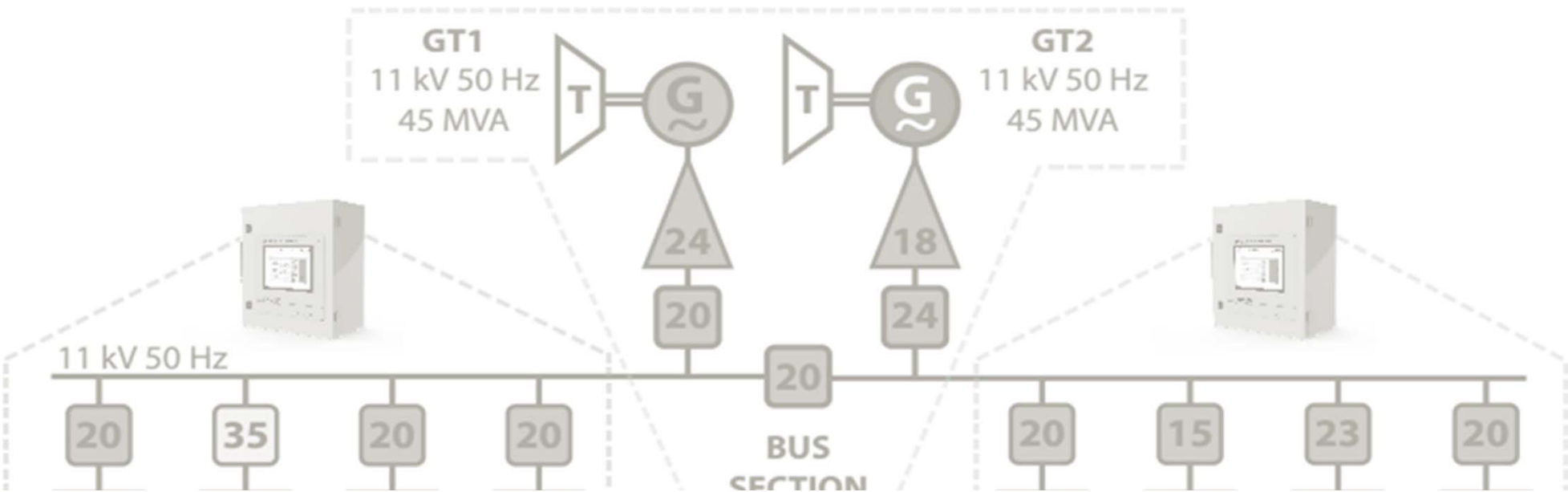
Phase-Phase PD (Y-B)



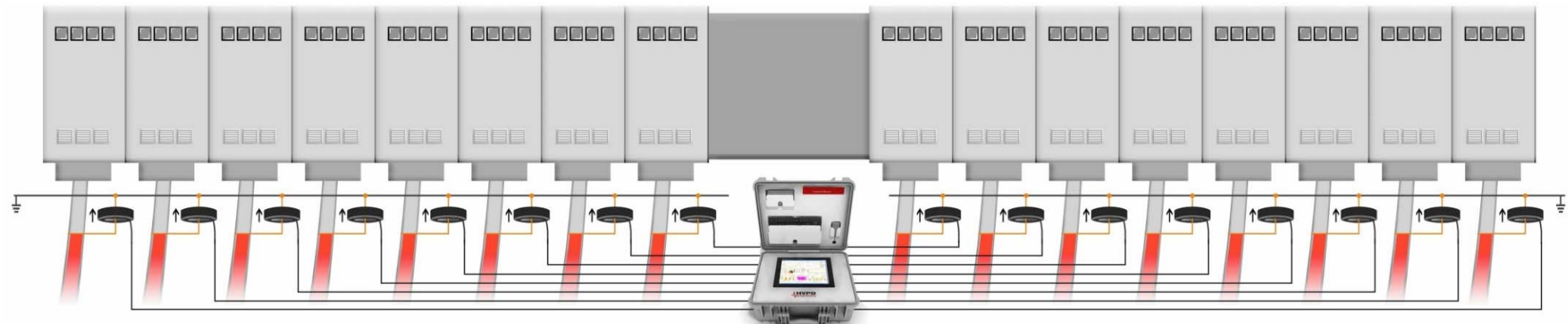
Machine PD

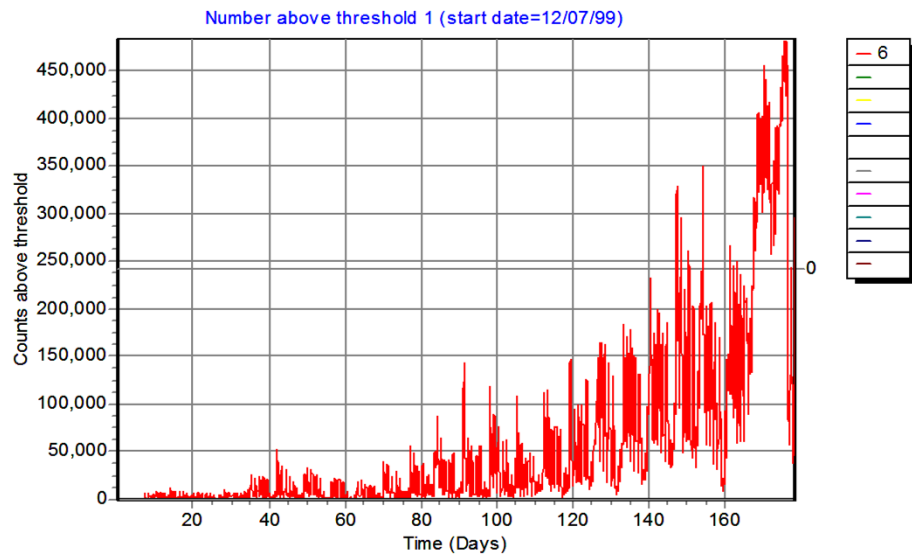


CONTINUOUS OLPD MONITORING

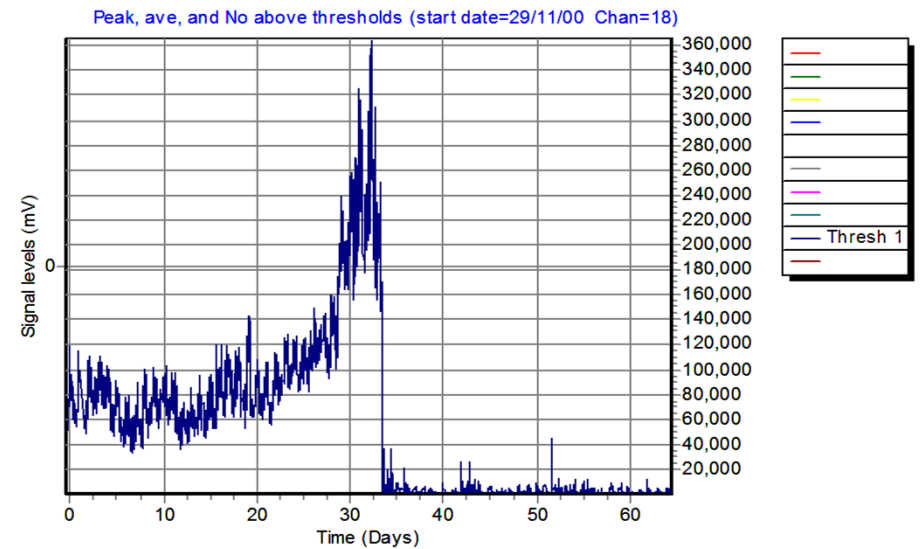


- Important/high-value/critical plant items
- Plant with known PD variations in time – paper cables, rotating machines, AIS/GIS.
- Plant with high PD identified in spot-tests

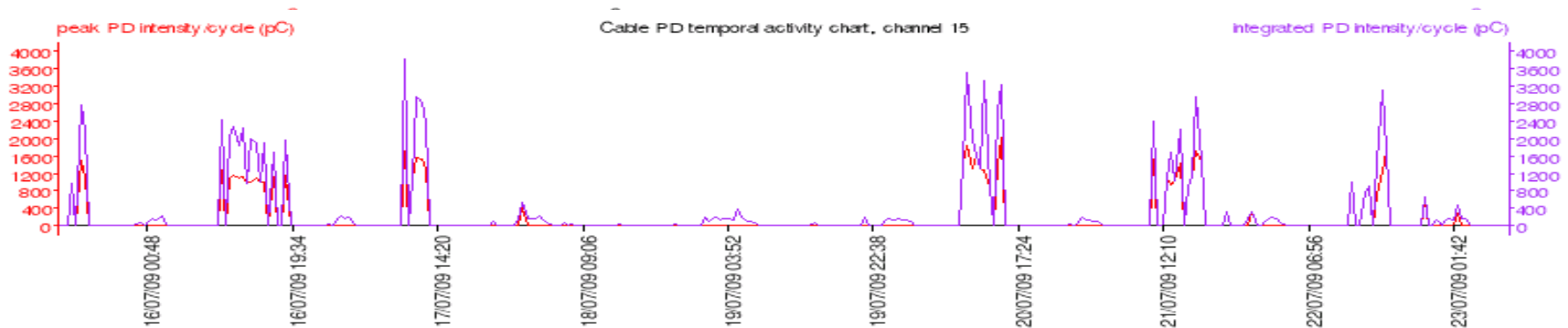
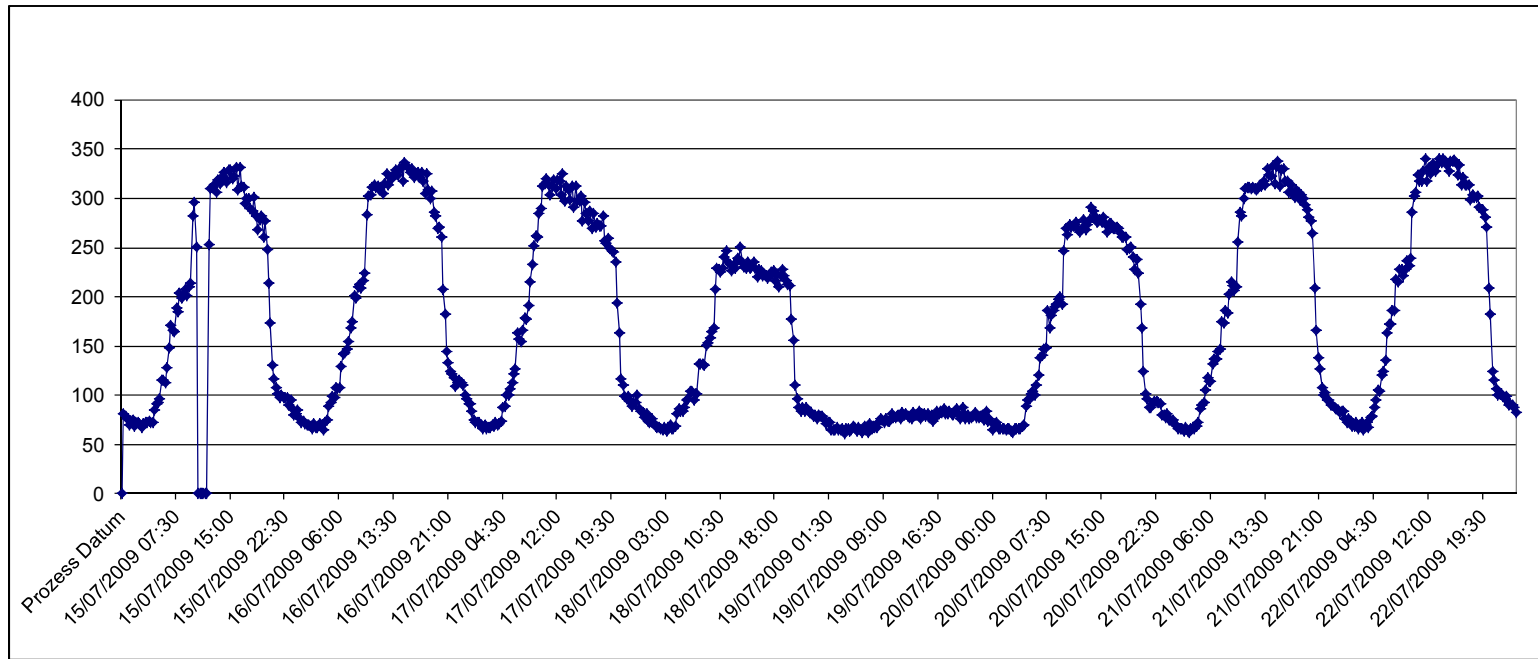




PD rise to failure over 100 days

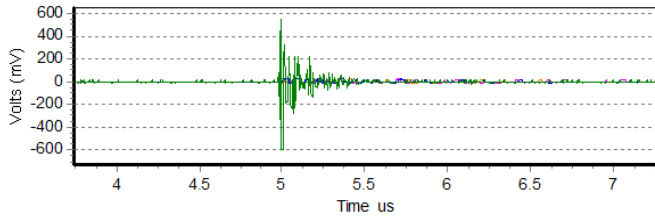


PD rise to failure over 20 days

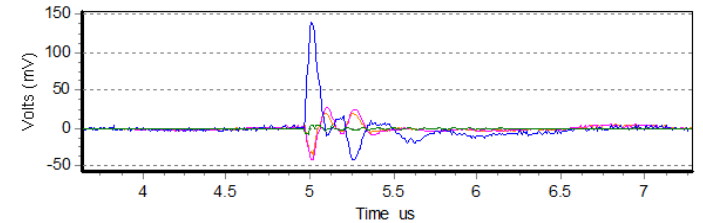


PD burns in a hot cable: electrodes expand - possible movements inside accessories lead to increased field strengths in dielectrics – PD in accessories.

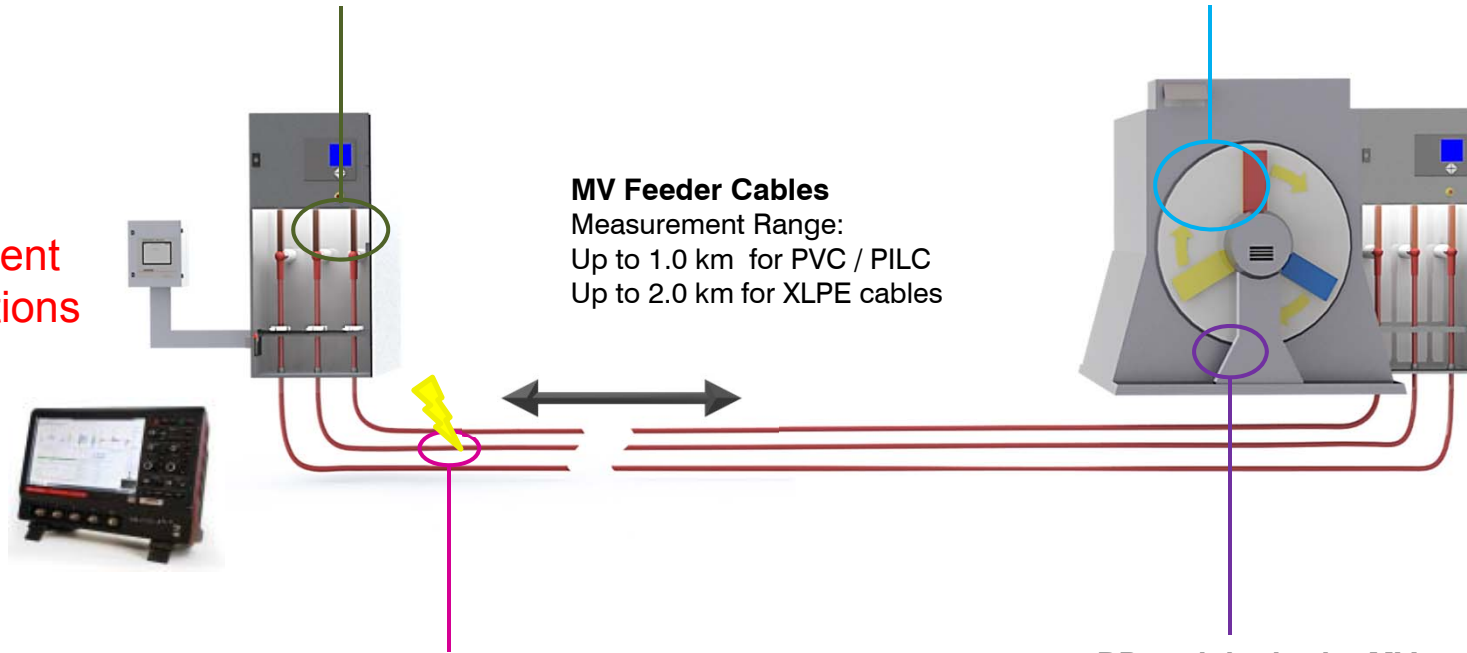
PD activity within the MV switchgear



PD activity within the MV motor stator slot section



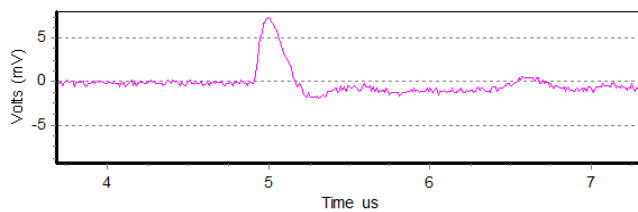
Safe Environment
(no restrictions apply)



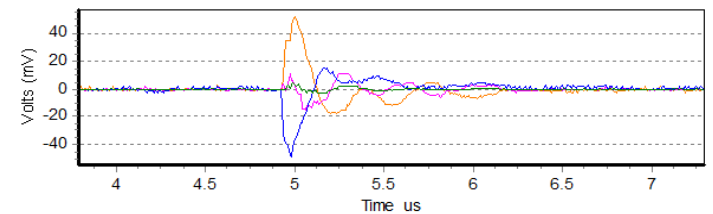
MV Feeder Cables
Measurement Range:
Up to 1.0 km for PVC / PILC
Up to 2.0 km for XLPE cables

Ex Environment
(restrictions apply)

PD activity within the MV feeder cable



PD activity in the MV motor stator end windings



HVPD TCO Monitoring Database

Analysis / Reports Substations / Network Selection

Local Area Network Criticality League Table

Networks	Criticality (0-100)	
	Cable	Local
Grid Connection 400 kV	0	0
Offshore 132 kV Export	0	0
Trans Network 110 kV	47	26
Industrial Network 110 kV	0	0

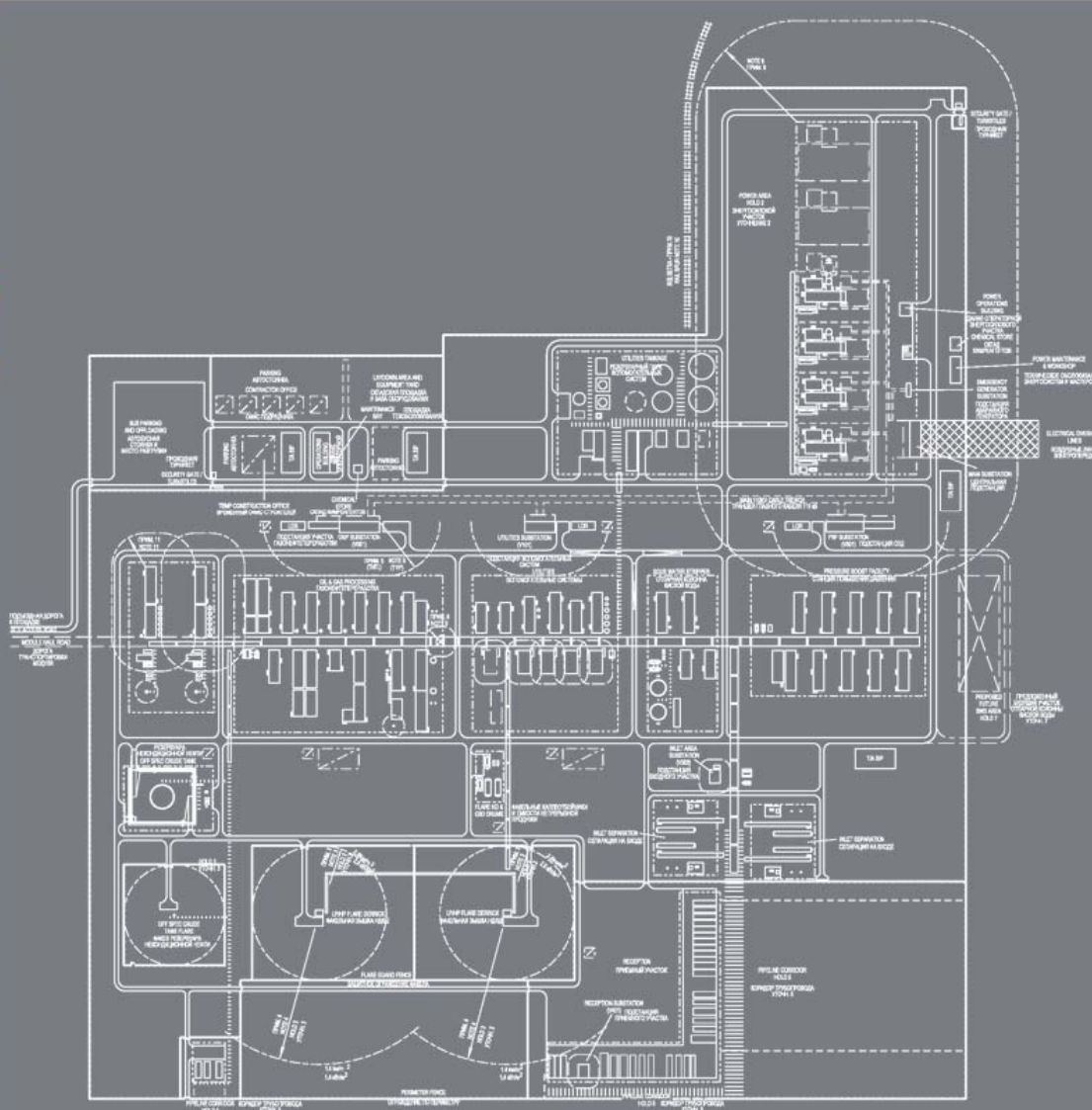
Condition/Action Guideline	Criticality (0-100)
High PD / Diagnostic	76-100
Moderate to High PD / Investigate	51-75
Moderate PD / Monitor	26-50
Plant OK / No Action	0-25

Key

- Cable / Machine PD Activity
- Local PD Activity

Monitoring Period

- Last Hour Last 24 Hours
- Last Week Last Month



Network Options

View Level

- GEO : TCO Overview
- SLD : TCO Overview
- Substation : select
- Location : select

Networks

- Grid Connection 400 kV
- Offshore 132 kV Export
- Trans. Network 110 kV
- Industrial Network 110 kV

Sensor Configuration

Monitor Configuration

PD Measurements

Analysis / Reports Location : Gen 52-GP-9401.1

Local Area Network Criticality League Table

Channels	Criticality (1-100)	
	Cable	Local
Gen 52-GP-9401.1 L1	16	24
Gen 52-GP-9401.1 L2	25	25
Gen 52-GP-9401.1 L3	47	24
Gen Circuit Breaker L1	21	24
Gen Circuit Breaker L2	16	24
Gen Circuit Breaker L3	25	25
Transformer 15 kV Input L1	47	24
Transformer 15 kV Input L2	21	24
Transformer 15 kV Input L3	25	26
110 kV GIS Bus L1	0	0
110 kV GIS Bus L2	28	26
110 kV GIS Bus L3	16	24

Condition/Action Guideline	Criticality (0-100)
High PD / Diagnostic	76-100
Moderate to High PD / Investigate	51-75
Moderate PD / Monitor	26-50
Plant OK / No Action	0-25

Key
● Cable / Machine PD Activity
■ Local PD Activity

Monitoring Period
 Last Hour Last 24 Hours
 Last Week Last Month

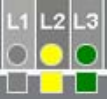
Generator
52-GP-9401.1



Generator
Circuit
Breaker



Transformer
52-TFR-9401.1
15 kV / 115 kV
157 MVA



110 kV GIS Bus
52-HDB-3301

Transformer 15 kV Input L3

Cable	25
Local	26

Network Options

View Level	
	GEO : TCO Overview
	SLD : TCO Overview
	Substation : TGTS4
	Gen 52-GP-9401.1
TGTS4 Locations	
	Gen 52-GP-9401.1
	Gen 52-GP-9401.2
	Gen 52-GP-9401.3
	Gen 52-GP-9401.4

Sensor Configuration
Monitor Configuration
PD Measurements

Analysis / Reports ▾

Local Area Network Criticality League Table		
Substations	Criticality (0-100)	
	Cable	Local
THRUSTER 1 HV PANEL	96	99
EARTHING Tx & RESISTOR	77	06
GENERATOR 1	13	74
HV Tx 1 (FWD)	16	70
HV SWBD 3 BUS TIE PANEL	13	65
TOPSIDE HV Tx 1 (HPU & LV)	09	39
GENERATOR 2	18	38
TOPSIDE HV Tx 1 (VFD)	36	44
HV SWBD 2 FEEDER	09	26
EM'CY HV SWBD INCOMER 1	25	21
THRUSTER 4 T/R	20	12

Condition / Action Guideline		Criticality (0-100)
High PD / Diagnostic		76-100
Moderate to High PD / Investigate		51-75
Moderate PD / Monitor		26-50
Plant OK / No Action		0-25

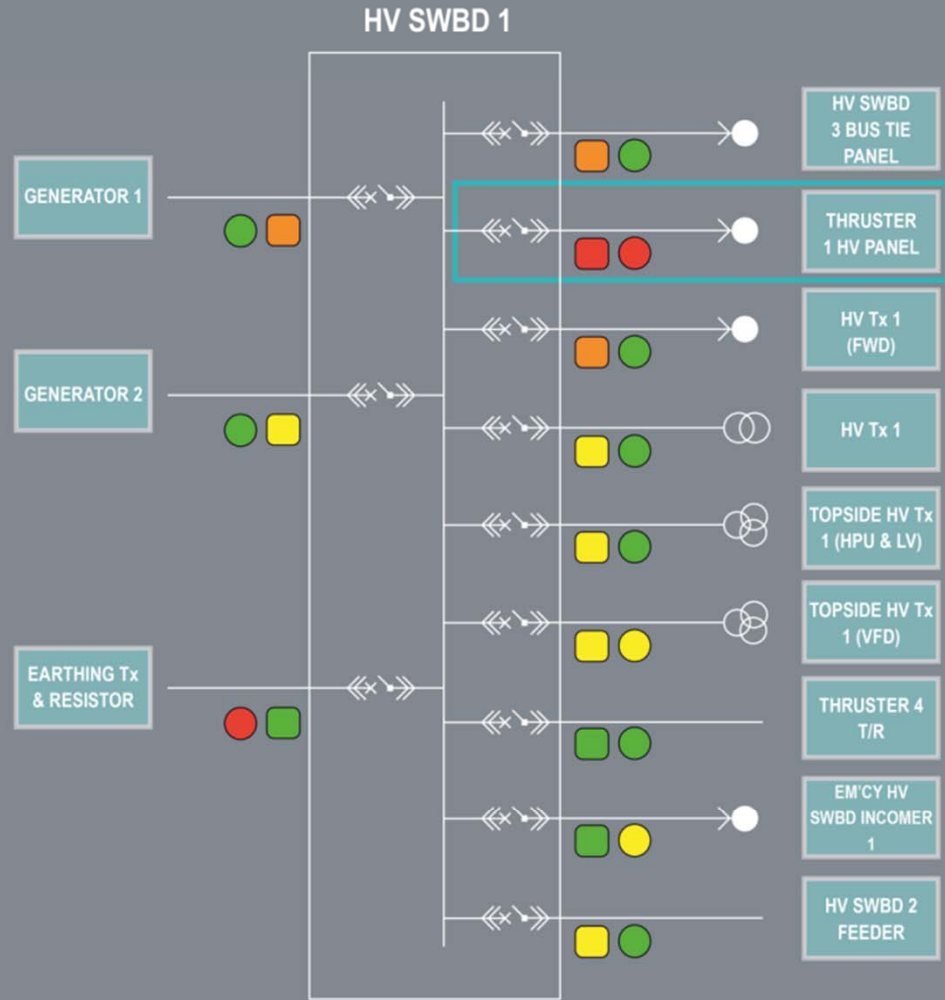
Key

- ID: Circuit ID
- Cable / Machine PD Activity
- Switchgear Local PD
- Cable length

Monitoring Period

12/04/15 14:00 - 13/04/15 14:00

Live Last Week
 Last 24 hrs Last Month



Network Selection ▲

Network Options

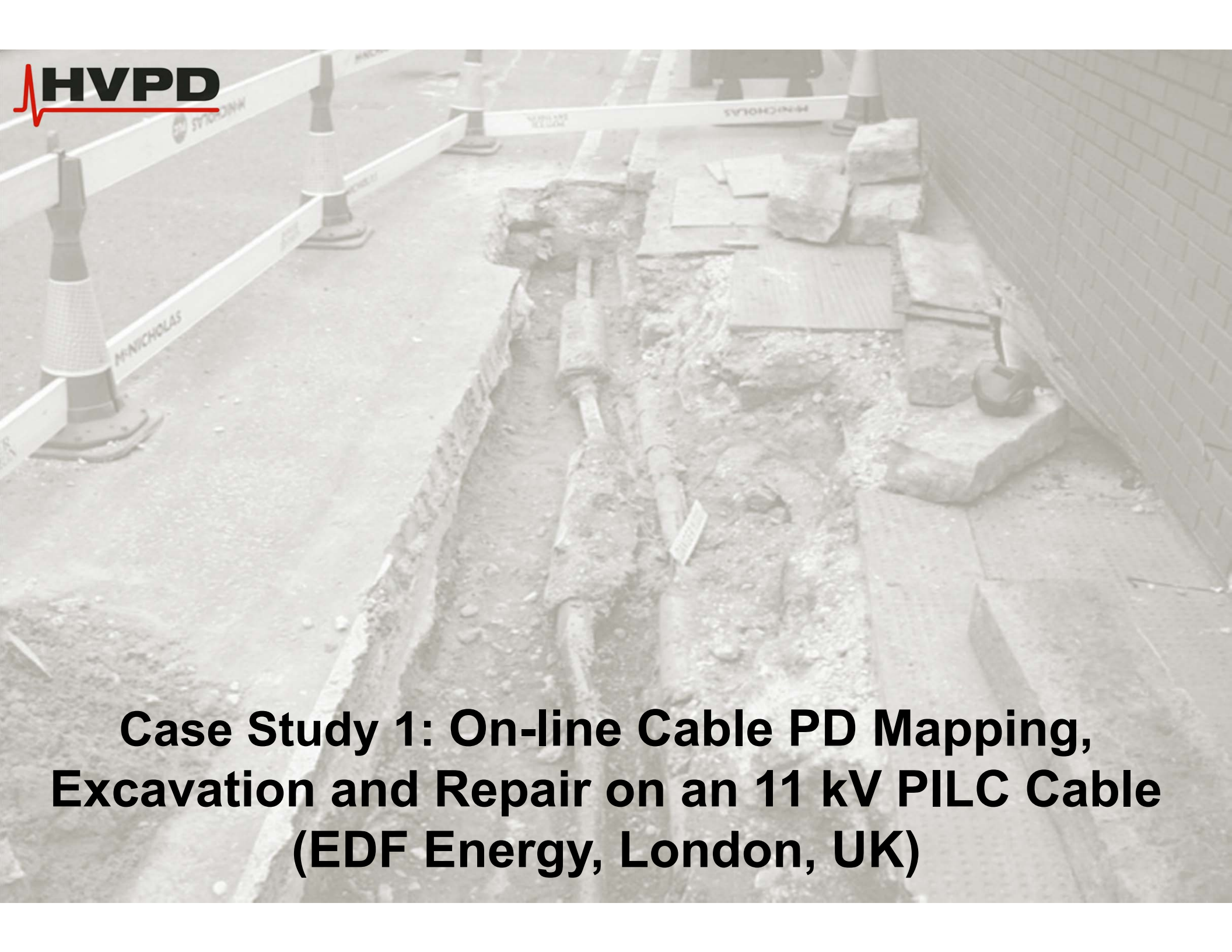
View Level

- Site Overviews
- SLD Overlay
- System Detail

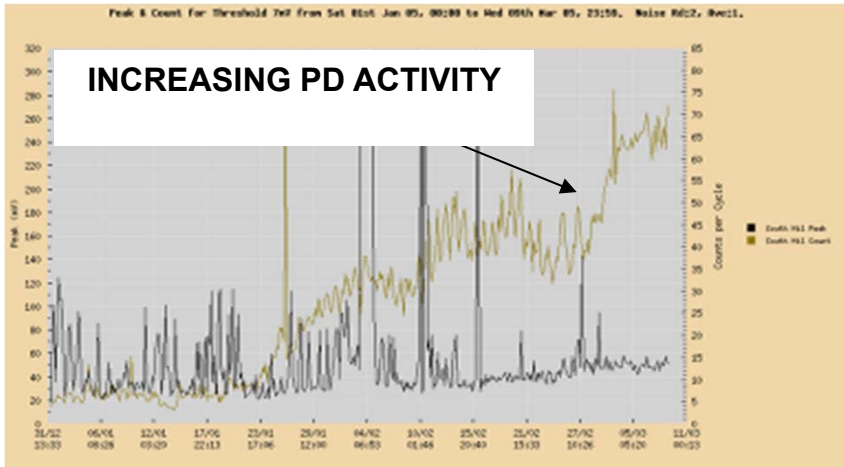
Common Sites

- Distribution Network
- 33 kV OWF Turbine Array
- 11 kV O&D Drilling Vessel
- 10 kV O&G Network

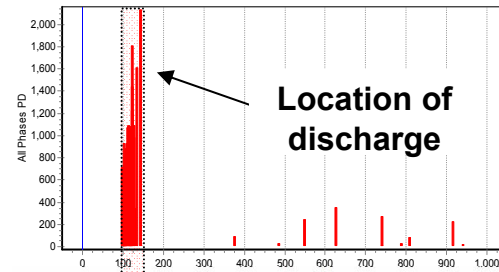
Sensor Configuration ▾
 Monitor Configuration ▾
 PD Measurements ▾

A grayscale photograph of an excavation site. A long, narrow trench has been dug into the ground, revealing a large, multi-core cable. The cable is wrapped in a thick, dark, protective sheath. The trench is lined with concrete blocks on the right side. In the background, there are several orange traffic cones and white safety barriers with the name 'M-NICHOLAS' printed on them. The ground around the trench is disturbed earth and debris.

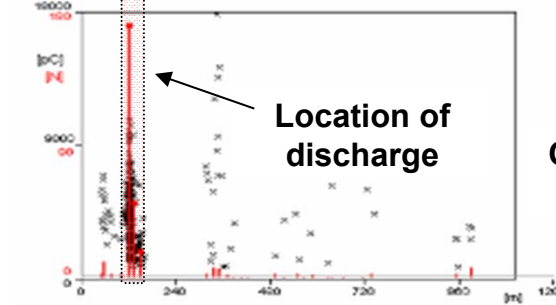
**Case Study 1: On-line Cable PD Mapping,
Excavation and Repair on an 11 kV PILC Cable
(EDF Energy, London, UK)**



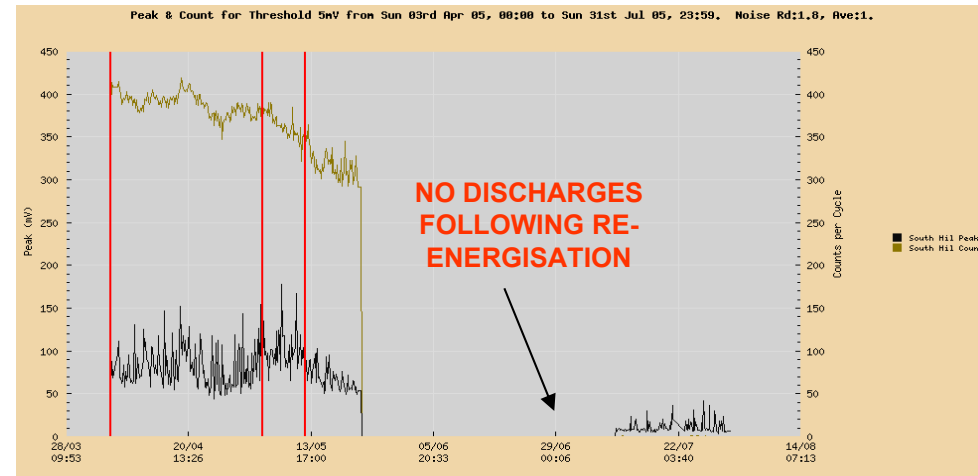
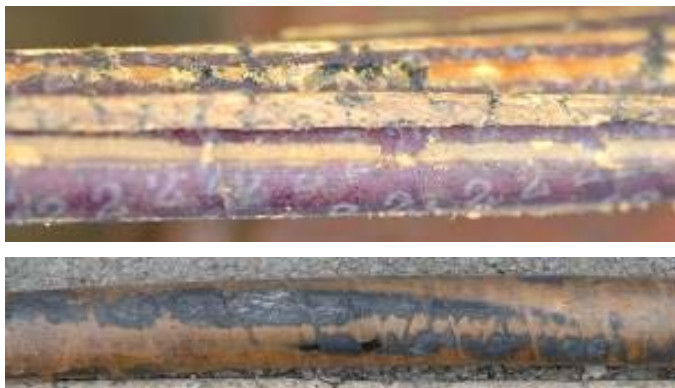
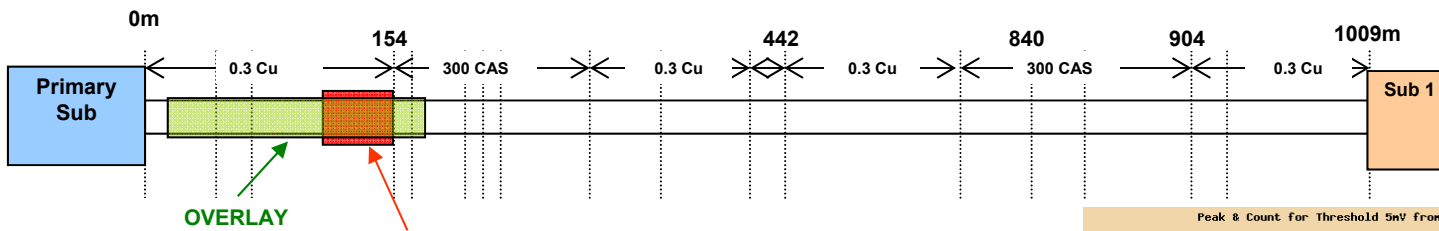
STAGE 1: On-line monitoring



ON-LINE MAPPING

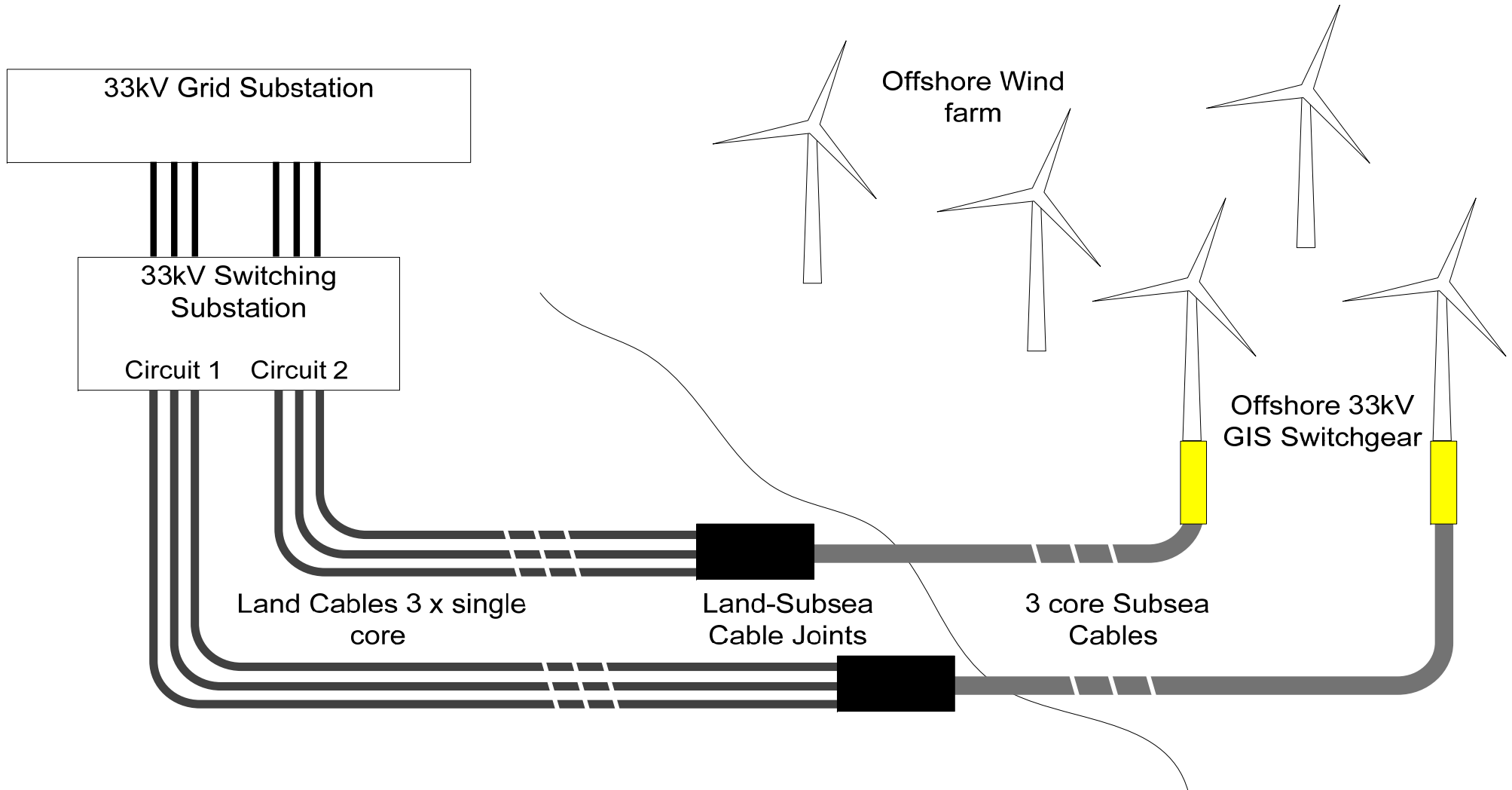


OFF-LINE MAPPING

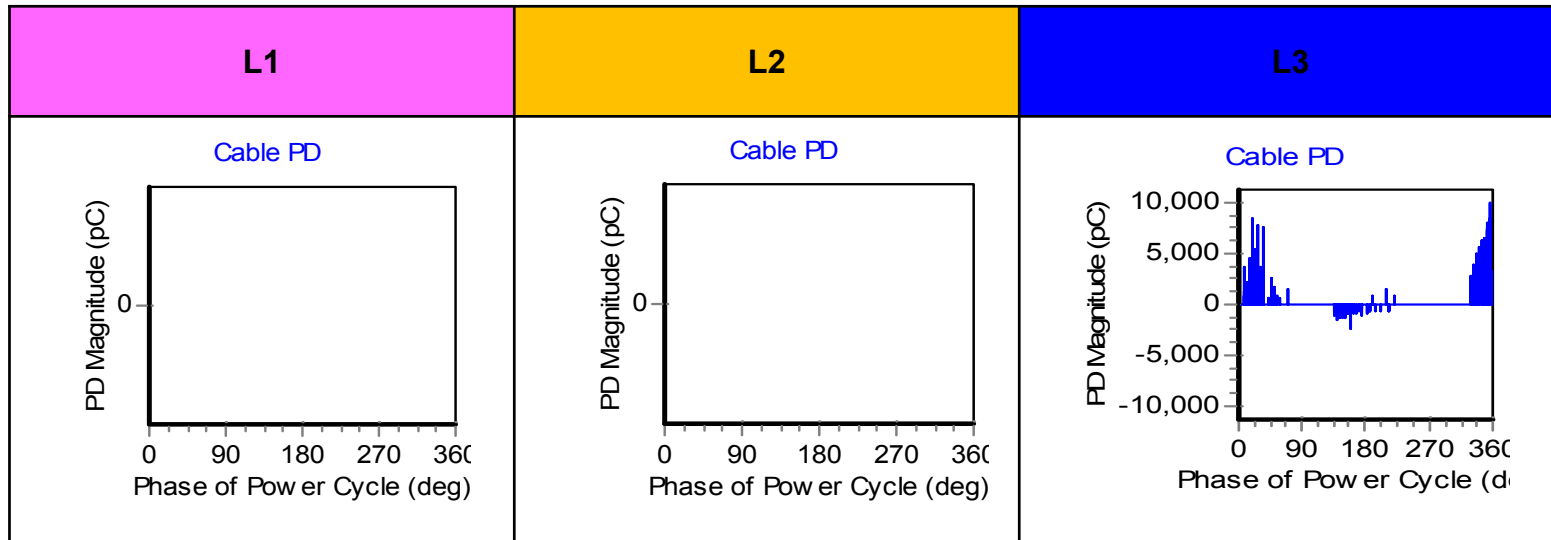


A wide-angle photograph of an offshore wind farm. Numerous wind turbines are visible, extending from the foreground into the distance across a vast expanse of water. The sky is filled with scattered white clouds. The overall scene is captured in a slightly desaturated, greyish tone.

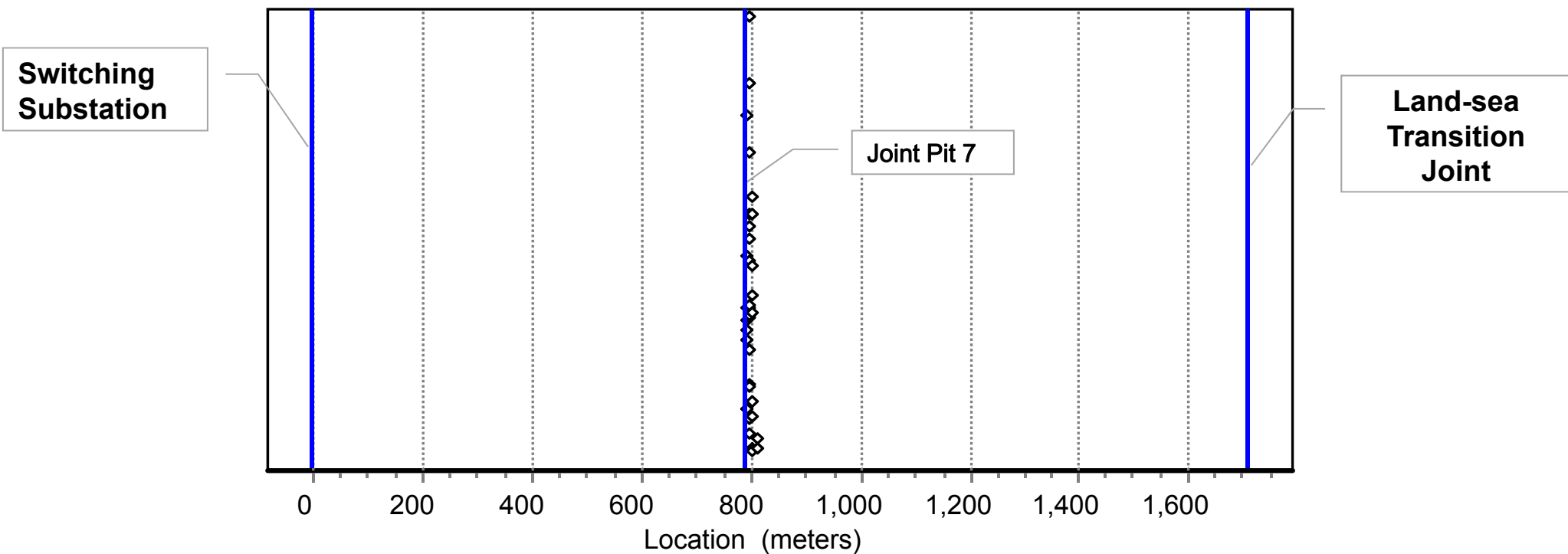
**Case Study 2: OLPD Testing, Location, Monitoring
with Preventative Maintenance on a 33 kV Land-
Sea Offshore Wind Farm Export Cable**



- 1.7 km single core XLPE land cable
- 9.6/11.5 km 3 core XLPE subsea cable

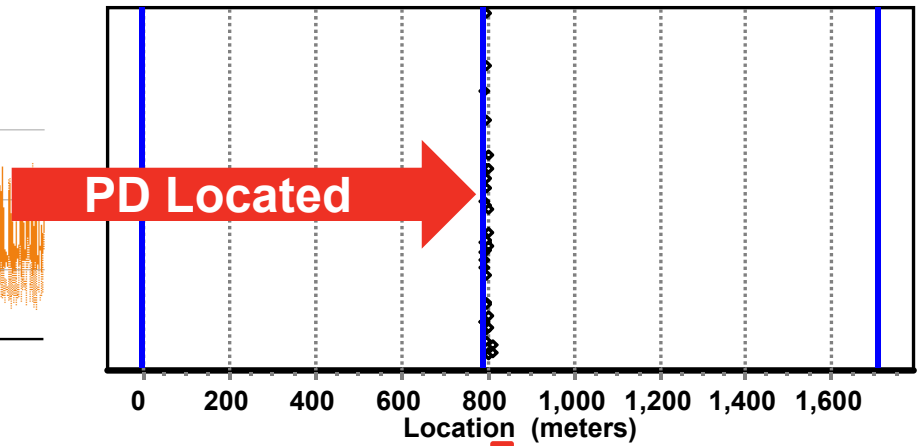
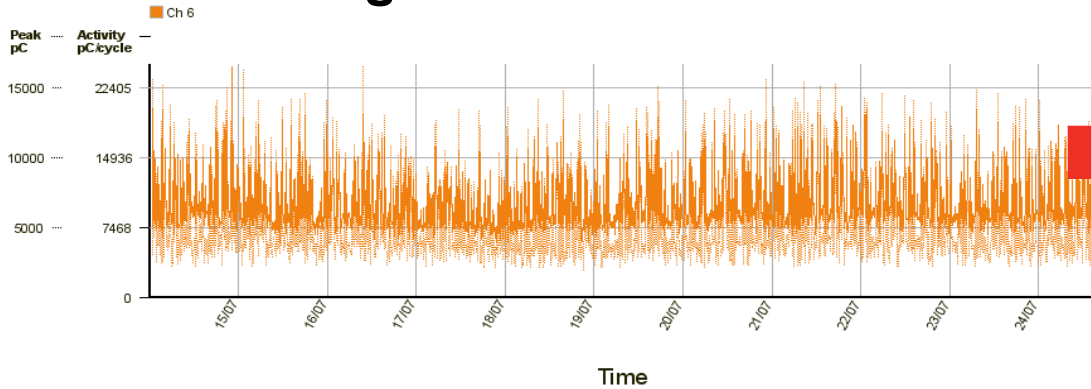


High levels of PD (of up to 10,000 pC / 10 nC)
measured on **Circuit B, Phase L3.**

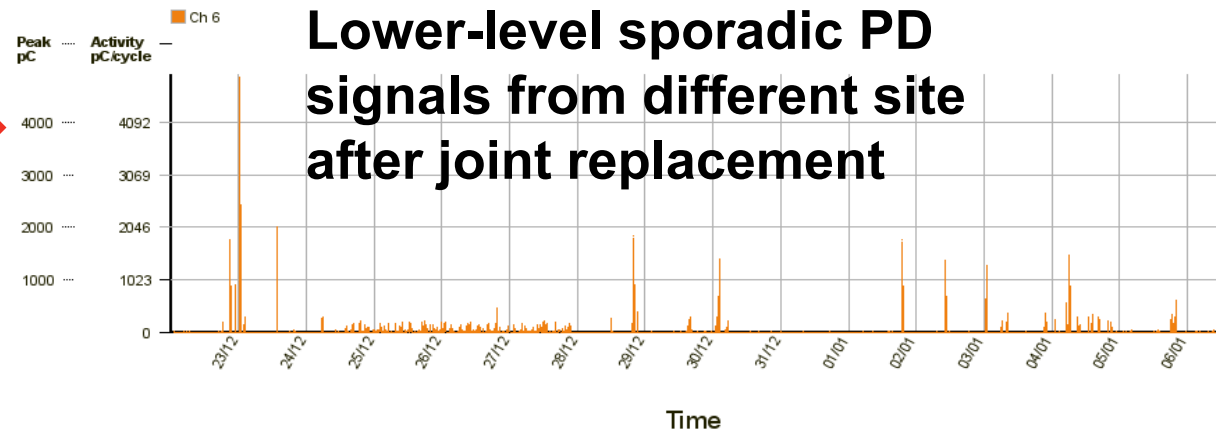


BEFORE

High PD detected on L3



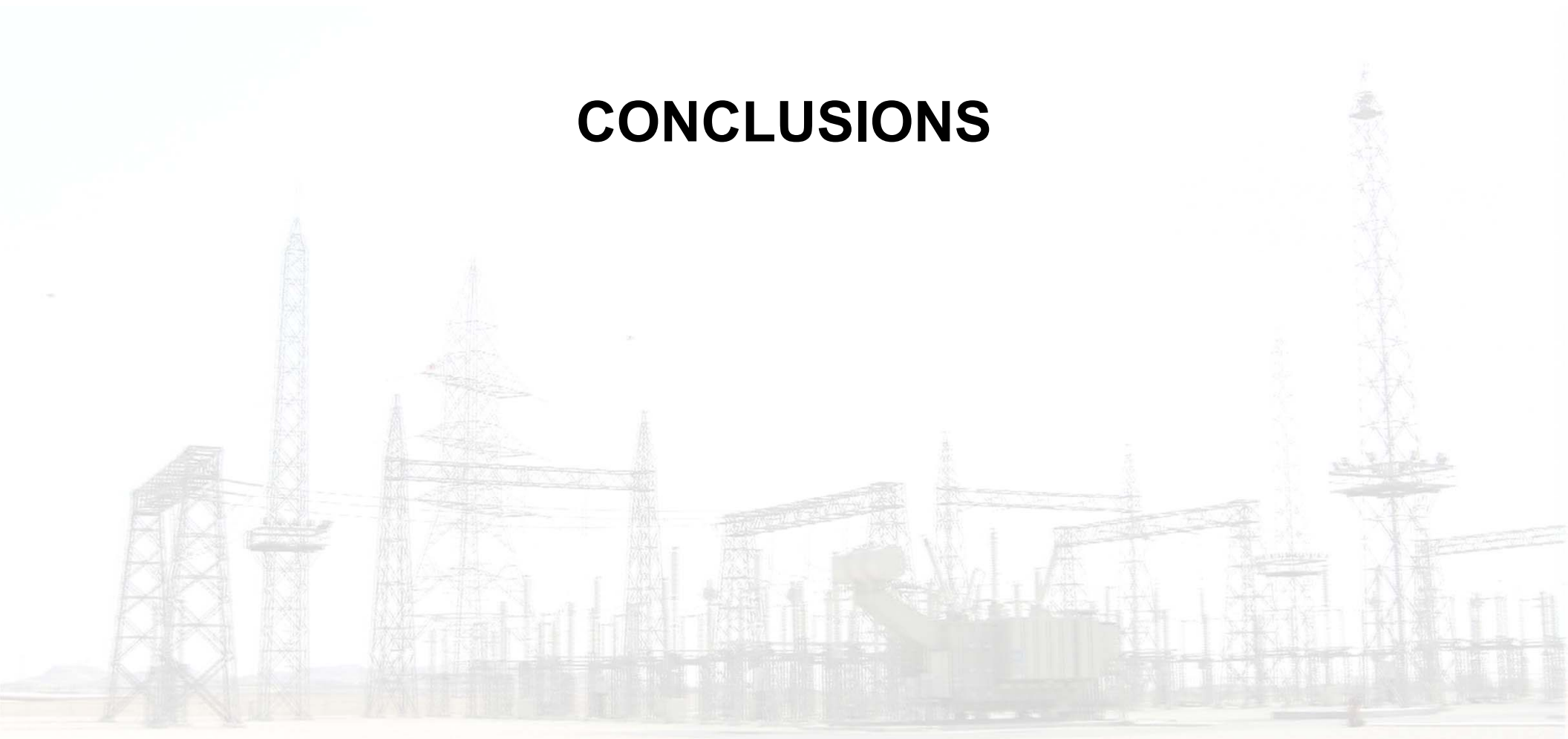
Joint 7 with PD removed and replacement cable section installed



AFTER



CONCLUSIONS



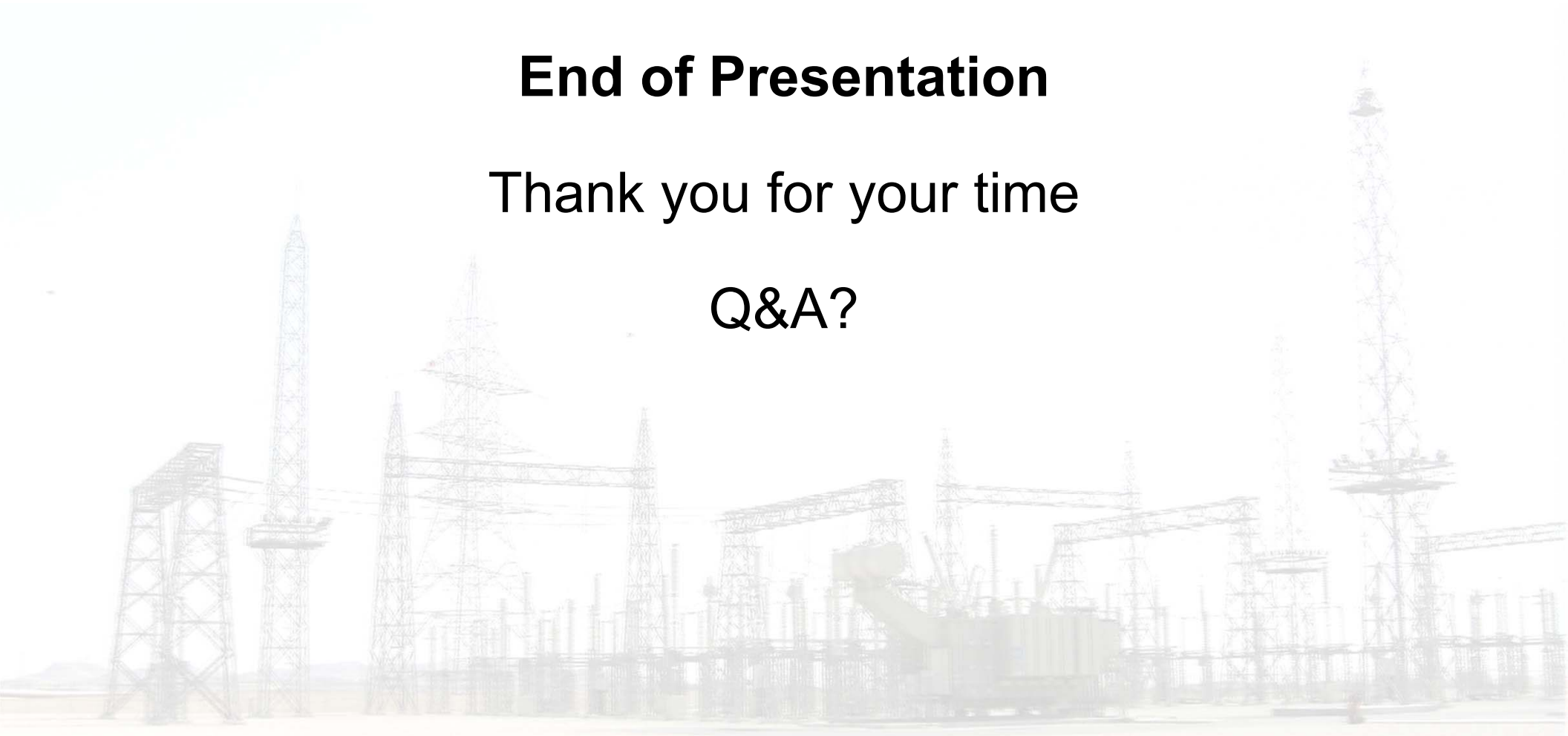
- OLPD testing is widely adopted for testing many types of MV & HV plant.
- The technologies enable the assessment of the health of MV/HV network with minimal disruption and cost.
- Equipment is tested under both normal (and abnormal) working conditions.
- PD can be detected, located and monitored, without the need to de-energise the plant.
- OLPD testing is an essential tool for the effective implementation of condition-based management (CBM) techniques to MV and HV power networks.



End of Presentation

Thank you for your time

Q&A?



Overview of On-line and Off-line PD Test Methods



CONTENTS

- On-line & off-line testing methods
- Overview of PD sensors
- MV/HV cable AC withstand voltage commissioning testing options
- Case studies



On-line

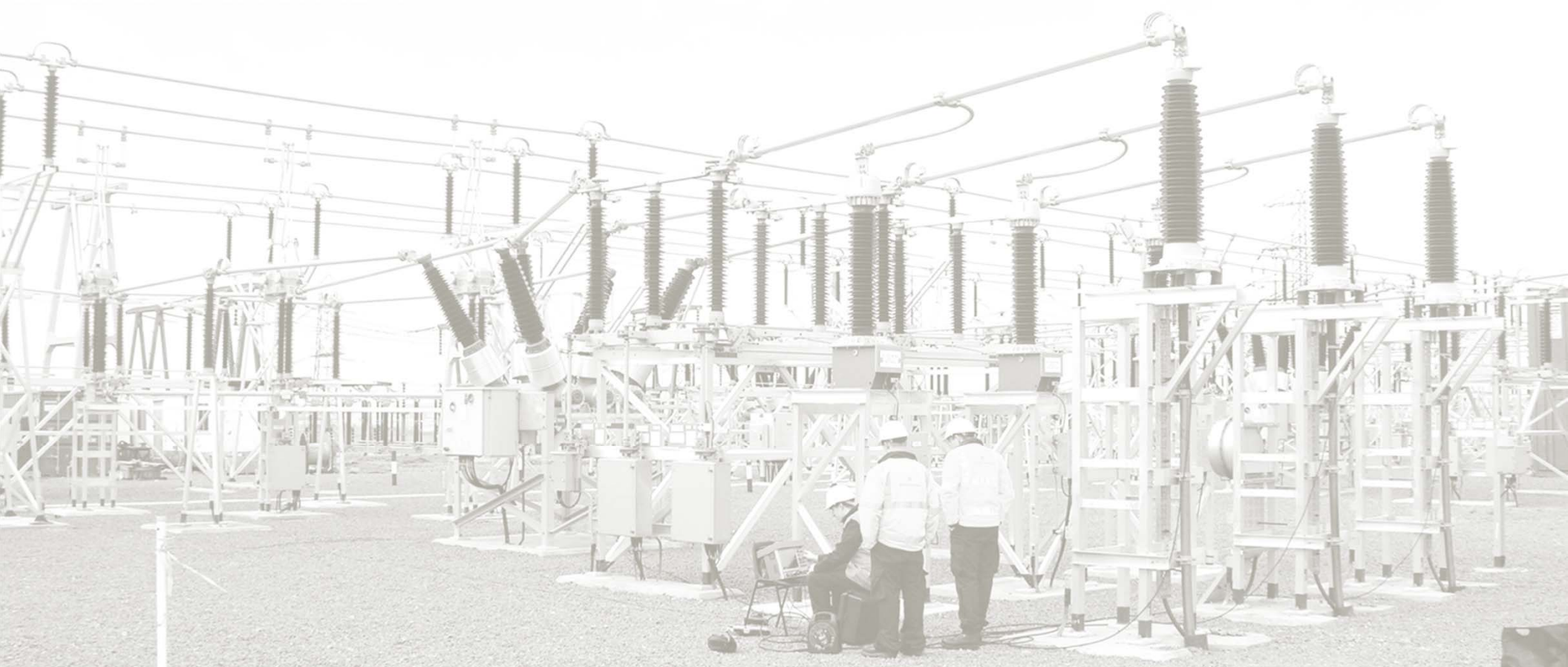
- In-service, under normal working conditions
- Various sensor options

Off-line

- Energised with external supply
- Usually HV Coupling Capacitor sensor used

ON-LINE	OFF-LINE
Advantages	Advantages
No need to isolate the circuit	Proven technology
Circuit loaded when tested	Better sensitivity
Economical & non-invasive	Drawbacks
Teed circuits can be tested	Circuit not loaded during testing
Drawbacks	Outage required
Data interpretation can be difficult	Expensive & time-consuming
Earthing pre-requisites	Teed circuits cannot be tested easily

ON-LINE TESTING METHODS





High Frequency Current Transformers (HFCT)

Detects PD in cables and remote plant (e.g. transformers/ rotating HV machines).



High Voltage Coupling Capacitor (HVCC)

Mainly applied to the PD monitoring of rotating HV machines.










Transient Earth Voltage (TEV)

Detects local PD within plant under test.

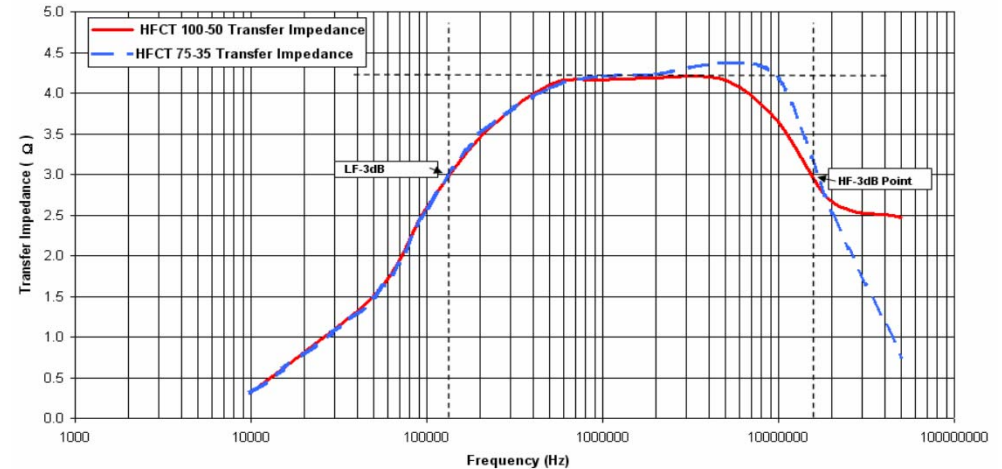


Airborne Acoustic (AA)

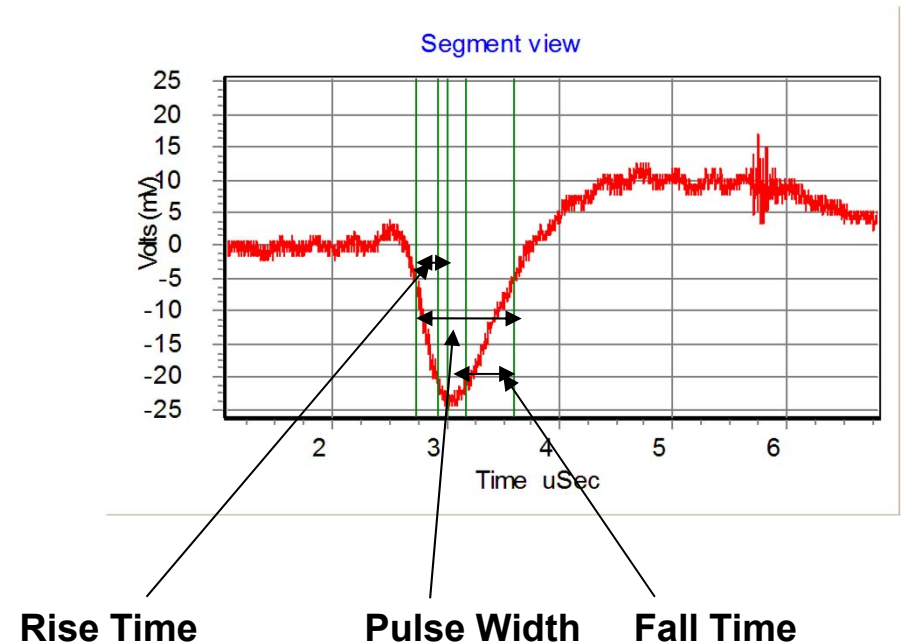
Detects airborne PD signals with direct line of sight to PD source.

Plant	Power Cables 	Cable Terminations 	Metal-clad AIS 	HV/EHV GIS 	Rotating Machines 	MV Transformers 	HV Transformers 
Sensors	HFCT	HFCT	TEV	UHF Coupler	HV Capacitor	Contact Acoustic	UHF Coupler
		TEV	Airborne Acoustic	Contact Acoustic	HFCT	HFCT	Contact Acoustic
		Airborne Acoustic	UHF Coupler		Rogowski Coil	TEV	Bushing Tap Adapters
		Contact Acoustic	HV Capacitor		RTD Sensor		HFCT
			HFCT		VHF Probes		TEV

- Detect PD in cables and connected plant
- Wide bandwidth (from 100 kHz to 20 MHz)
- Attach to power cables at terminations and earthing links of HV equipment
- Installation inside or outside of cable box
- Temporary or permanent



- Cable PD is measured in terms of charge.
- It is important to measure the number of PD pulses/power cycle (i.e. the cumulative PD activity).



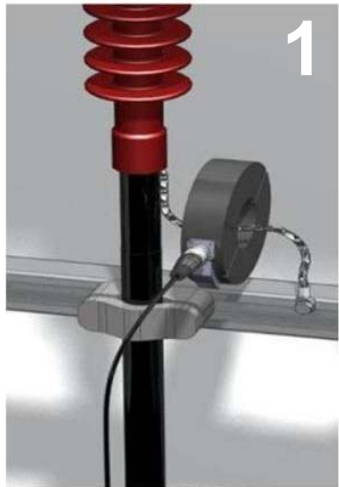
The PD magnitude (in pC) is the area under the PD pulse.

This can be calculated from the output voltage of the HFCT using the HFCT's **Transfer Impedance, Z_{TR}**

$$Q_{app} = \frac{1}{Z_{TR}} \int_{pulsestart}^{pulseend} V_{out} dt$$

The HFCT sensor should be attached to intercept *either* the conductor PD current (**i+**) or the earth PD current (**i-**)

HFCT on Earth (**i-**)



HFCT on cable with Earth brought back through (**i+**)



HFCT around cable (**i- + i+ = 0**)





Solidly bonded - lead plumbed



Solidly bonded - No insulated gland

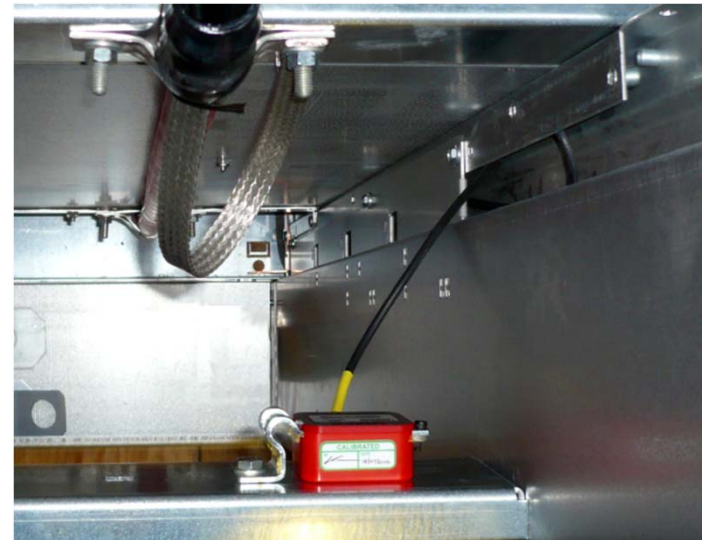


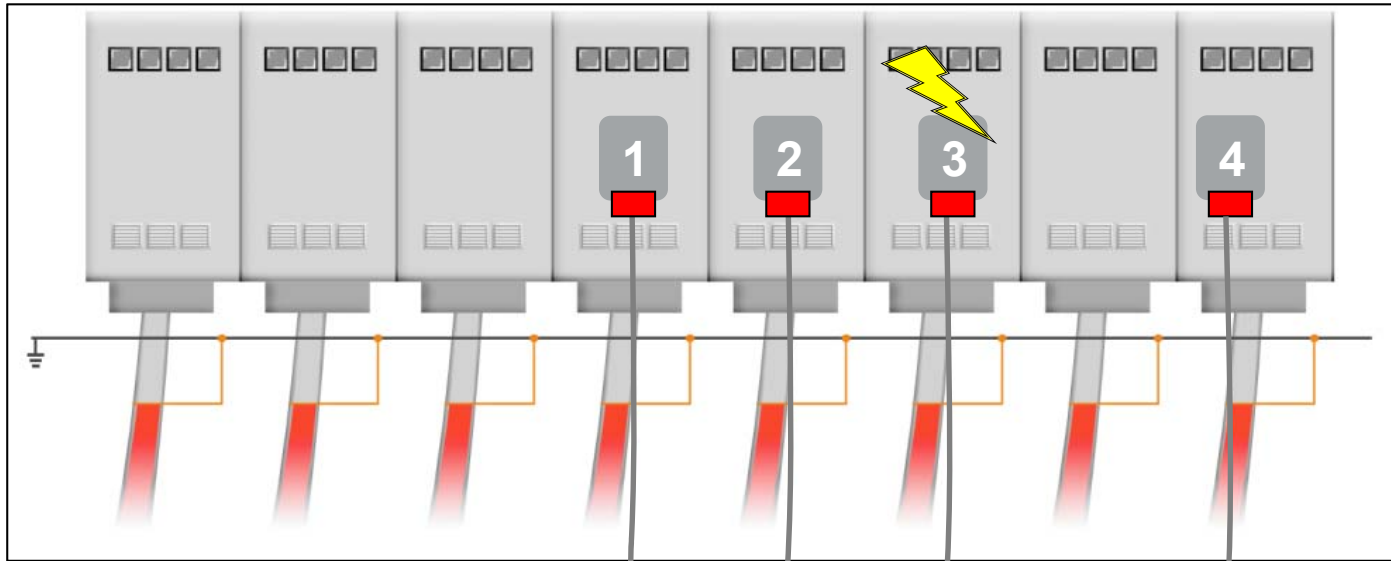
Shorting links

- Short outage to attach
- Permanent installation with external connection point
- Periodic testing/monitoring without subsequent outages



- Electromagnetic radiation from PD sites
- High frequency >5 MHz
- Main application: metal-clad AIS and SIS
- Sensitive to local (nearby) PD sites
- Also used at cable terminations and transformers
- Local PD magnitude is measured in dB

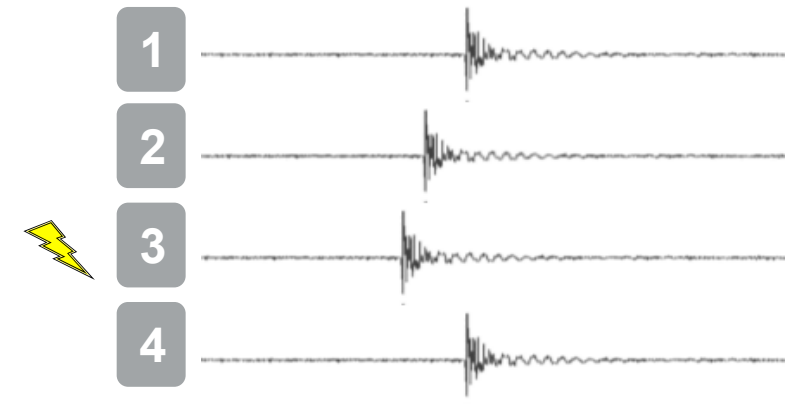


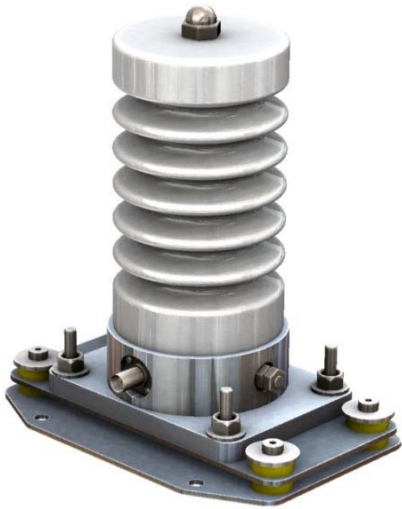


**Matched Length
Co-axial Signal
Cables**



Measured Signals on 4x TEVs



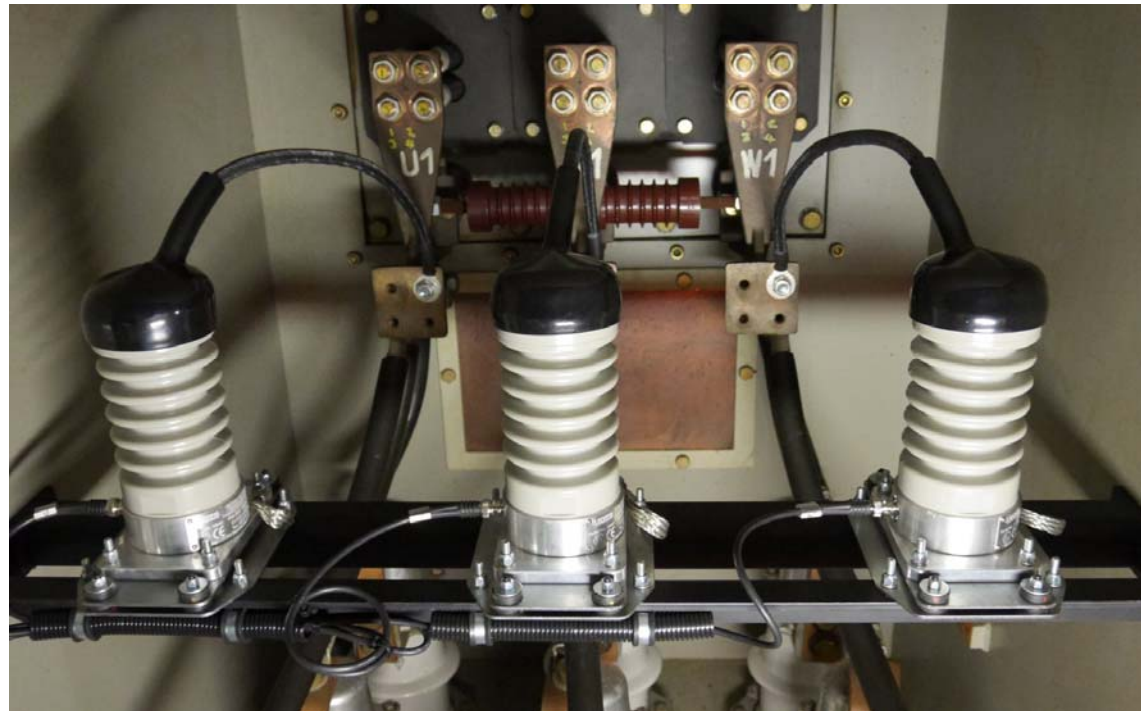


Permanent on-line unit

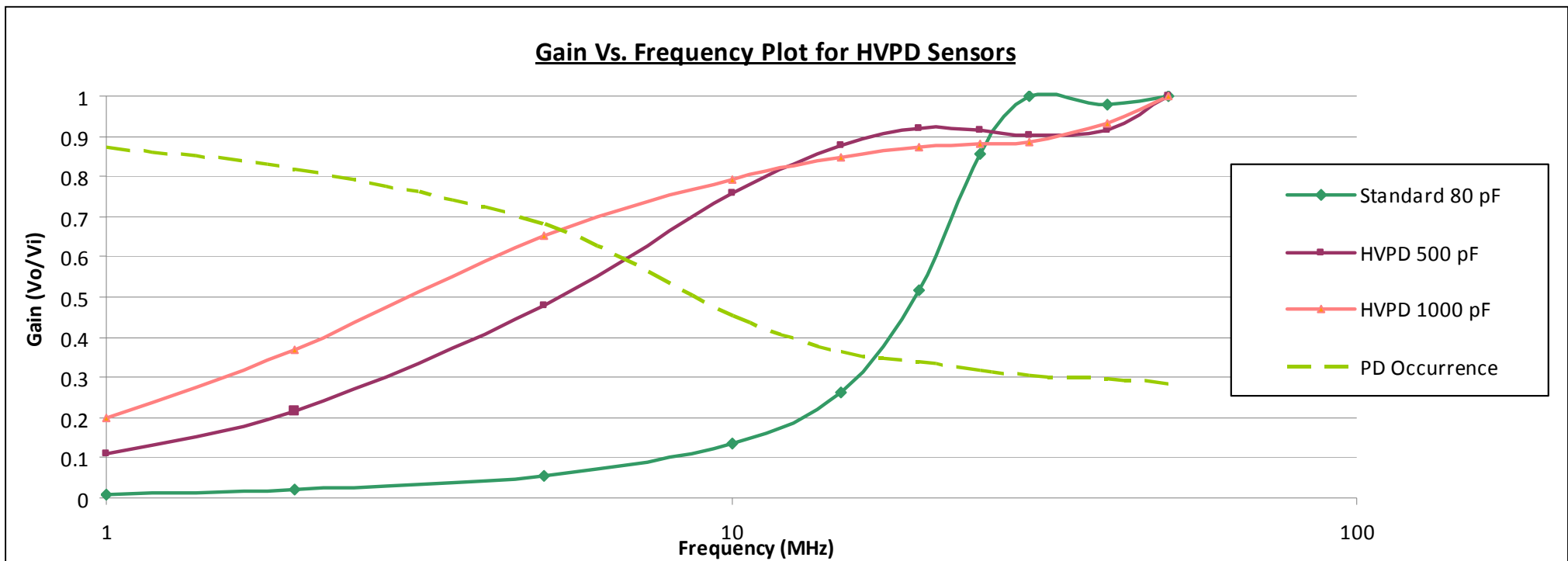


Off-line unit

- Conventional sensor for factory/lab tests
- Placed in parallel with cable/plant under test
- Requires galvanic connection to the plant under test
- Common application for rotating machines/switchgear



Higher capacitance = higher bandwidth = higher sensitivity to PD deep in machine windings





Airborne Acoustic Probe and Amplifier

- Sensitive to local PD sites
- From 10 kHz to 1.2 MHz (≈ 40 kHz common)
 - Airborne – line of sight
 - Corona
 - Surface discharge

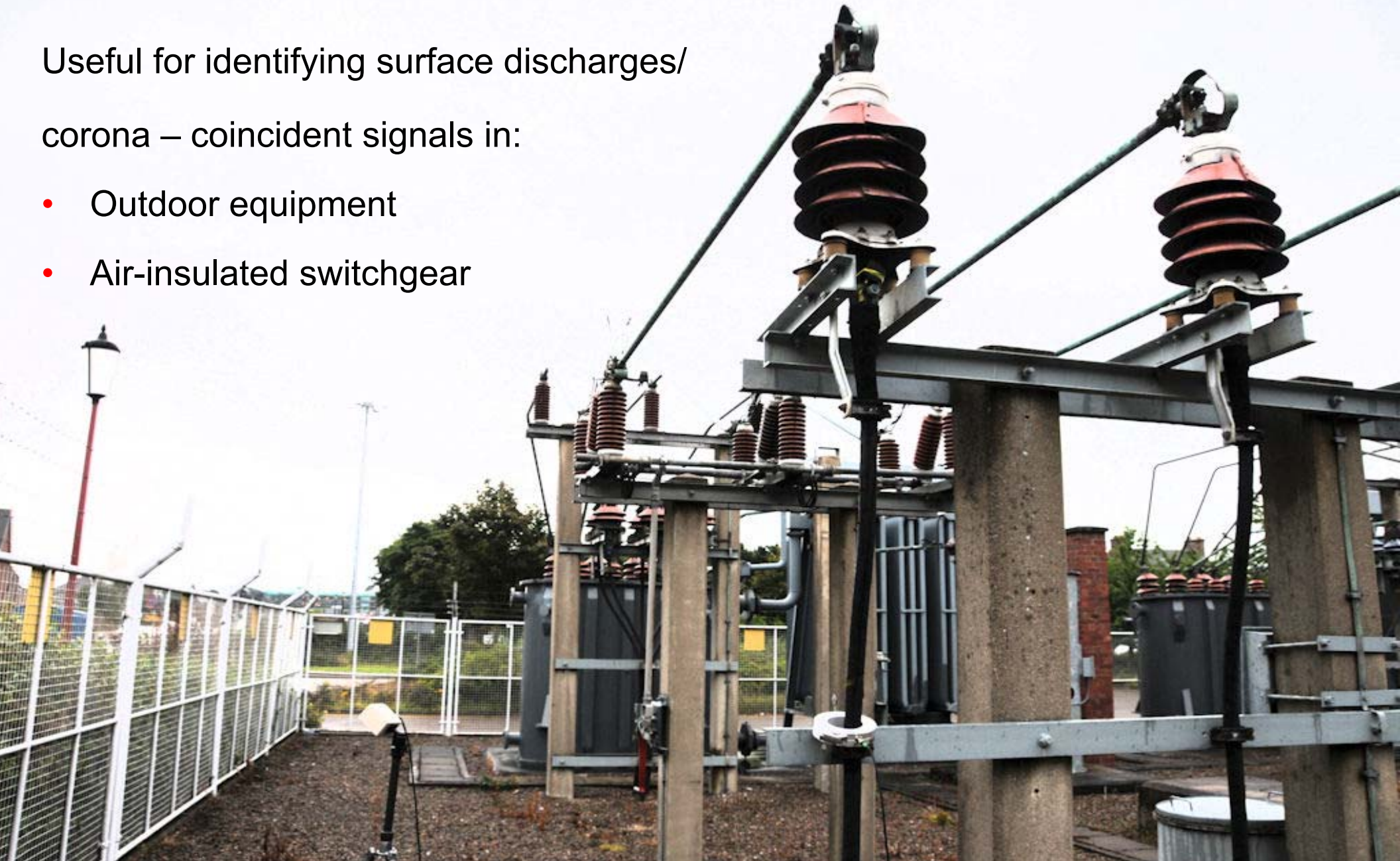


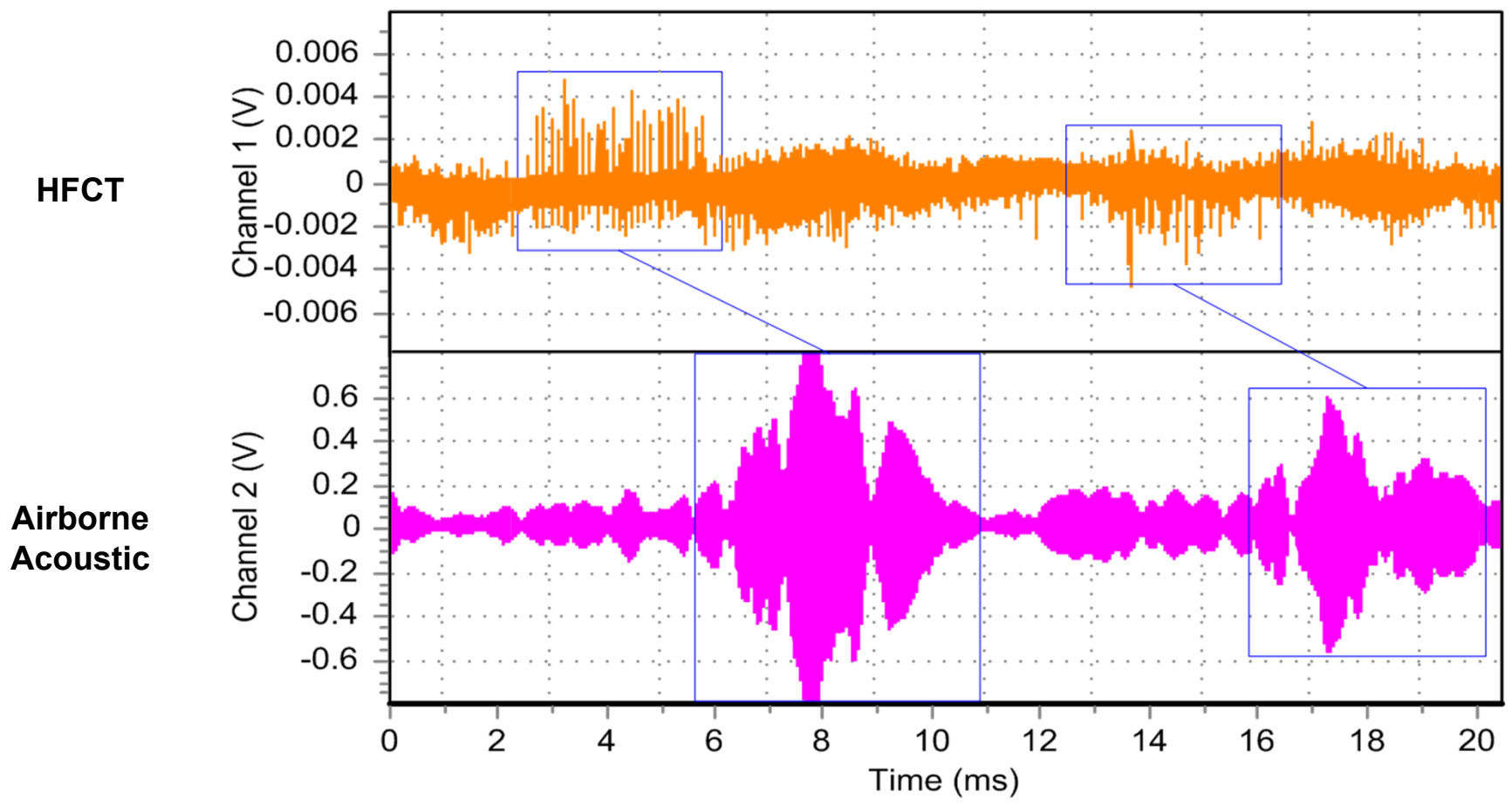
Airborne Acoustic Linearplex Sensor

- Contact
 - Vibration of equipment housing
 - Internal PD
 - Surface discharge

Useful for identifying surface discharges/
corona – coincident signals in:

- Outdoor equipment
- Air-insulated switchgear





Delay due to difference between speed of light and speed of sound

OFF-LINE TESTING METHODS



- New cable systems require AC withstand acceptance tests at commissioning.
- PD testing is now included as part of the field acceptance tests for HV and EHV cables.
- Some test specifications reference acceptance criteria from conventional, laboratory PD testing (5/10 pC).
- Whilst factory PD tests are performed at power frequency, field tests are often not.

Off-line power supplies must be dimensioned for the charging current of the plant under test.

$$I=j\omega CV$$

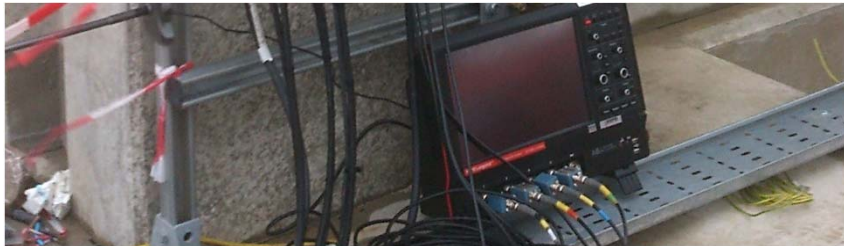
I =Charging current, ω =Test Frequency,
 C = Cable Capacitance, V =Test voltage



1. VLF (Very Low Frequency) (0.01–0.1 Hz)
example supplier: Baur (Austria), B2HV (Germany)



2. Resonant Test Systems (RTS)
example supplier: High-Volt (Germany)



3. 24-Hour Soak Test (at U_0)
No external power supply is required but extended,
24-hour PD monitoring is necessary.



4. Damped AC / Oscillating Wave (OWTS)
example suppliers: Seitz, SEBAkmt (Germany)

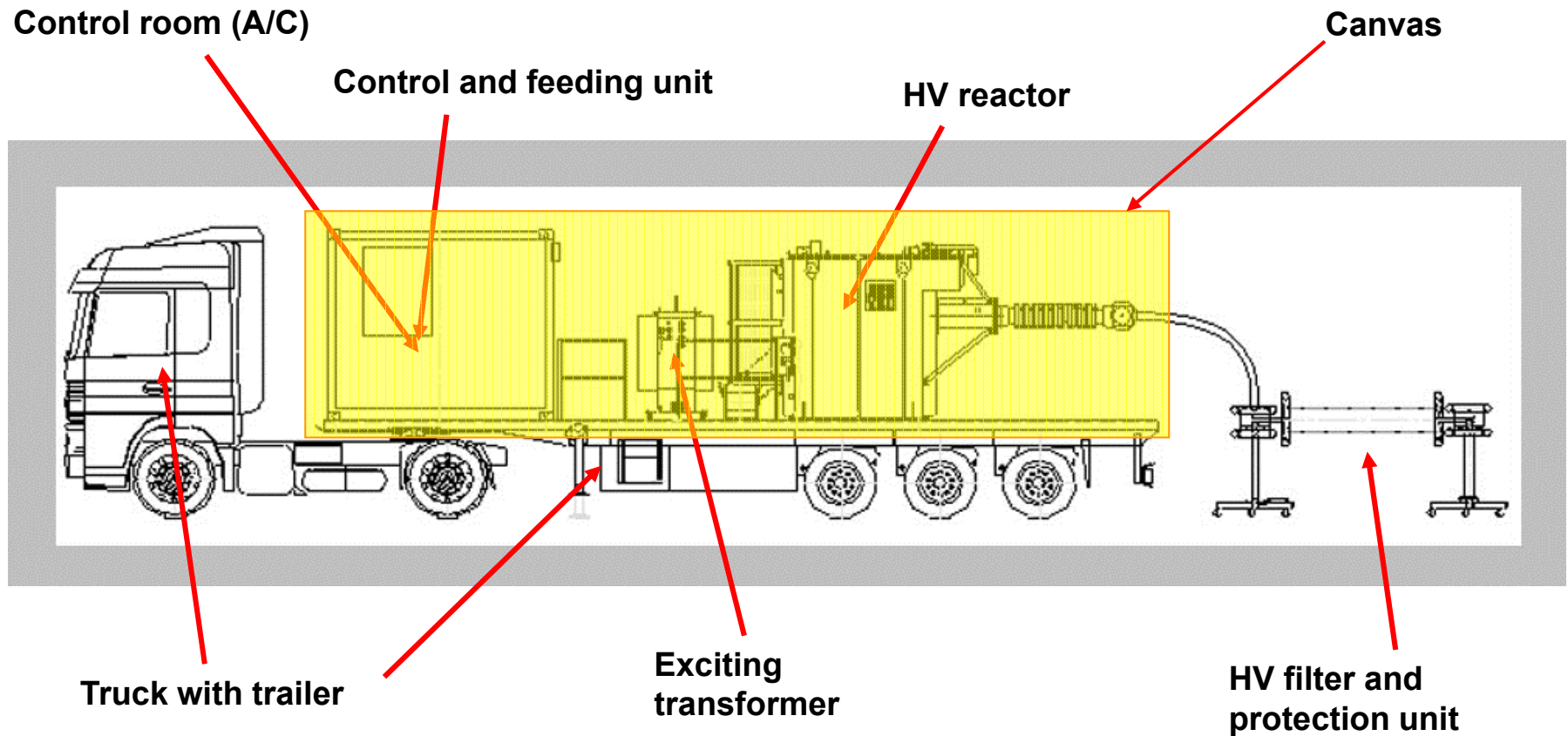


Pros

- Inexpensive, **portable** equipment
- Effective in finding water-treed cables for shorter lengths.
- Easy to perform, non-expert test
- IEEE Standard 400.2.

Cons

- PD at VLF not directly comparable to PD at AC power frequency.
- 'Noisy' test sets, filtering required.
- Concerns about trapped charges at frequencies less than 0.1 Hz.



83 A/260 kV (1650 nF) AC Resonant Test System (for 132–220 kV cables)



Pros

- Allows direct comparison of factory PD tests to the field tests.
- Provides continuous, near power frequency AC withstand voltage.

Cons

- Large, expensive test equipment (for HV/EHV cables) although more compact RTS technology is available for MV cables.

Commissioning Testing (Off-Line)

- Measure PDIV, PDEV.
 - Measure PD Level & Intensity.
 - Identify PD pattern.
 - Identify location of PD source.
- ⇒ Guiding criterion is that the cable system should be **PD free** (<5 pC) at the specified test voltage ($1.7U_0$) for the HV cable systems.
- ⇒ Less than 10 pC for MV systems using conventional test systems.

Maintenance Testing (On-Line)

- Assess individual PD sources separately.
 - Measure PD level & intensity.
 - Identify the location of the PD source(s) by PD mapping.
 - Assess impact of individual PD sources against cable design (i.e. insulation materials, experience, etc).
- ⇒ Develop individual assessment and ranking of cable joints, terminations and cable sections.



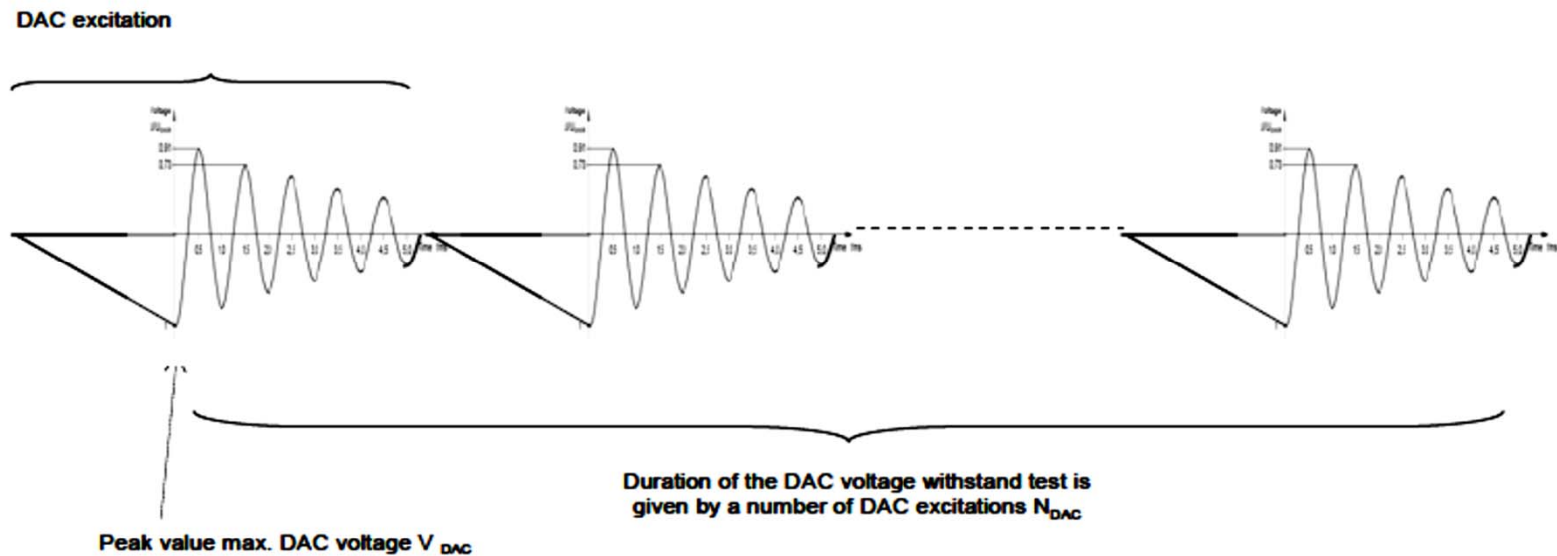
Pros

- Can energise long lengths of cable with smaller power supply.
- Easy to perform, non-expert test.

Cons

- Only limited number of over voltage cycles (2–3) applied.
- Difficult to do PD reading reliably (distributed PD).
- Tan Delta / Loss factor measurements are derived, not measured.

- 50 shots of individual discharges.
- Not continuous AC.



Wide variation of test voltage parameters:

DC charging time: 0.25–62.5 s

DAC frequency: 38–368 Hz

DAC damping: 3.7–20.4%

The different scales of the DC charging and the DAC oscillation create a wrong impression!



Pros

- Inexpensive as they do not require an external power supply
- Energised at line voltage U_0 only.
- Low risk of failure during test.
- Can perform extended PD testing and monitoring over the entire 24-hour soak test.

Cons

- May not find incipient insulation defects at U_0
- Not fully diagnostic or predictive as there is no overvoltage.

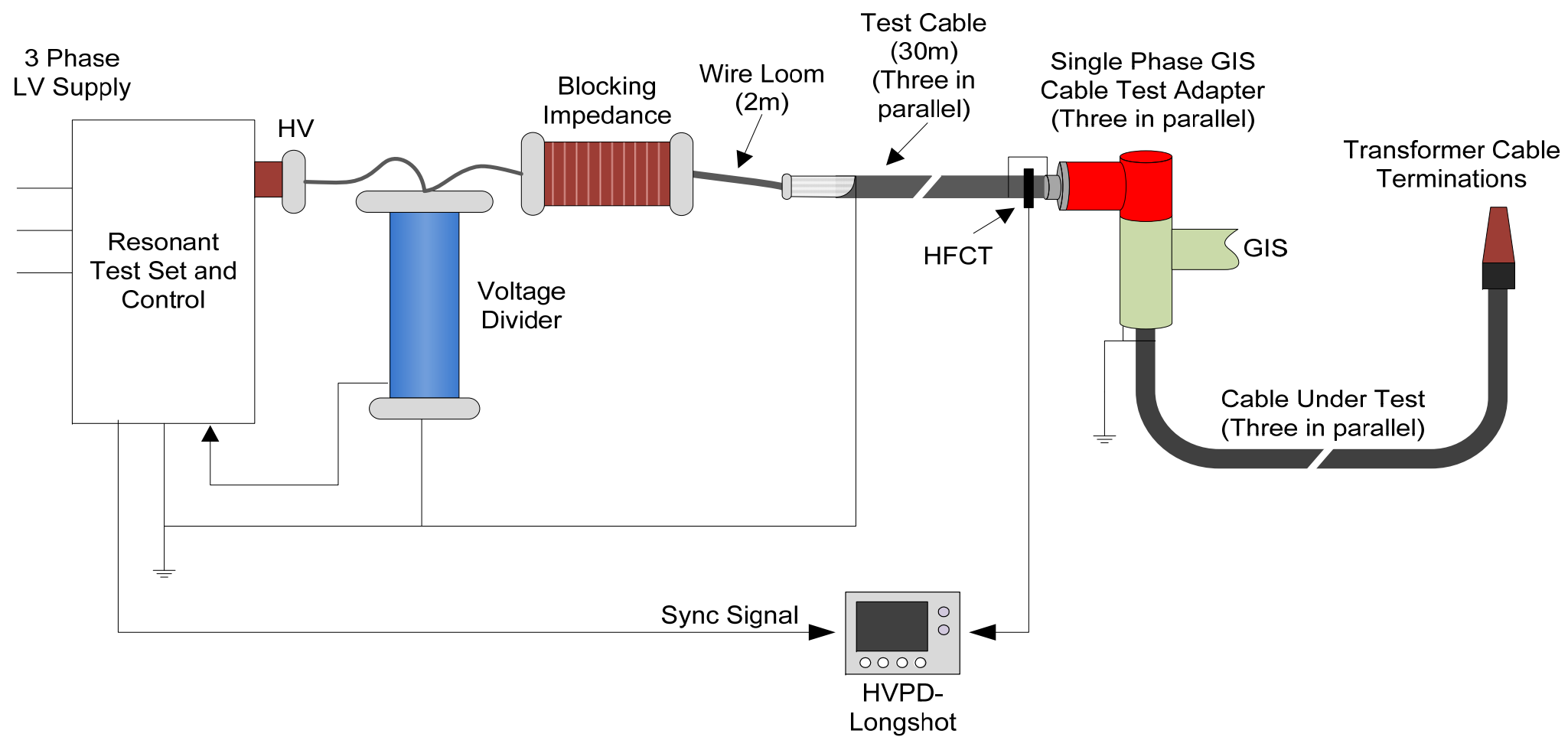


CASE STUDY 1: RESONANT TEST SYSTEM (RTS) TESTING

- The distance from RTS to cable under test could be tens of metres.
- Exposed HV connections pickup noise and generate corona.
- Length of exposed HV connections (and interference) minimised with test cable.

PD signals were measured using:

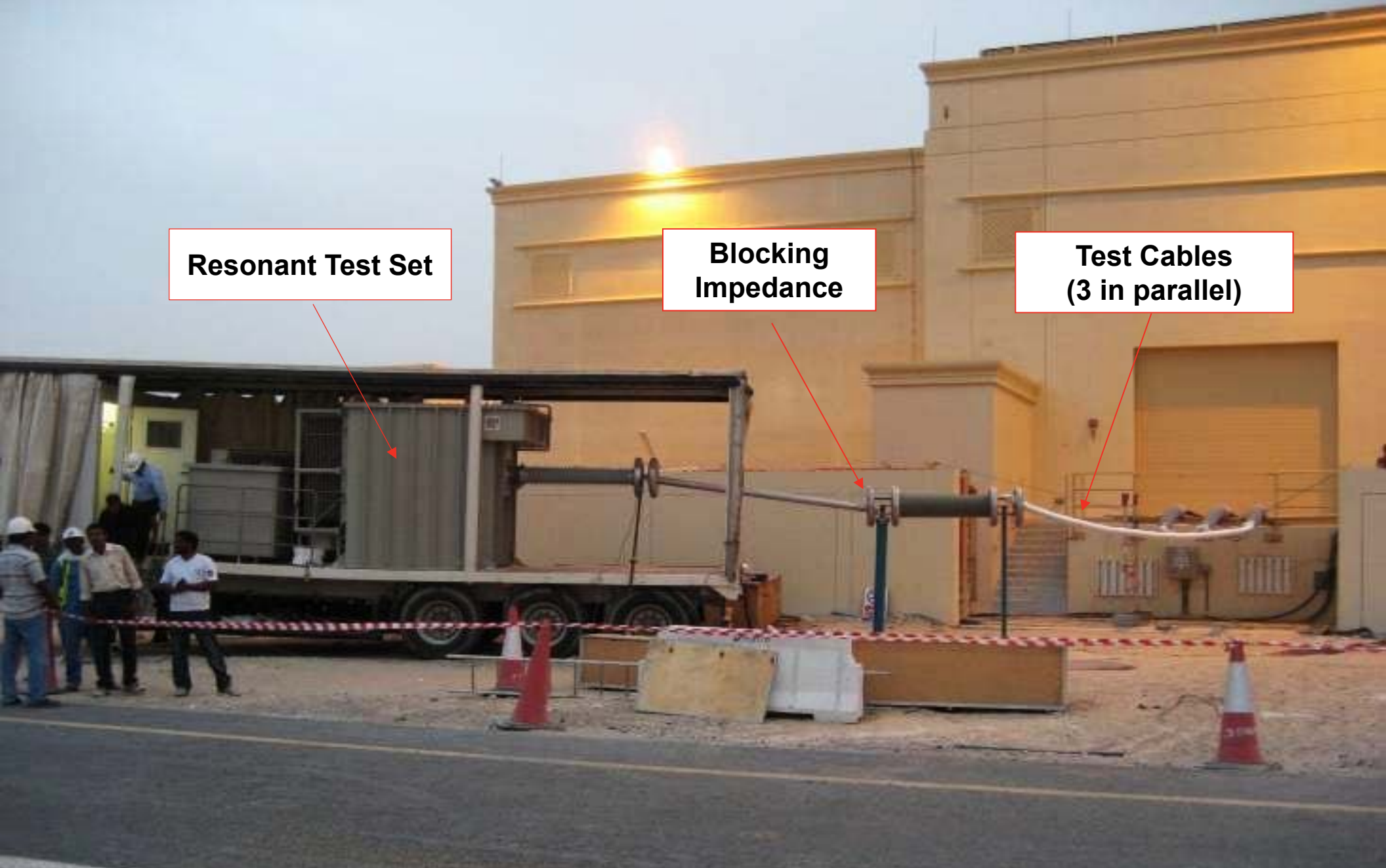
- HFCT sensors placed around the earth jumper cable between the cable termination and GIS housing.
- 8.3 nF coupling capacitor placed on the feeding end of the resonant test set to discriminate any noise or interference from the test set.



Resonant Test Set

Blocking Impedance

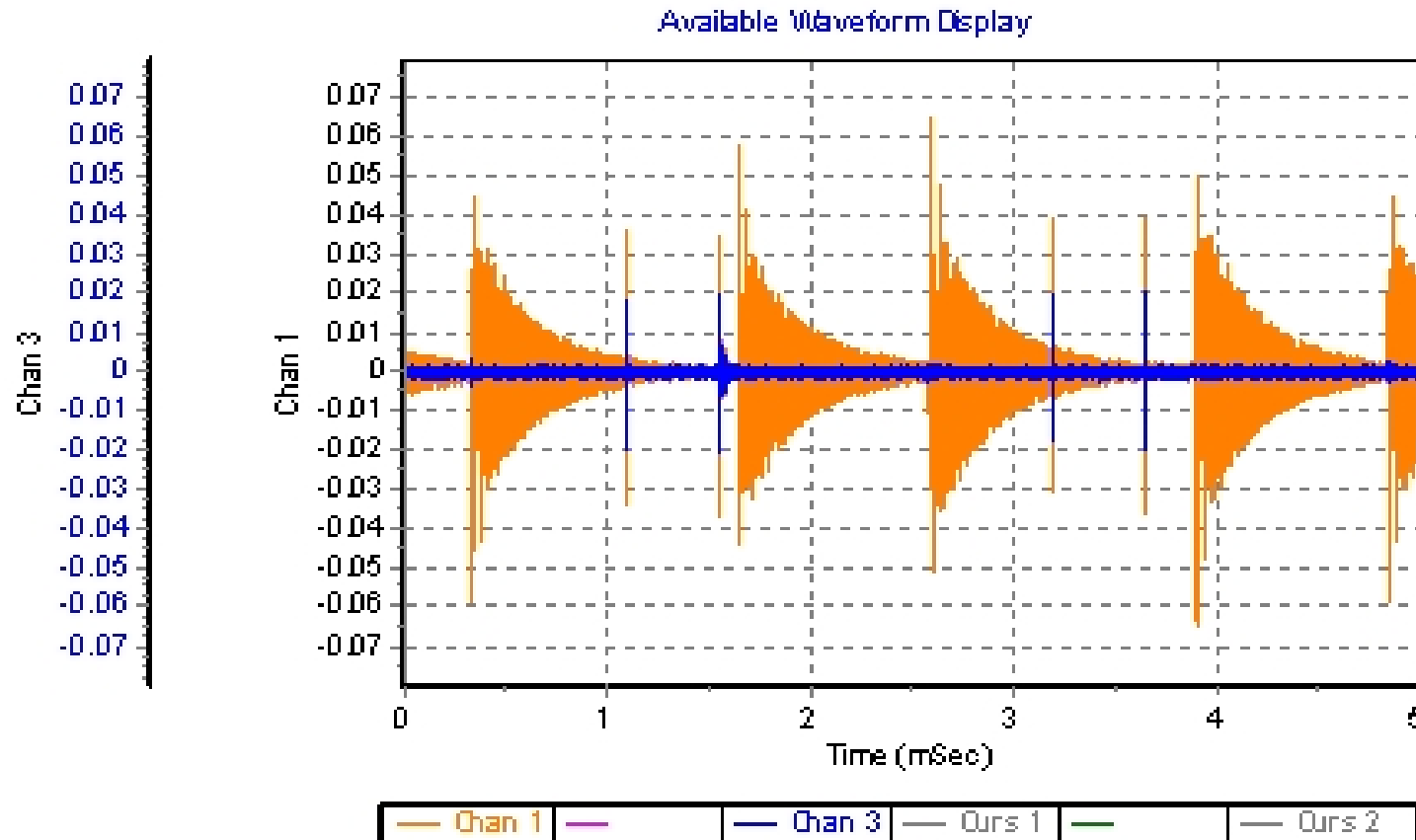
**Test Cables
(3 in parallel)**







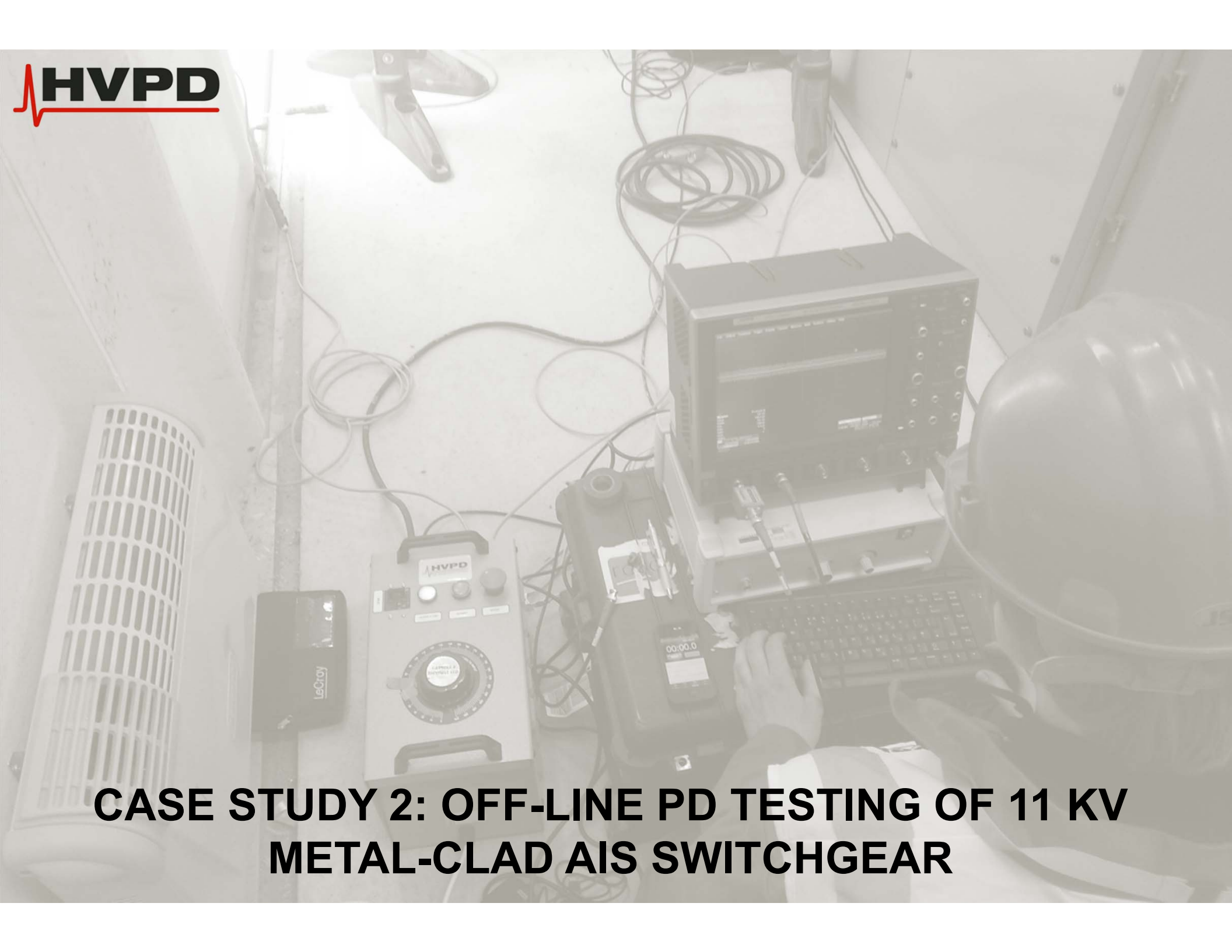
- Noise generated by RTS frequency convertor.
- Blocking impedance helps with filtering.
- Can be gated out with dedicated channel.
- PD event recognition or high pass filters often more effective.



- PD measurements made at various voltage steps.
- Ensure cables are PD-free.

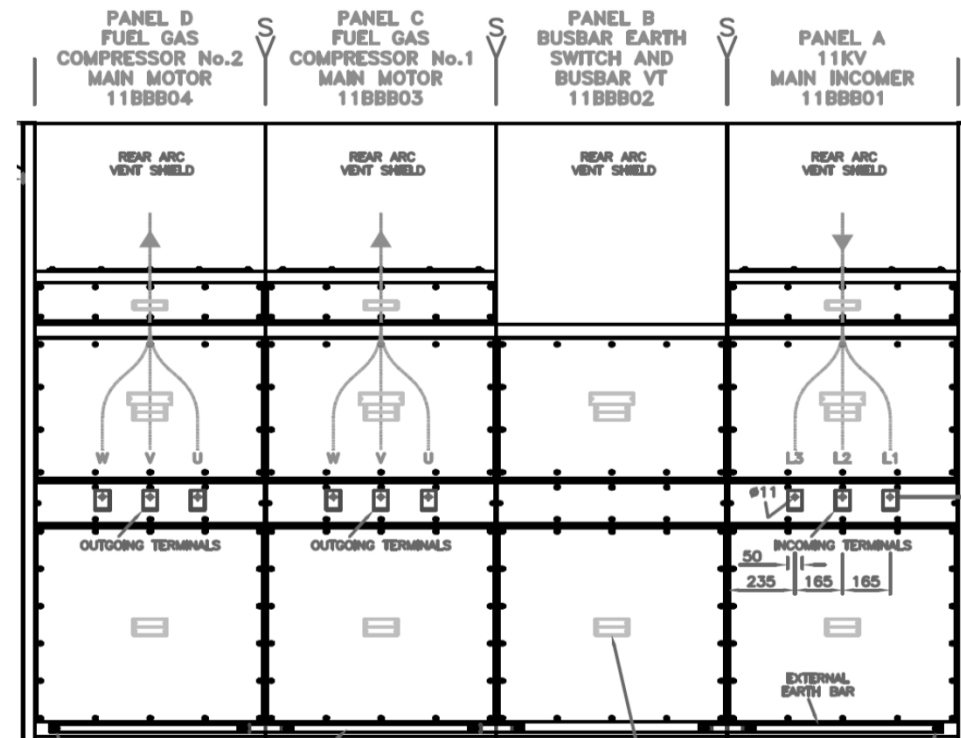
Circuit:	Circuit 1							
Test Date:	13/05/10							
Test Voltage (kV)	Current (A)	Frequency (Hz)	Power (kVA)	Reactor Temp. (°C)	PD Level R (pC)	PD Level Y (pC)	PD Level B (pC)	Result
76	3.4	221.33	250	42	no PD	no PD	no PD	Ok
114	5.1	221.33	561	42	no PD	no PD	no PD	Ok
132	5.8	221.28	777	42	no PD	no PD	no PD	Ok
76	3.4	221.33	250	42	no PD	no PD	no PD	Ok
114	5.1	221.33	561	42	no PD	no PD	no PD	Ok

- PD measurements were made at 76 kV, 114 kV and during the 132 kV HVAC withstand test.
- No PD signals were detected.
- Corona interference was detected in some cases and remedial action was taken to remove this so that this did not confuse measurements.
- The background noise levels on the HFCT sensors were relatively low in all tests, allowing good sensitivities of down to 20pC to be achieved.
- Noise interference from the resonant test set was detected with two 150 μ s pulses at the zero crossing points of the voltage waveform.
- The HVPD PDGold© *EventRecogniser* software was able to classify and discount these signals as noise.



CASE STUDY 2: OFF-LINE PD TESTING OF 11 KV METAL-CLAD AIS SWITCHGEAR

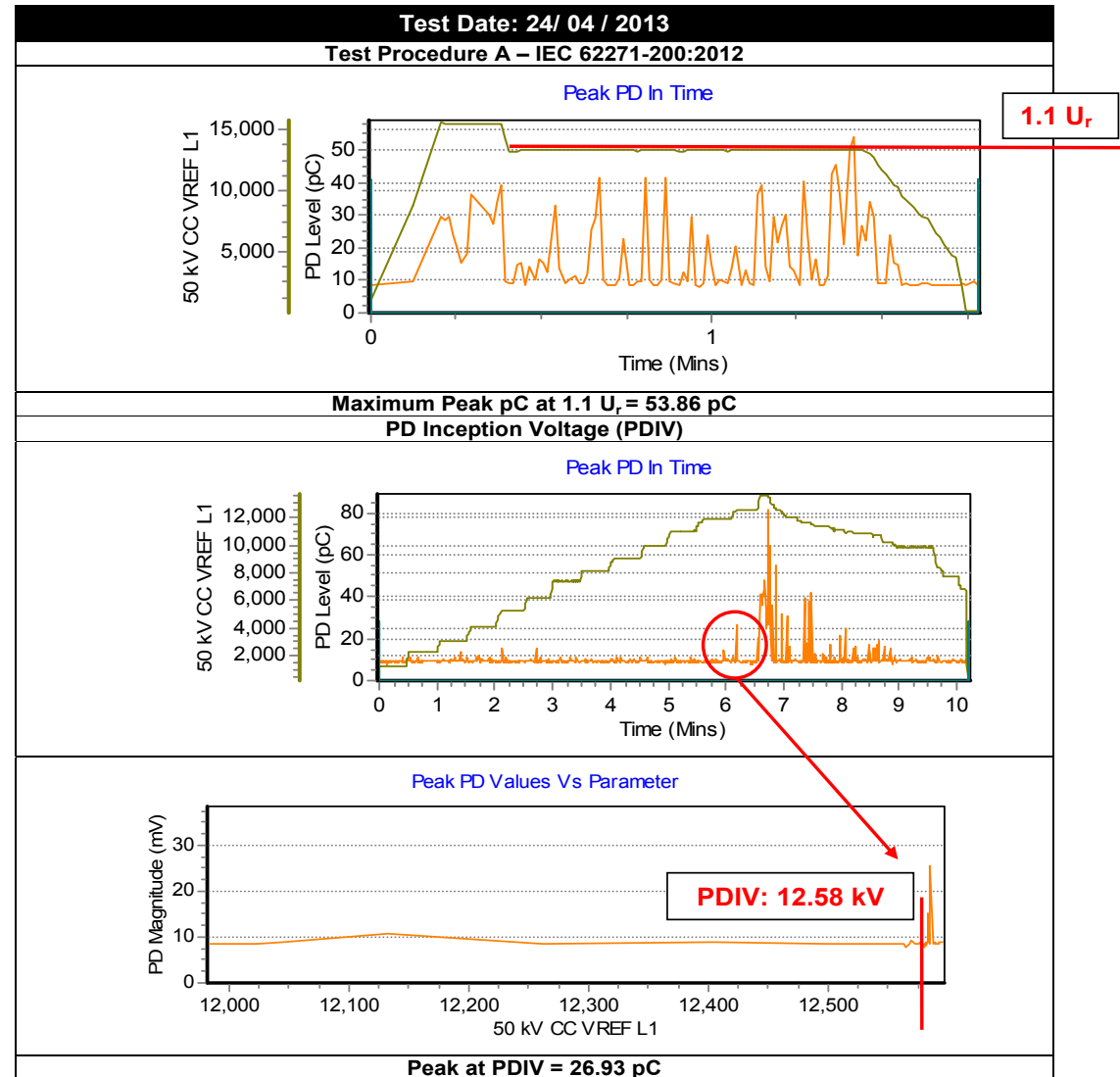
- Off-line PD testing of the newly installed 11 kV Air-Insulated Switchgear following a failure.
- Measurements made to determine insulation was in good condition prior to putting it into service.
- Portable power supply used to energise the busbar to $1.1 U_0$ (13.2 kV).



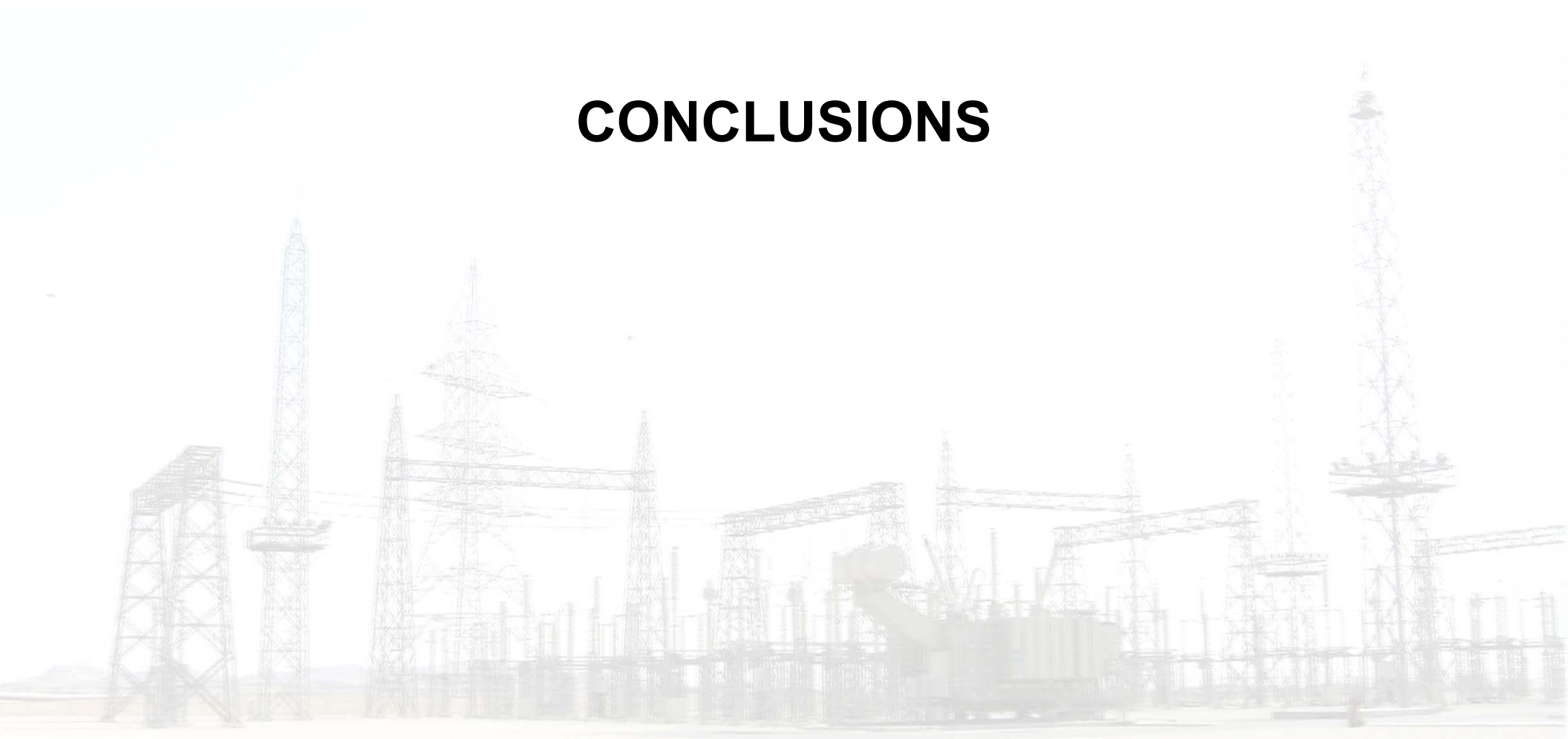
- The off-line test equipment and HVPD Longshot™.
- Voltage was applied (as per IEC 62271-200:2012) to each individual phase in turn with other phases isolated.



- Low levels of PD with peaks up to 54 pC were detected at 1.1 U₀ (13.2 kV phase to ground)
- Concluded the PD was not originating in the breaker sections (Breaker open and closed). PD was isolated within the Bushing and visual inspection was recommended (dirt, moisture or signs or tracking).
- The PD levels detected were considered to be low however maximum permissible partial discharge quantity at 1.1 U₀ shall be ultimately agreed between the manufacturer and the end user as per IEC 62271-200:2012.



CONCLUSIONS



On-line PD Testing

- Provides good data.
- Quick compared to off-line PD testing.
- Test under normal working conditions.
- Allows continuous monitoring.
- Does not require any HV power supply.

Off-line PD Testing

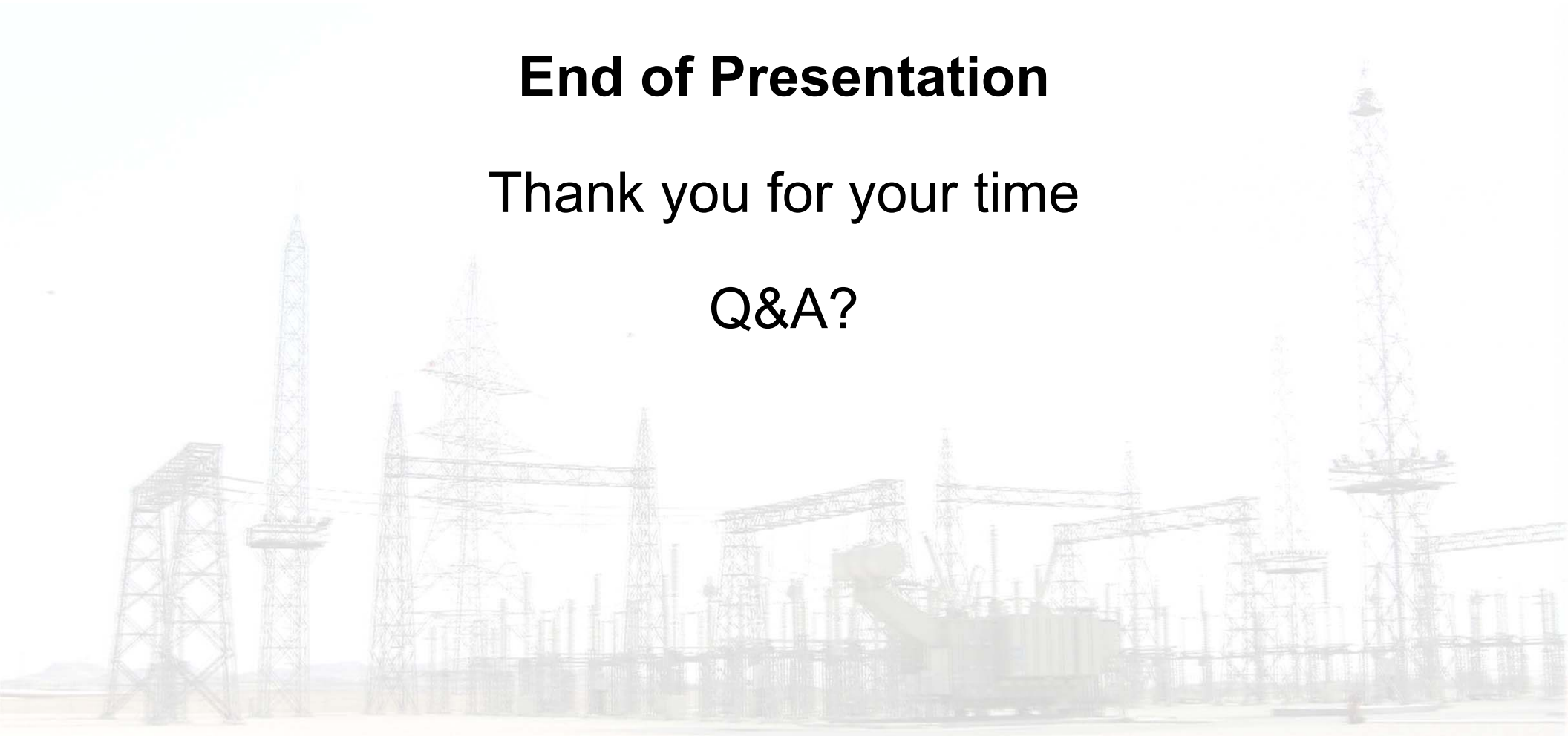
- Useful for factory and commissioning tests.
- Allows easy isolation of plant under test.
- Offers better sensitivity than on-line PD testing.
- Has a longer history.
- Allows testing at elevated voltages.



End of Presentation

Thank you for your time

Q&A?



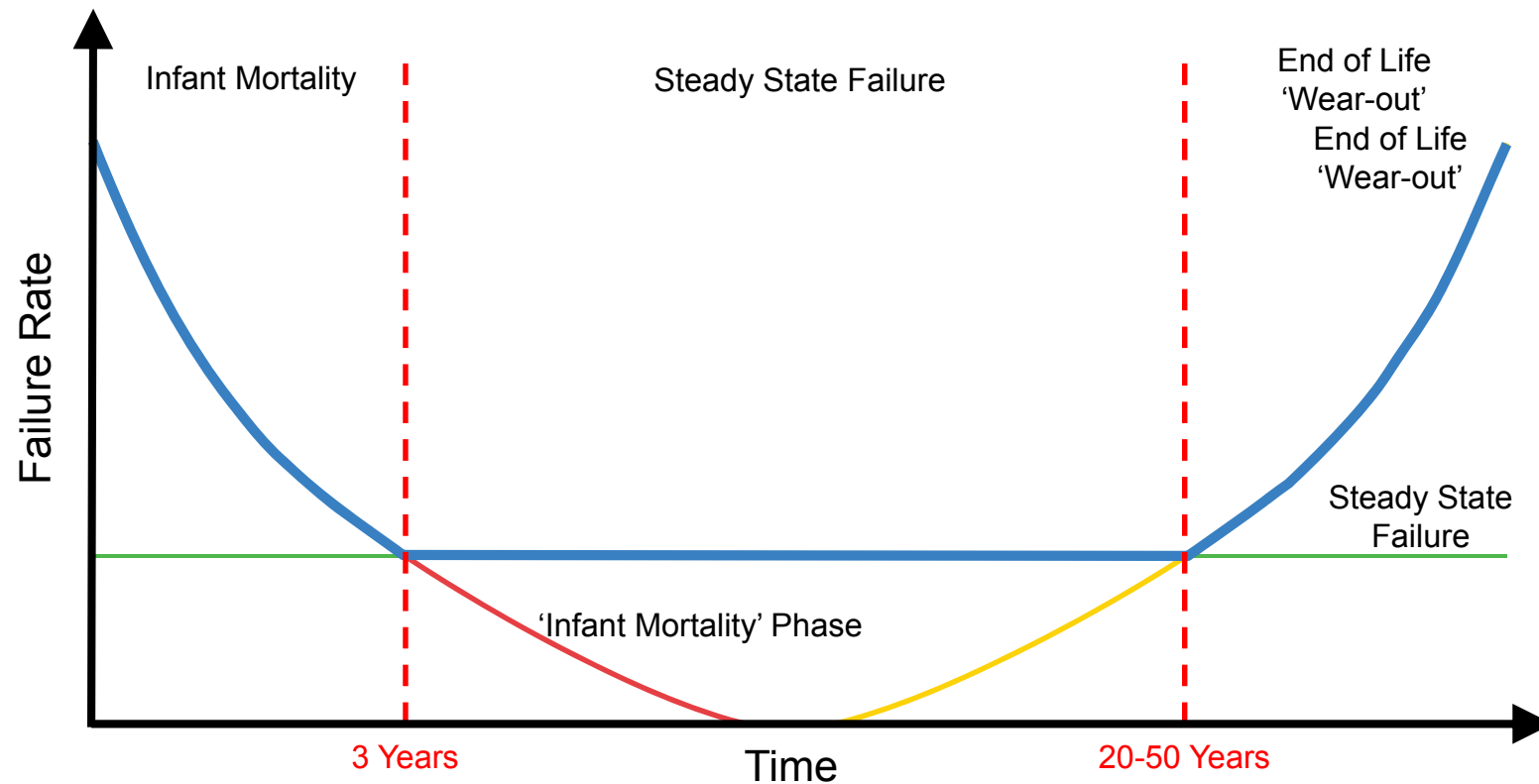


On-line PD Testing & Diagnostics for MV and HV Equipment – Case Studies

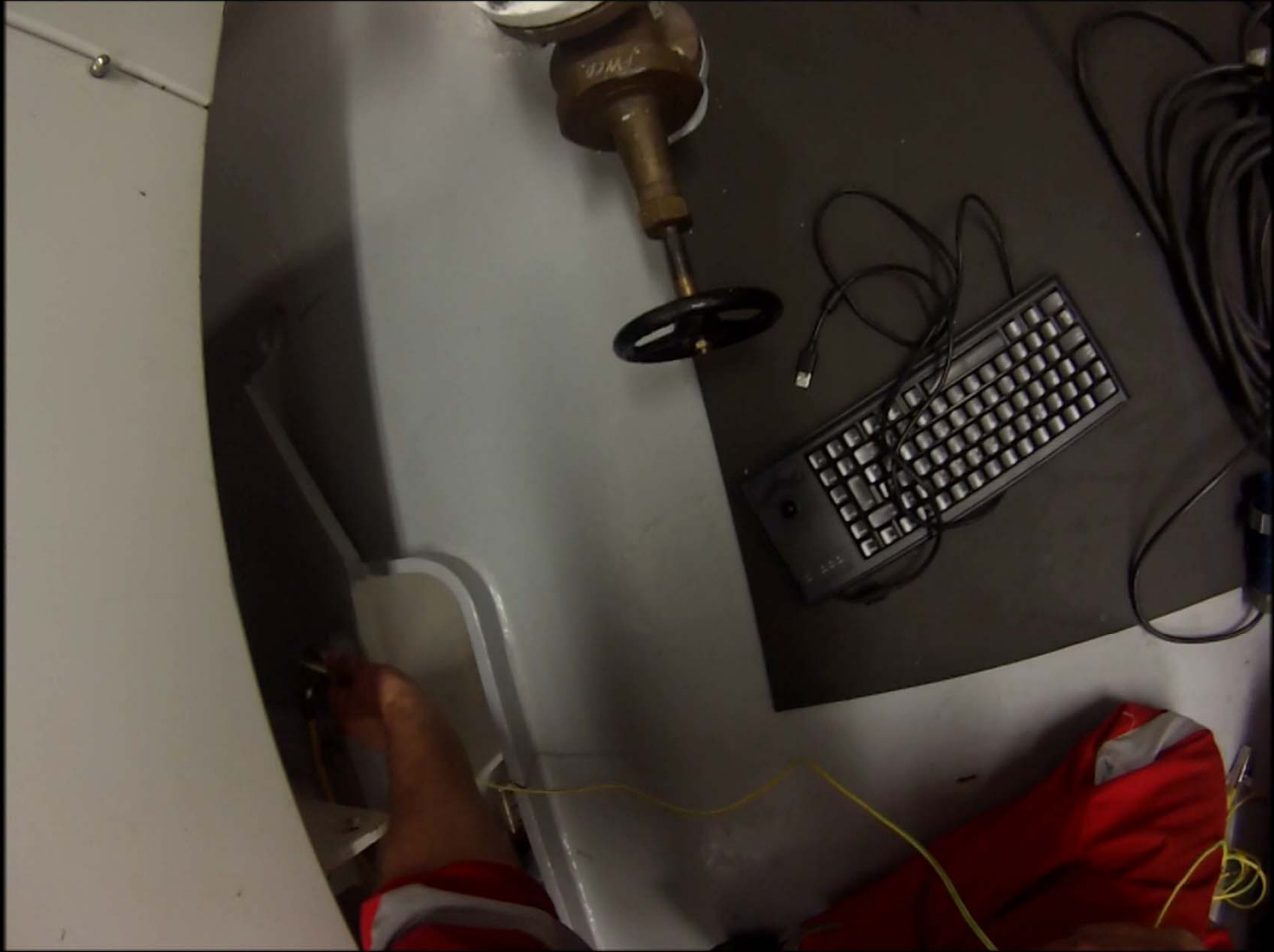


CONTENTS

- Reliability centred maintenance
- Application-specific examples of OLPD testing
- Insulation condition monitoring strategies



- **Infant Mortality Phase:** the initial 'bedding in' period
- **Steady State Failure Phase:** the 'normal' operating lifetime up to the 'Design Life' of the asset
- **End of Life 'Wear-out':** up to the manufacturer's recommended replacement time of the asset





**CASE STUDY 1: OLPD TESTING OF 6.6 KV
DIESEL GENERATORS ON CRUISE LINER**



Case Study: League Table of OLPD Test Results

Vessel	Generator	PD Level 1 st Test	PD Level 2 nd Test	PD Level 3 rd Test	PD Level 4 th Test
Vessel 1	1	-	18,412	-	5,239
	2	17,416	-	-	4,259
	3	15,854	-	-	7,866
	4	29,248	21,637	5,800	9,466
Vessel 2	1	2,162	5,891	7,340	
	2	16,696	2,094	1,474	
	3	-	520	3,790	
	4	12,986	4,557	6,644	
Vessel 3	1	1,969			
	2	3,470			
	3	3,833			
	4	2,251			
	5	5,001			
Vessel 4	1	439			
	2	542			
	3	1,610			
	4	2,643			
	5	510			

- White oxide deposits at the end windings of the stator: a by-product of surface discharge activity
- The problem caused by a coolant leak.
- Recommendations: clean the end windings, fix the coolant leak and re-seal access hatches.



Vessel	Generator	July 2008	August 2008	November 2008	August 2009
Vessel 1	1	-	18,412 pC	-	5,239 pC
	2	17,416 pC	-	-	4,259 pC
	3	15,854 pC	-	-	7,866 pC
	4	29,248 pC	21,637 pC	5,800 pC	9,466 pC
Vessel 2	1	2,162 pC	-	5,981 pC	7,340 pC
	2	16,696 pC	-	2,094 pC	1,474 pC
	3	-	-	520 pC	3,790 pC
	4	12,986 pC	-	4,557 pC	6,644 pC

- Tests performed over 12 months to trend PD data.
- Low-cost, simple maintenance performed on generators in 2008 to remove dust, dirt and oil mist observed.
- PD levels after maintenance reduced from 'Red = Unreliable' to 'Green = OK'.

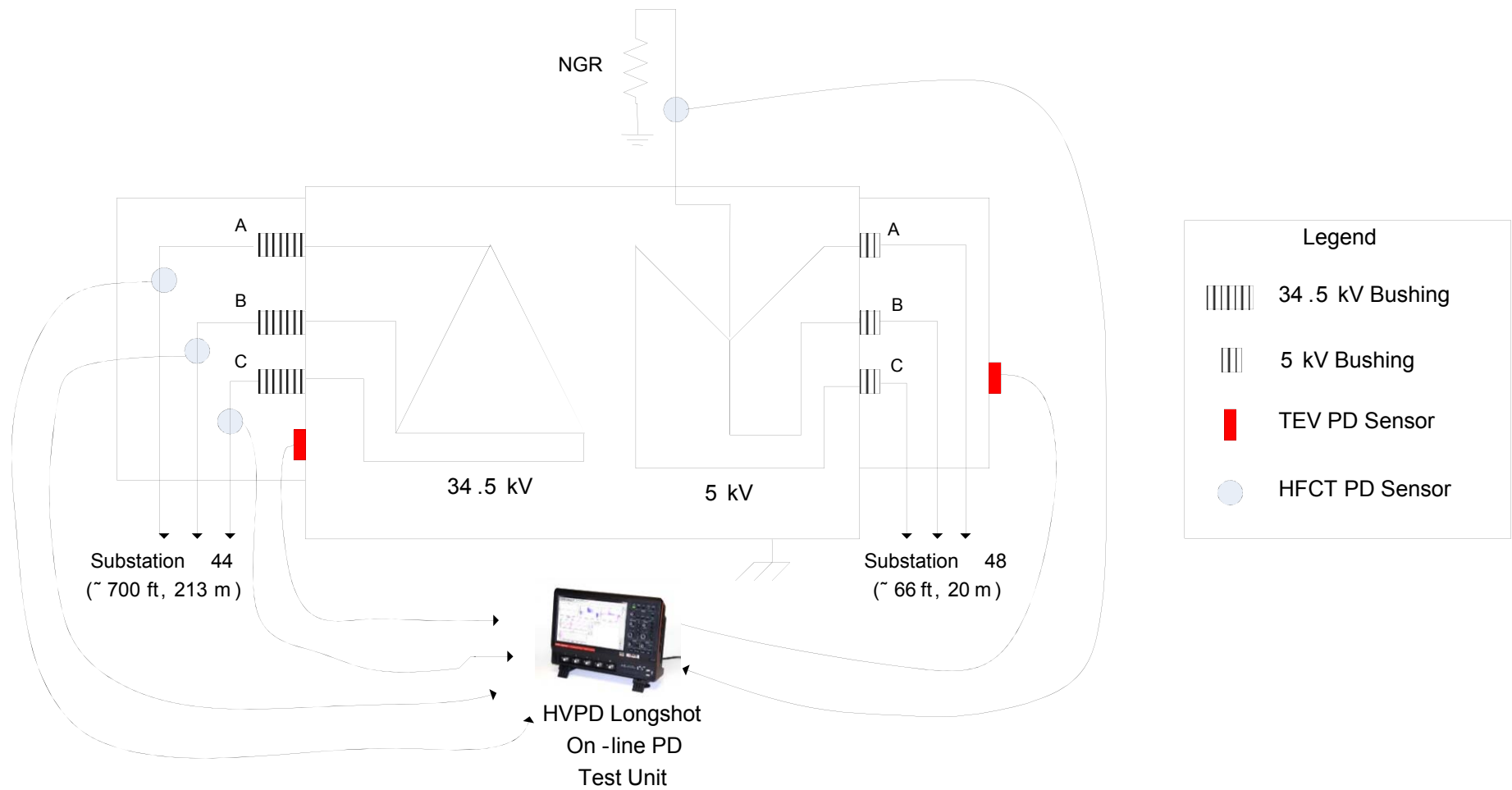


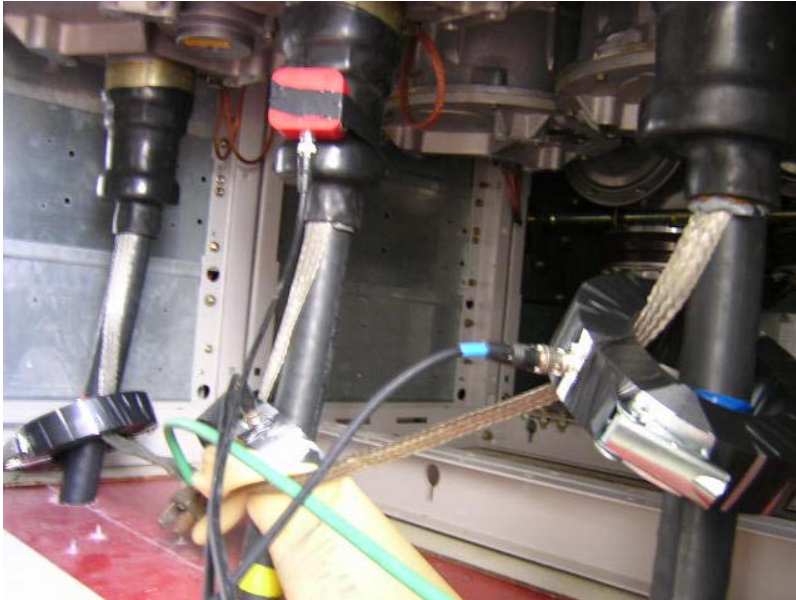
**CASE STUDY 2: IN-SERVICE, ON-LINE PD TESTING
OF 34.5/5 KV 10 MVA TRANSFORMER
(U.S. VIRGIN ISLANDS)**

- Following a failure of a 34.5/5 kV 10 MVA transformer, it was decided to carry out OLPD testing on the 'sister' transformer.
- Tests were carried out on-line, measurements made at both transformer and 34.5 kV Substation – takes into account possible radiation of PD signals from other items of plant (i.e. connecting cables & switchgear).







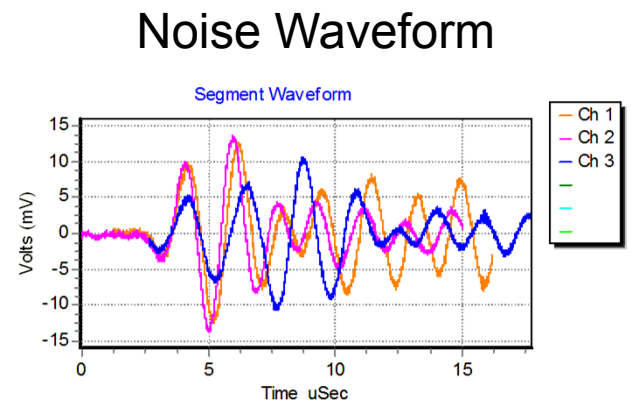
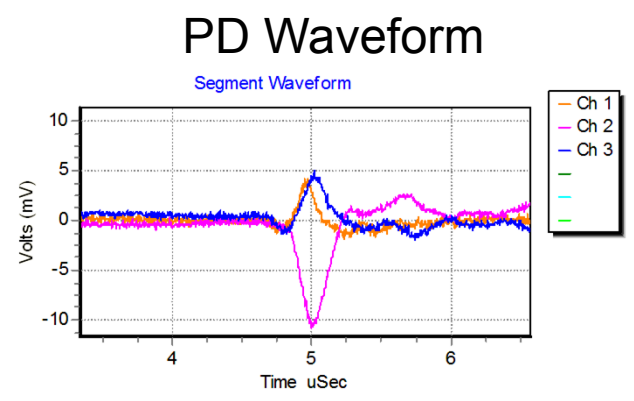
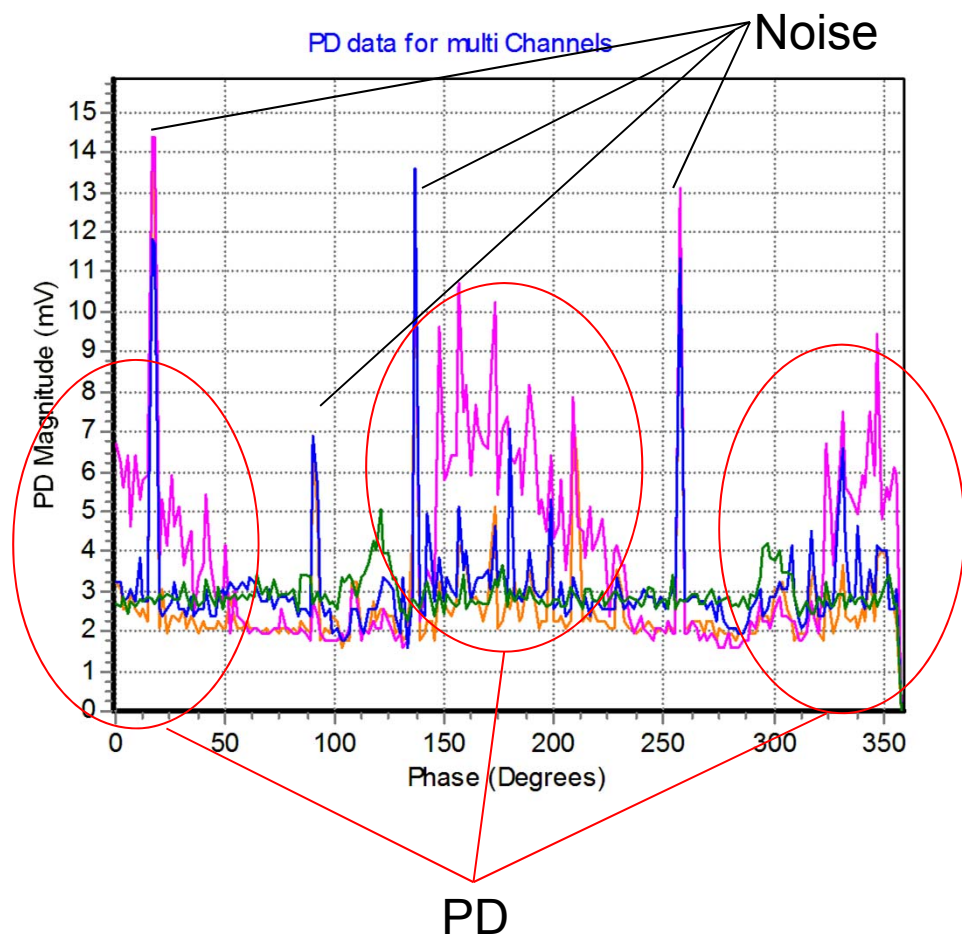


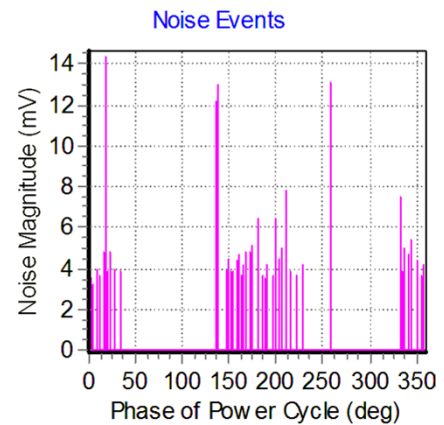
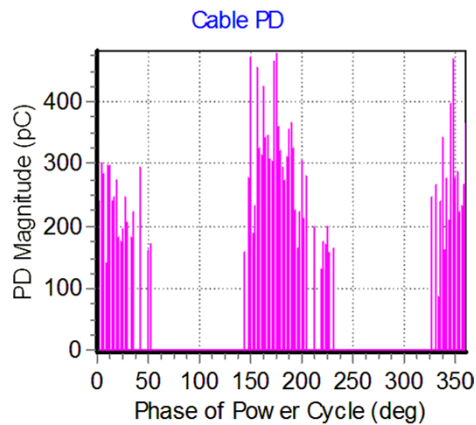
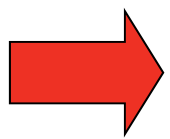
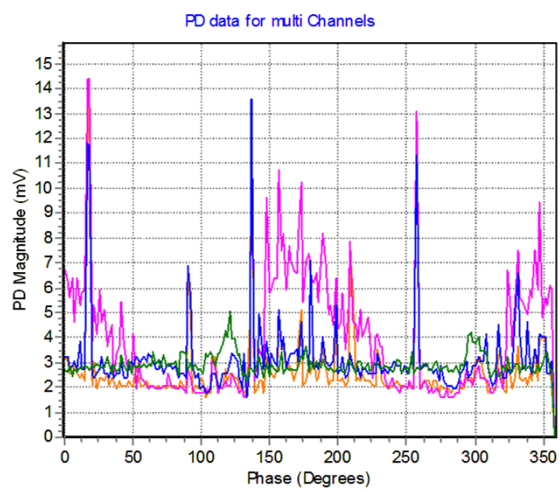
Sensor Connections at Substation End



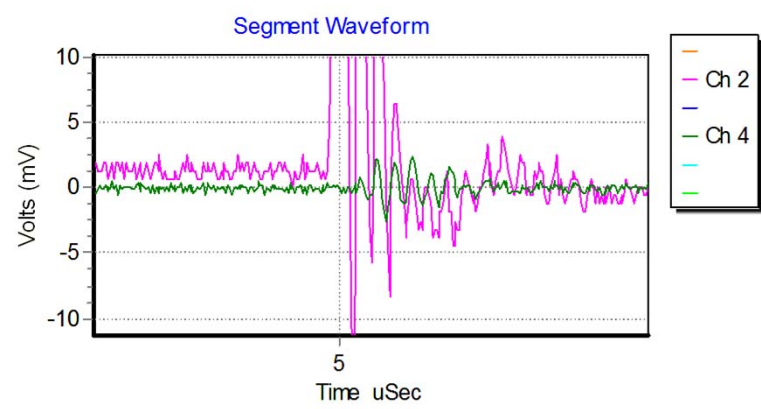
Sensor Connections at Transformer

- PD activity was found on the circuit and isolated to the transformer side of the cable.
- Further tests at the transformer revealed the likely source of the PD was in the *Phase B* of the 34.5 kV cable termination, transformer bushing or end winding.
- To isolate the PD source to either the cable or transformer components, the 34.5 kV cables on phases A, B and C were disconnected from the transformer and tested under working voltage supplied from the substation.
- No PD was detected on this test and thus through process of elimination it was concluded that the PD pulses originate from the transformer.

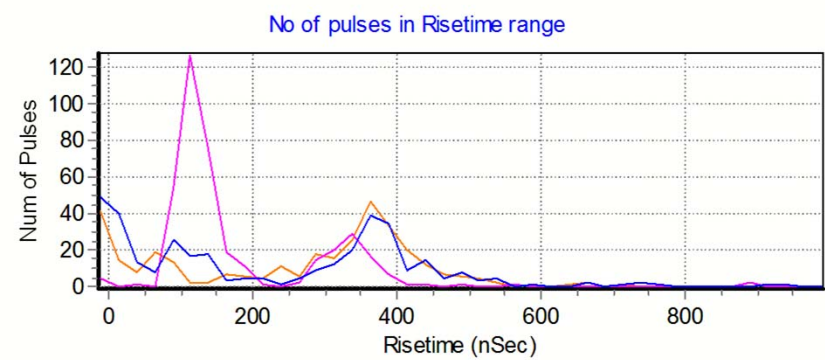
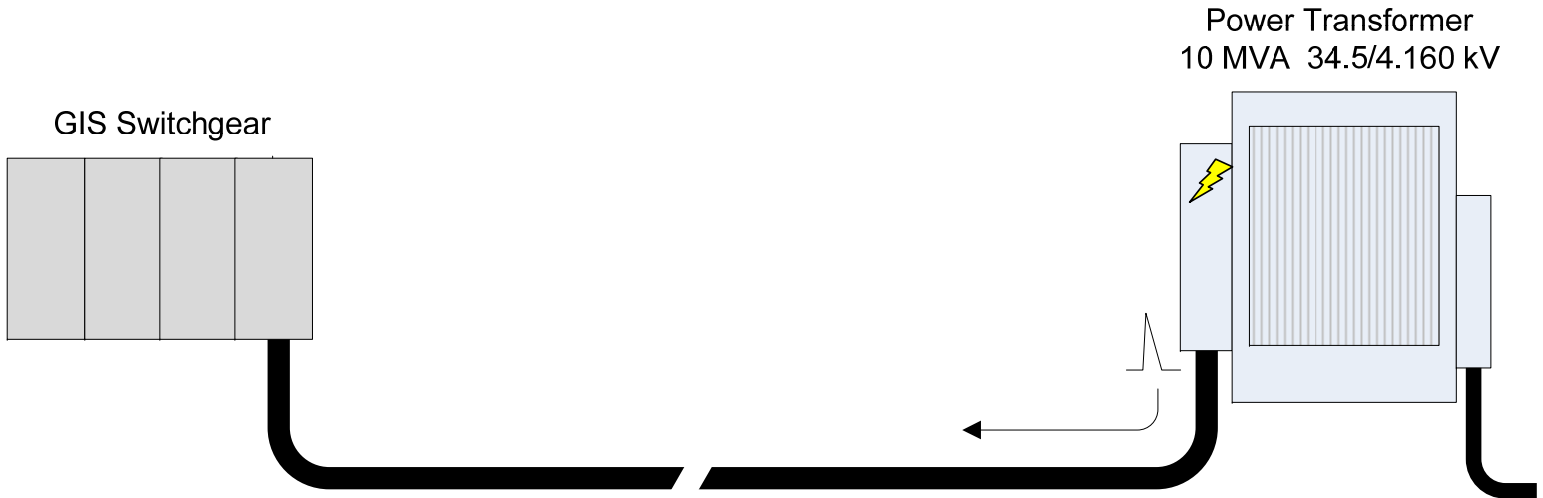




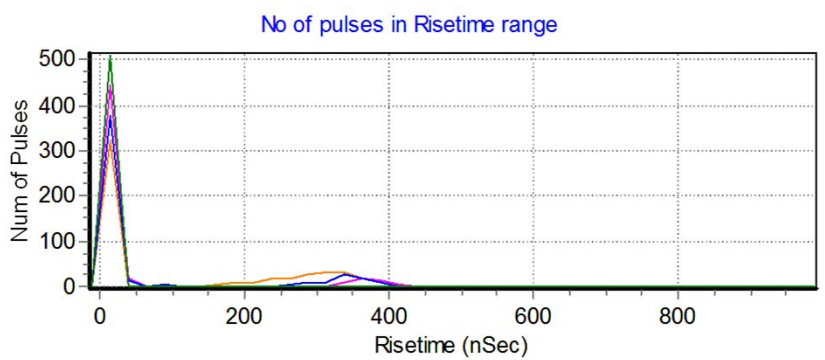
Separated PD and Noise against Power Cycle



Waveform Measured at Transformer HFCT B Phase with HFCT on LV Neutral

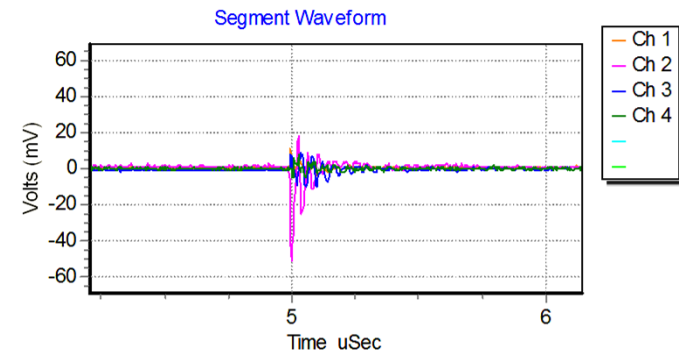
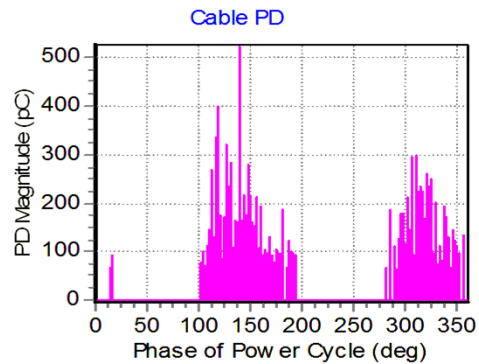


Substation End

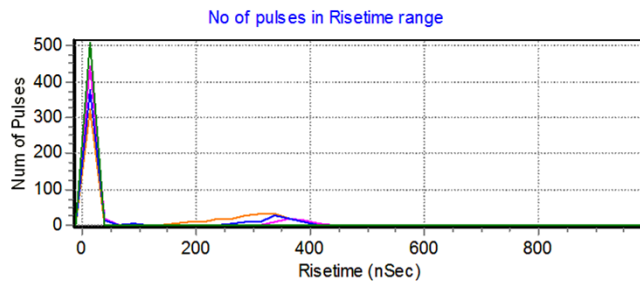


Transformer End

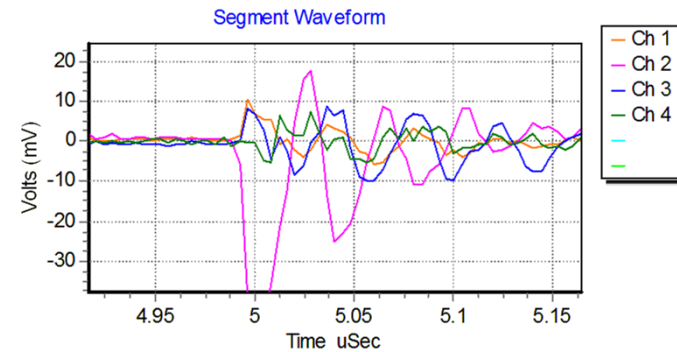
B Phase PD Data from Online Test (Purple Colour)



PD Across 60Hz Power Cycle



PD Waveform Shape (expanded trace below)



Pulse Risetime Graph

- The peak levels of PD detected were 500 pC which is a reasonably moderate level for MV cable accessories and transformer bushings.
- The PD detected was not thought to be an imminent threat but should have definitely been regularly monitored/tested.
- The presence of PD, even at relatively moderate levels, does make the risk of failure higher than that on a discharge free component.
- Regular on-line testing and monitoring of PD activity was recommended to ensure the PD in Phase B does not escalate to an unacceptable level.

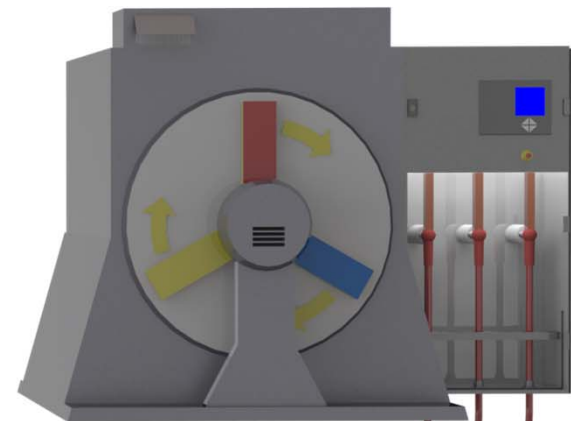


**CASE STUDY 3: OLPD TESTING OF 6.6 KV
MOTORS AT GAS POWER STATION (UK)**

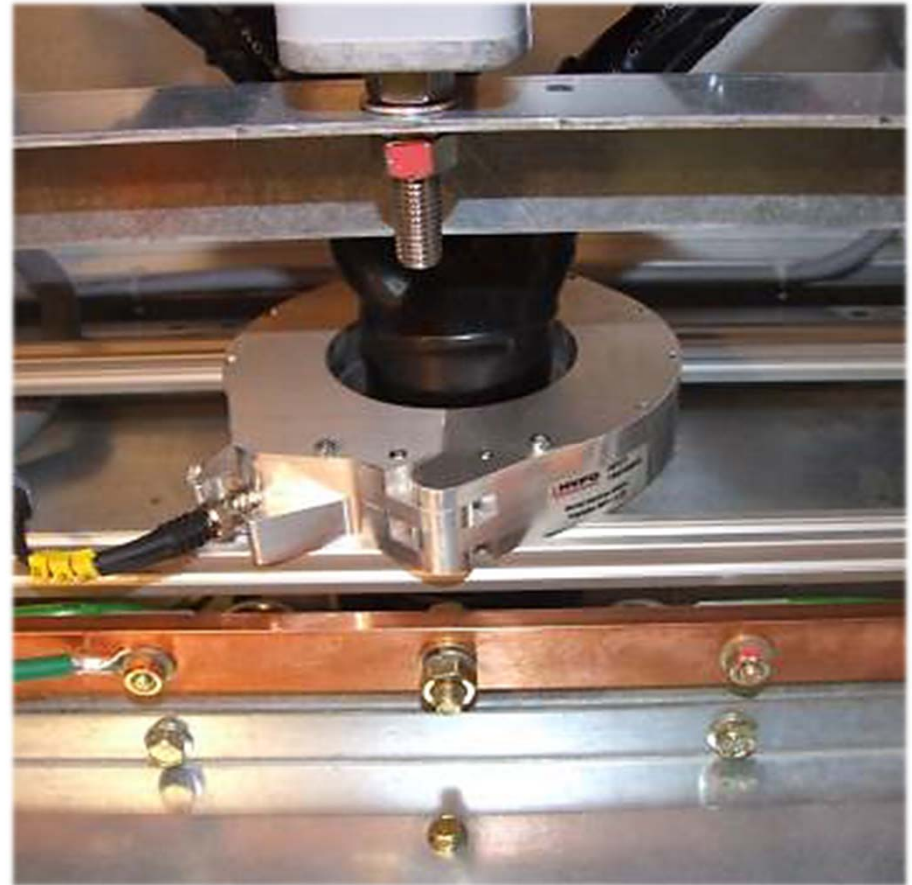
HFCT Sensors located at
HV Switchboard Cable End



Rotating HV Machine
End



Range:
Up to 1 km for PVC
Up to 2 km for XLPE



Motor Ref	PD Level [pC]	PD Activity [nC/Cycle]
Manufacturer A – Motor 1	12,152	95
Manufacturer A – Motor 2	3,123	12
Manufacturer A – Motor 3	3,165	4
Manufacturer B – Motor 1	52,589	296
Manufacturer B – Motor 2	33,135	370
Manufacturer B – Motor 3	68,071	85

Motor	U Phase		V Phase		W Phase		All Phases	
	PD (IEC) Magnitude		PD (IEC) Magnitude		PD (IEC) Magnitude		PD (IEC) Magnitude	
	2010	2011	2010	2011	2010	2011	2010	2011
Motor 1	10,530	30,260	12,870	24,960	7,865	4,846	17,180	44,040
Motor 2	14,920	30,620	17,730	27,070	15,640	22,100	26,390	42,520
Motor 3	15,140	30,890	16,920	31,040	16,530	24,410	26,780	44,370

All off-line PD measurements showed an increasing trend from the 2010 tests to the 2011 tests with an average increase in PD levels across all 3 motors of around 100% i.e. the PD levels **had doubled over the 12 months between these tests.**

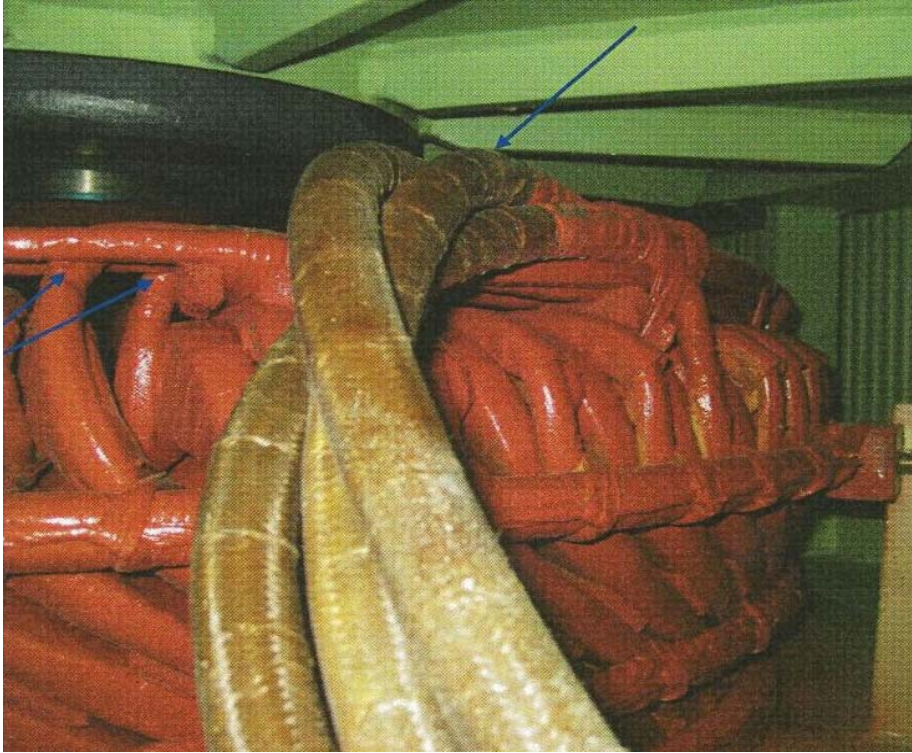


Image of Neutral Terminal Box. The Glass Cover (arrowed) was removed to inspect the windings



Image of winding connections. Neutral Cables and internal connections not spaced apart (arrowed)

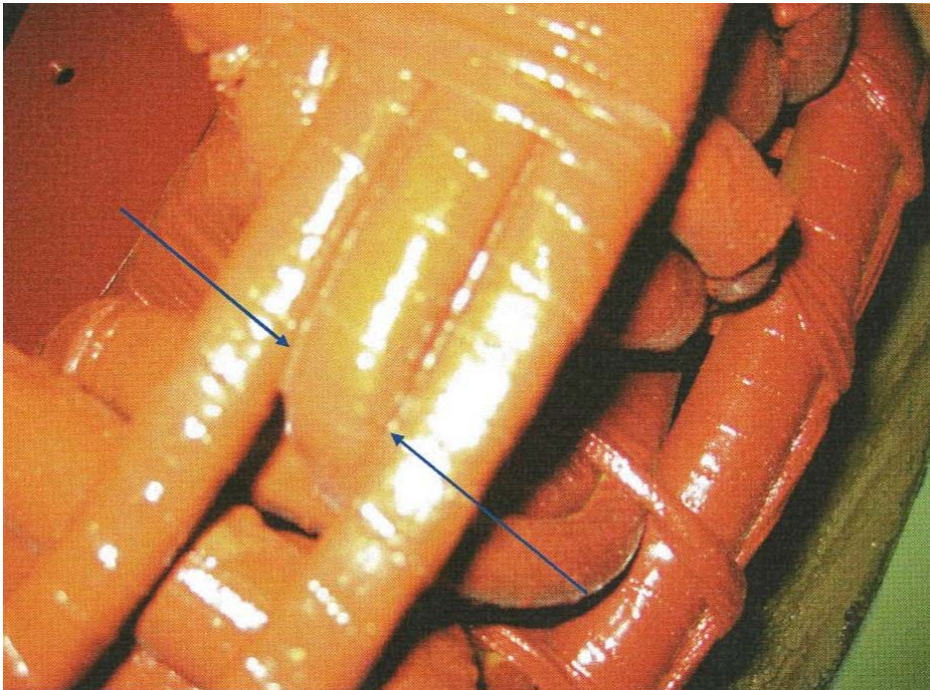
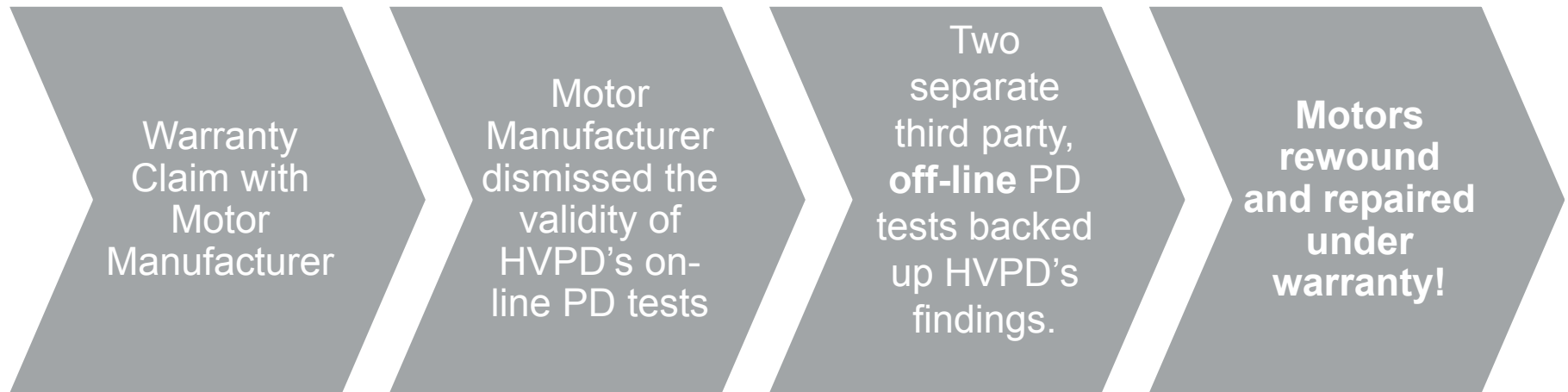


Image of connections not adequately spaced (arrowed) = design issue




Image of coil – coil connections touching a neutral cable (arrowed) = design issue



Customer's feedback:

'Thanks for your support throughout the whole process, your equipment and advice has played a big role in a fairly complicated warranty claim that enabled us to successfully identify and rectify a defect, which with PD was always going to be a difficult one to secure.'

A grayscale photograph of a construction site. In the foreground, a trench has been dug into the ground, with several large, dark, cylindrical cables laid out along its length. Four men wearing hard hats and work clothes are standing in the trench, looking down at the cables. In the background, there is a large, multi-story building under construction, with a metal framework visible. A chain-link fence runs along the left side of the site. The overall scene is a busy industrial construction environment.

**CASE STUDY 4: OLPD TESTING AND MAPPING
OF 34.5 KV XLPE CABLES FOR A PROCESS
INDUSTRY CLIENT (SAUDI ARABIA)**

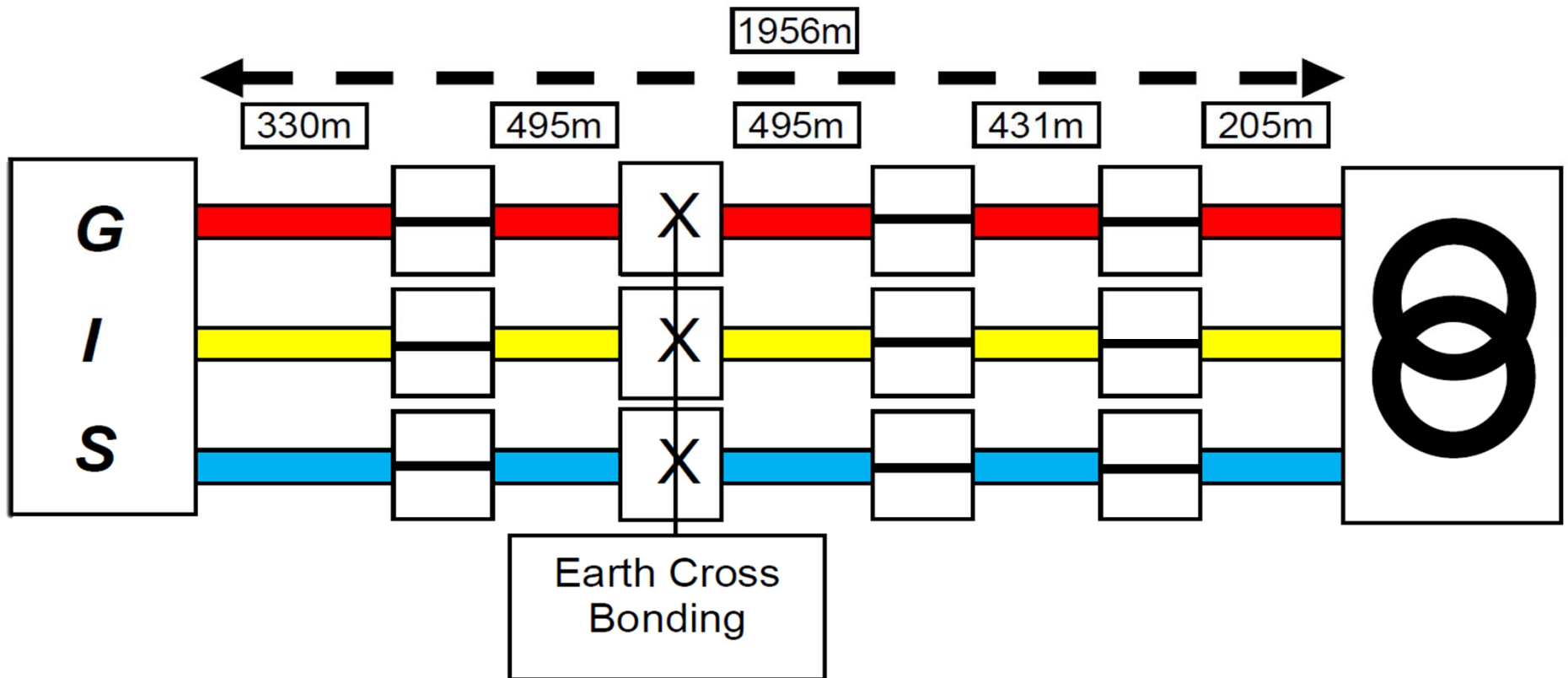


- OLPD tests on a number of cable circuits **where recent cable joint failures had occurred.**
- Four cable circuits that were known to have been subjected to heavy circulating currents in the earth screen & armour (in excess of 80 Amps) which had led to **catastrophic in-service failures.**
- The previously failed joints showed evidence of tracking.

- OLPD tests on a number of cable circuits where recent cable joint failures had occurred.
- Four cable circuits that were known to have been subjected to heavy circulating currents in the earth screen & armour (in excess of 80 Amps) which had led to catastrophic in-service failures.
- The previously failed joints showed evidence of tracking.



The 1.9 km long, 34 kV XLPE cable circuit had 5 jointed sections with only one cross-bond point.





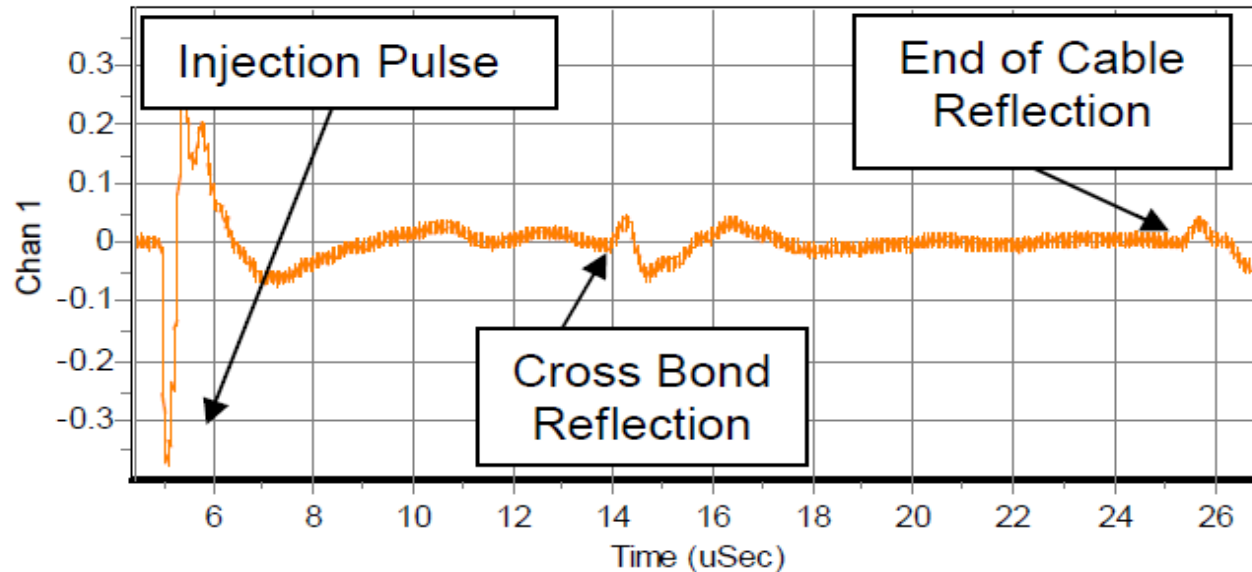
The HVPD PDSurveyor™ was used to detect any Local PD in the cable terminations / joints and switchgear panels.



The HVPD Longshot™ unit was used to test and locate the discharging joints.

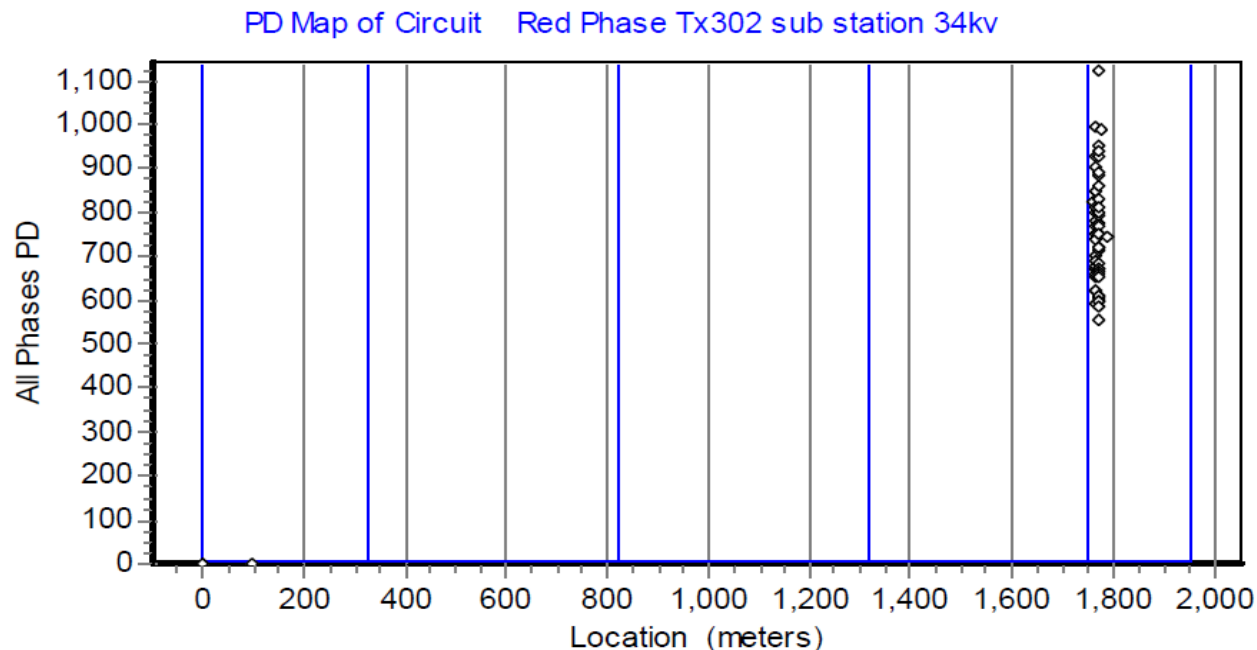




On-line TDR Using HVPD Longshot PD Test System

- The measured **Cable Return Time** for the pulse injected at the switchgear to travel to the far end of the seawater feeders and back was **20.4 μ sec**.
- Given that the seawater feeder cable is 1956 metres in length, this gives a **return speed** for the 34.5 kV XLPE cable of **95.9 m/ μ sec**.

- PMap© software was used to create a map of the 1956 m cable.
- The source of PD activity was located within the Red Phase cable of seawater pump Tx302 at 1770 metres out from the 34.5 kV main substation (or 185 metres out from the Seawater Pump Transformers).
- This corresponds with the location of Joint No.3 on this cable as shown below.





The cable joint was replaced, re-tested and found to be discharge-free.

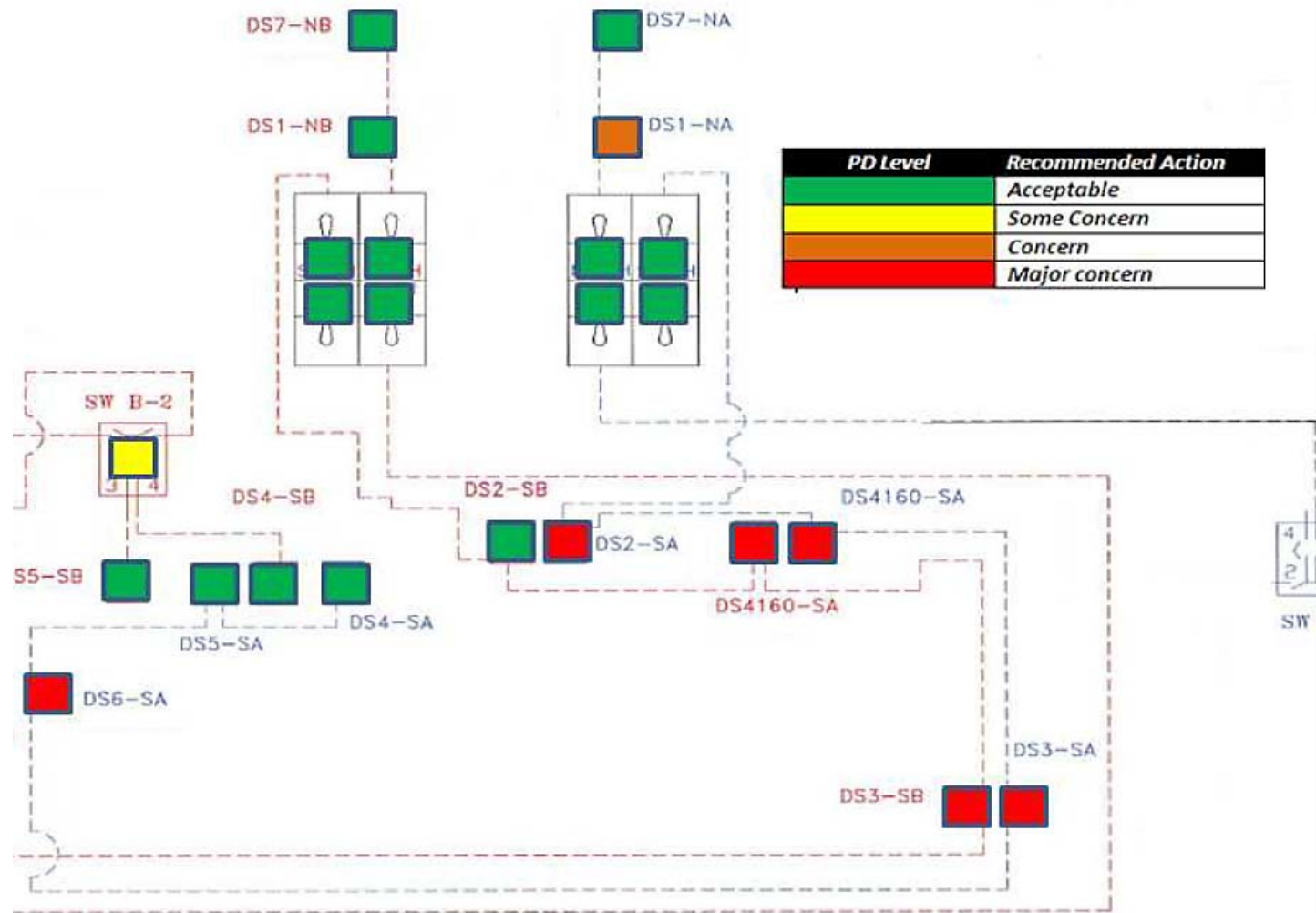
A large, grey, industrial electrical cabinet, likely a Siemens product, is shown in an outdoor setting. The cabinet has multiple doors with handles and ventilation grilles. The word 'SIEMENS' is visible on one of the doors. The cabinet is mounted on a concrete base. In the background, there is a fence and a car.

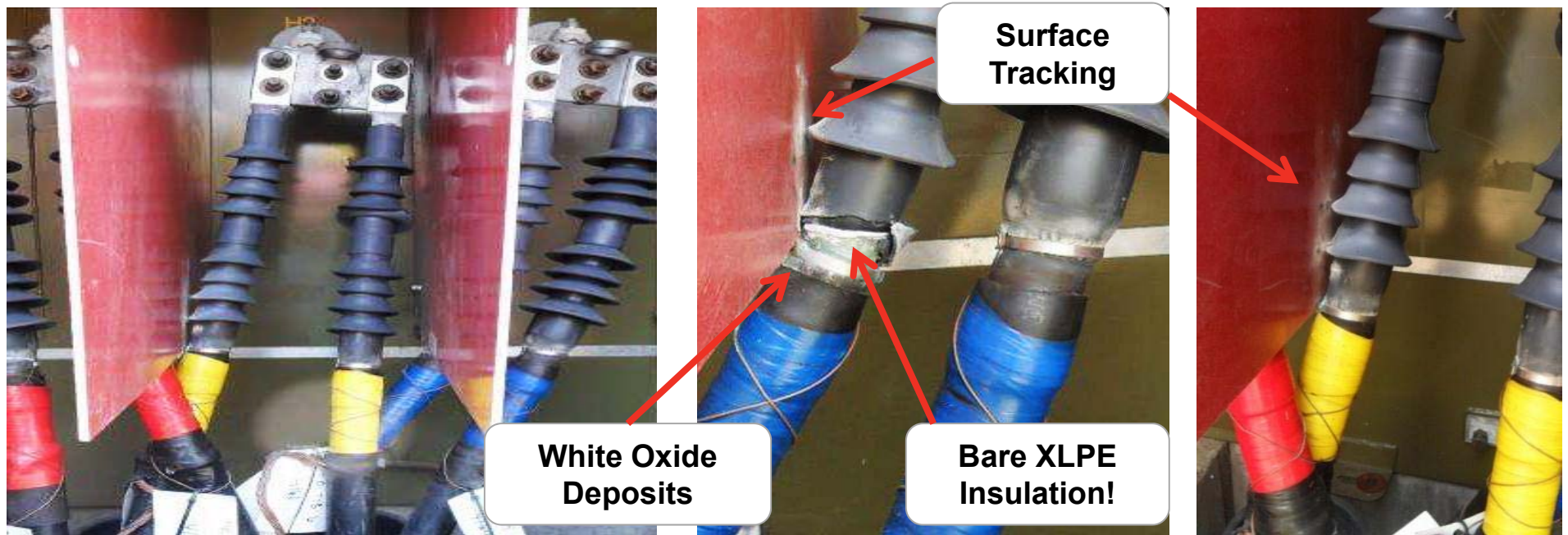
**CASE STUDY 5: ON-LINE PD TESTING OF 34.5
KV INDUSTRIAL CABLE NETWORK (USA)**

- OLPD tests were conducted within the 34.5 kV XLPE cable terminations at the padmount transformers in follow up to recent in-service failures of cable terminations.
- 21 cable circuit terminations were tested with 42 points of attachment (POA) with the PDSurveyor™, HVPD Longshot™, and temporarily installed HFCT sensors.



- Considerable cross-coupling of the PD signals at each padmount.
- PD signals propagate far into the cable network from source.
- Four sources of this type of activity located.





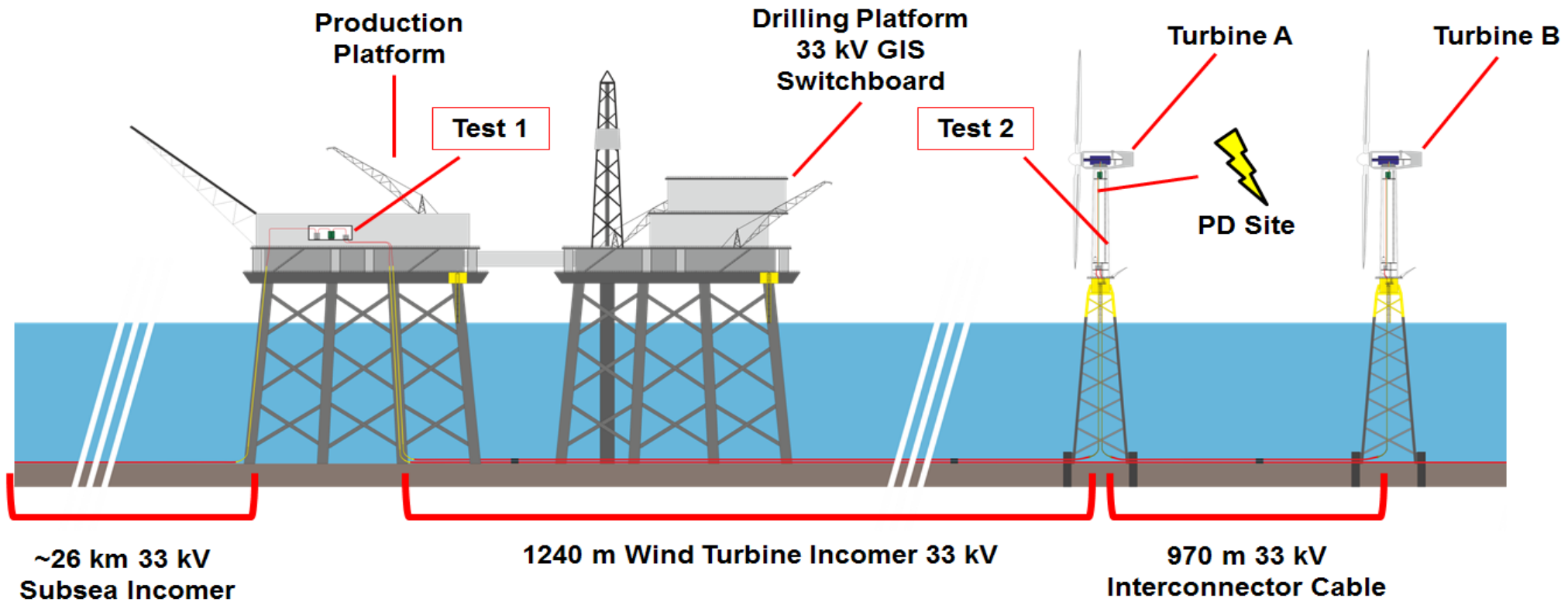
- **Poor workmanship** was the main contributing factor to the surface PD activity detected.
- **Signs of PD activity** on the cable terminations
- The rubber stress cone termination had been completely eroded.

- Re-termination of the cables into the six 'RED PD Level' padmounts.
- Further OLPD tests showed no PD activity and confirmed the rework had been effective.
- The customer was advised that regular, periodic OLPD 'screening' tests should be carried out.





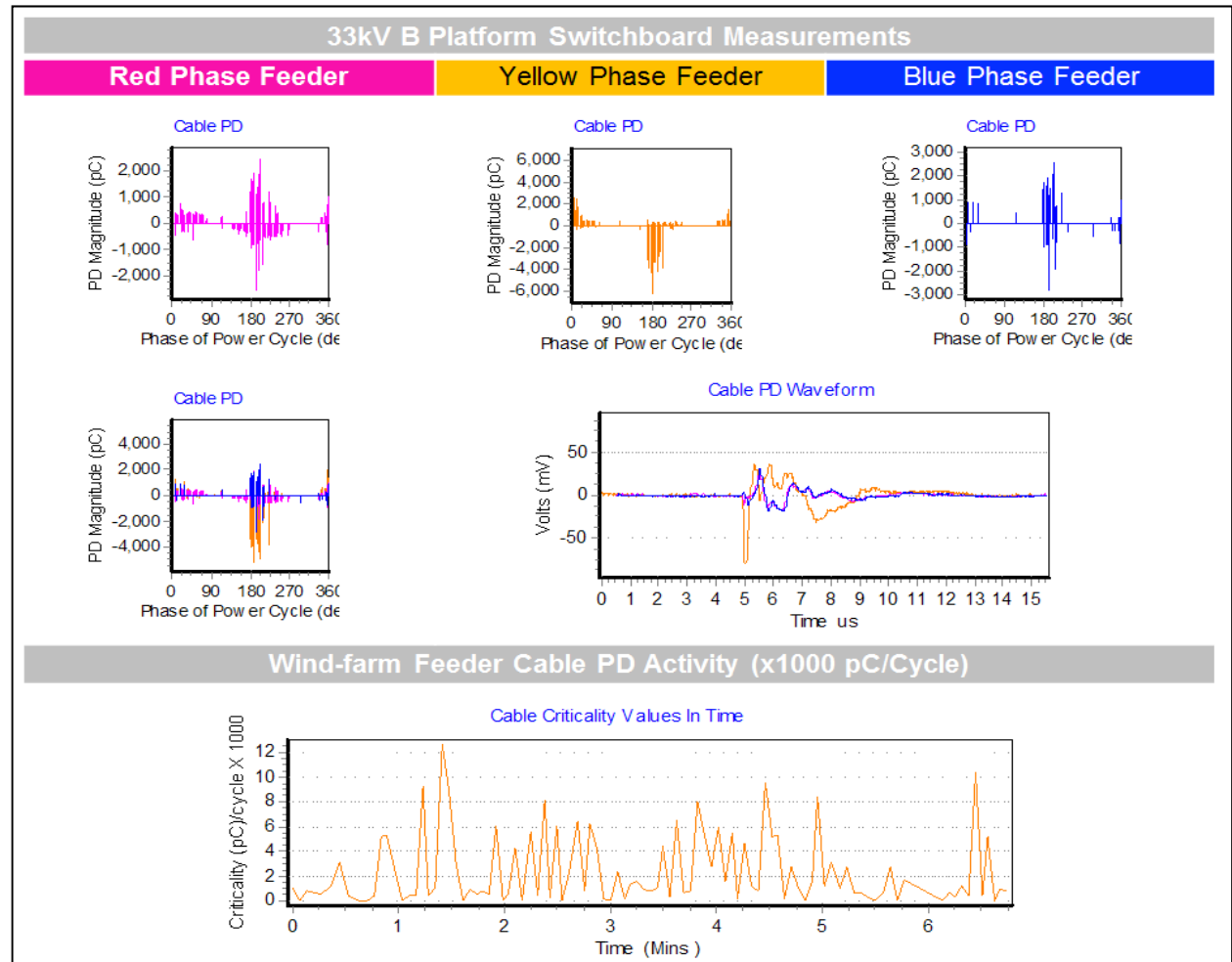
**CASE STUDY 6: OLPD TESTING AND LOCATION ON
OFFSHORE WIND TURBINE TO OIL & GAS PLATFORM
33 KV CABLE FEEDER**



- Two deep-water wind turbines supply power exclusively to an oil production platform 2km away.
- Two on-line PD tests were performed to assess the condition of the turbine feeder cables.

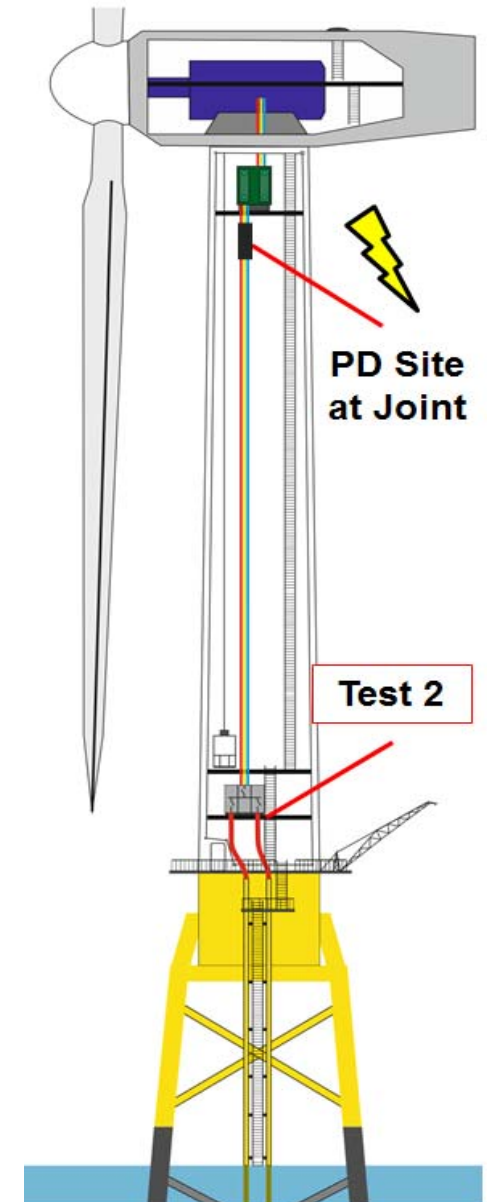
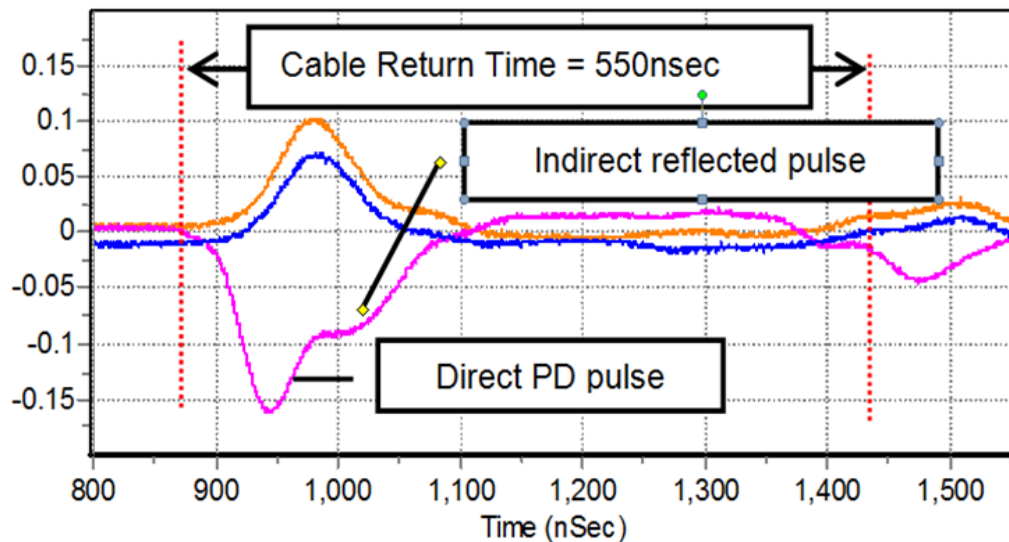


- **PD on Turbine A Feeder was detected** and was considered to be remote source based on pulse properties.
- Analysis predicted the **location to be near the far end of the Turbine A feeder cable**. Mapping recommended.

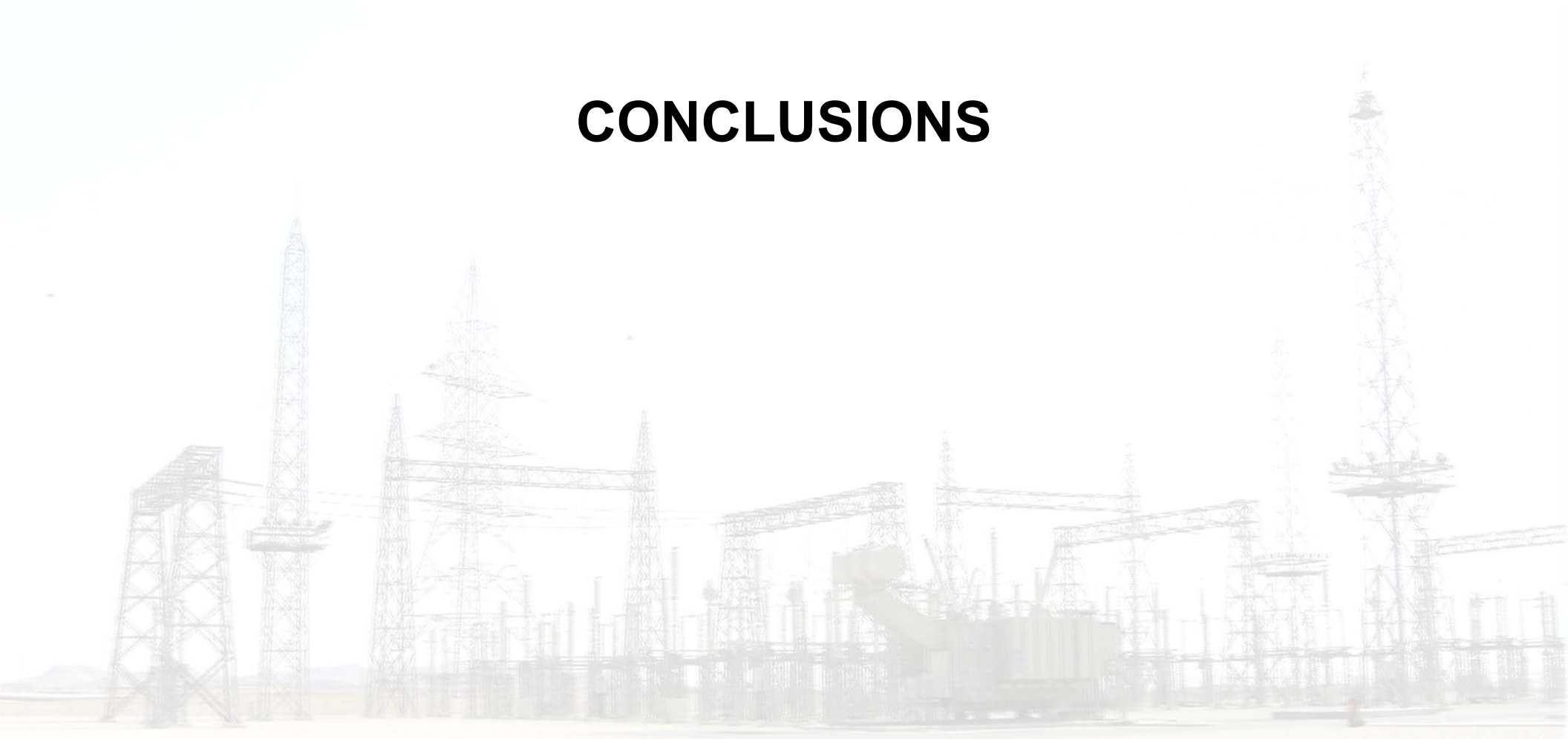




- High PD magnitudes in excess of 6,000 pC, with average levels of 1,871 pC detected on Yellow phase.
- Test identified the PD source was the Y ϕ local turbine 33 kV transformer/cable joint.
- Measurement of PD pulses on wind turbine cable feeder show clear direct & indirect reflected pulses.
- Joint location was confirmed at 52 metres from the RMU.



CONCLUSIONS

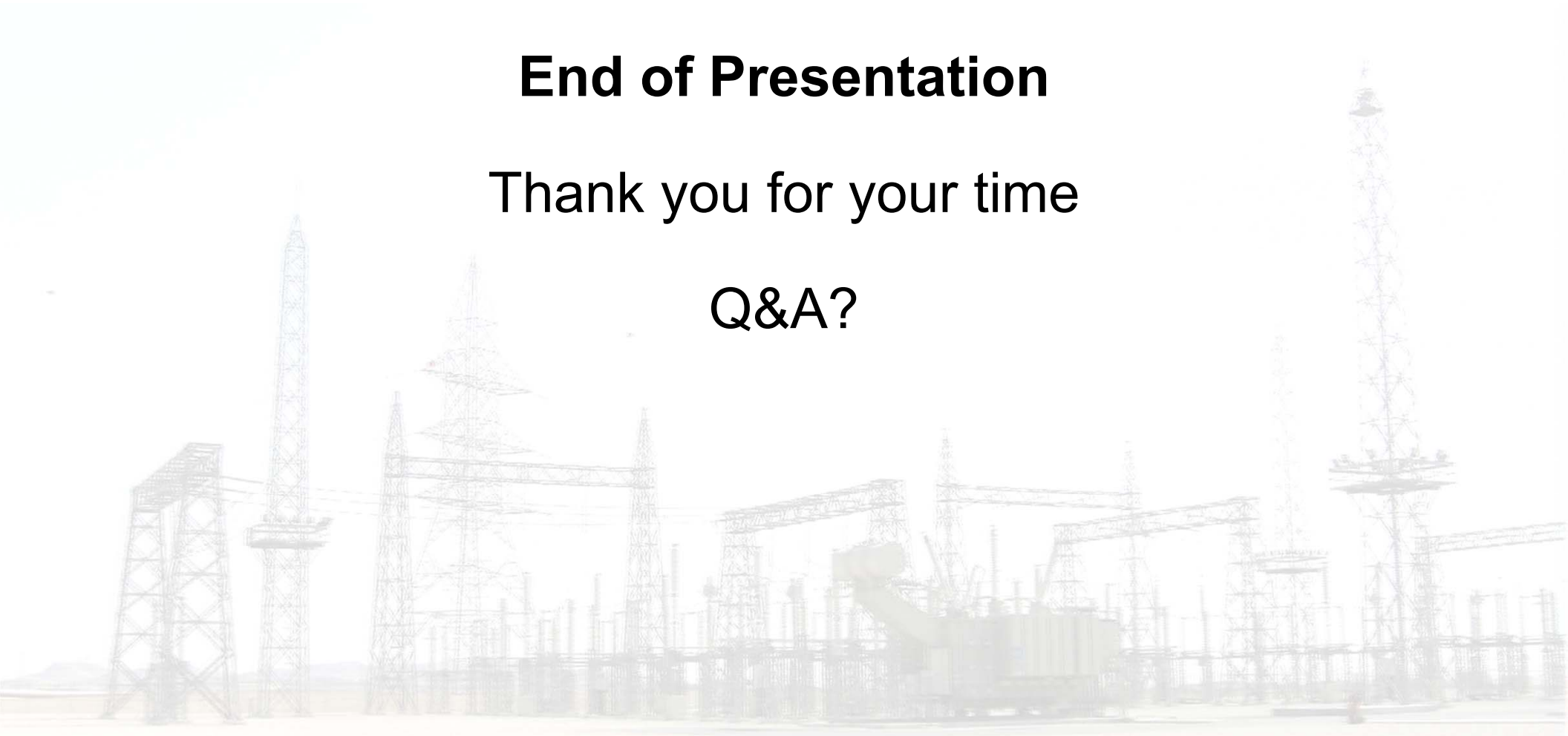


- Insulation Condition Monitoring (CM) using OLPD requires a **continuous evaluation** of the HV insulation's dielectric integrity throughout the service life of the asset.
- **Continuous OLPD monitoring** should be carried out throughout the first 3 years of service - the 'bedding in' period.
- **Test and monitor after any repairs to faults** – to ensure the repair has worked!
- **Continuous OLPD monitoring is recommended throughout the service design life** (of 20–25 years+).

End of Presentation

Thank you for your time

Q&A?





Deployment of OLPD Testing in Asset Management Systems





CONTENTS

- HVPD 4-Phase approach for OLPD monitoring of MV networks
- PD trending
- Plant condition analysis
- OLPD league tables
- Examples of deployment of PD testing in asset management systems



- A complete solution for the OLPD screening, diagnostic testing and extended monitoring.
- Identify, locate and monitor PD activity in the **‘Worst 5%’** of the customer’s network.
- A range of portable and permanent OLPD test and monitoring technology can be applied to achieve this.



The HVPD Integrated OLPD Test and Monitoring Solution For Medium Voltage (MV) Networks (Voltage Range: 3.3–36 kV)

Phase 1

100% of the network

OLPD 'Pre-screening' with Handheld OLPD Surveying Technology

'Look-see' tests, only requiring 10–30 second test per plant item



PDS Air™ with TEV, HFCT and Acoustic Sensors

Phase 2

~20% of the network
(as identified in Phase 1)

Diagnostic OLPD Testing & PD Site Location with Cable Mapping

PD Testing: 5–10 minutes
PD Mapping – 10 minutes to 1 hour



HVPD Longshot™ 4-channel Diagnostic OLPD Spot Tester

Phase 3

~10% of MV plant
(as identified in Phases 1 and 2)

Temporary OLPD Monitoring with Portable OLPD Monitors

Periods from 1 day up to 3 months



HVPD Multi™ Portable & HVPD Mini™ Portable OLPD Monitors

Phase 4

~1–5% of MV Plant
(as identified in Phases 1, 2 and 3)

Continuous OLPD Monitoring with Permanent OLPD Monitors

3 months+



HVPD Multi™ Permanent Monitor (16 to 96 Channels)

12 Month Iterative Process

Our Knowledge is Your Power





- Used for initial, quick screening of large numbers of MV plant items.
- The MV cable/plant can be tested in-service under normal operating conditions, no outage required!
- Easy to read, 7-level, colour-coded PD level indication panel.







- Combines HFCT, TEV and AA sensors to enable OLPD testing of both cables and switchgear.
- A look-see OLPD scan, indicating the plant which requires further diagnostic testing.
- Low cost, lightweight & portable, easy to use.
- Test the insulation condition of the plant in seconds.

**On-Line Partial Discharge
Surveying System**

PD Level Guide:

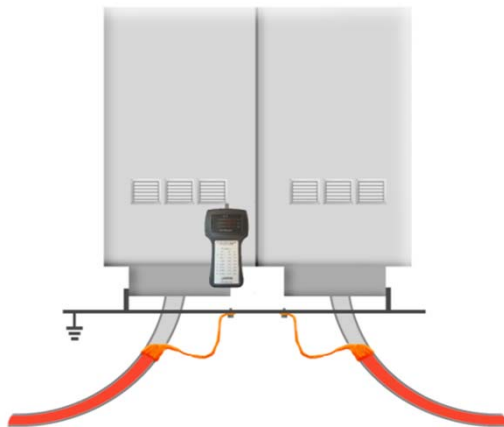
	CT	AA	TEV
●	300 pC	8 dB	15 dB
●	600 pC	12 dB	20 dB
●	1200 pC	15 dB	25 dB
●	3000 pC	19 dB	30 dB
●	7800 pC	22 dB	35 dB
●	20000 pC	26 dB	40 dB
●	30000 pC	30 dB	45 dB

www.hvpd.co.uk

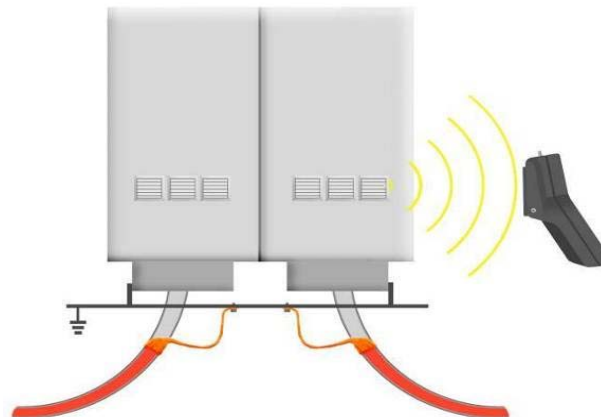
- **LED 1** – Green (Plant OK)
- **LED 2 & 3** – Yellow (Moderate PD – Monitor)
- **LED 4 & 5** – Orange (Moderate To High PD – Investigate Source Of PD)
- **LED 6 & 7** – RED (High PD – Test & Restrict Access)

NB: It should be noted that the PD levels & actions recommended are guideline levels only and are based on HVPD's experience in testing MV Plant

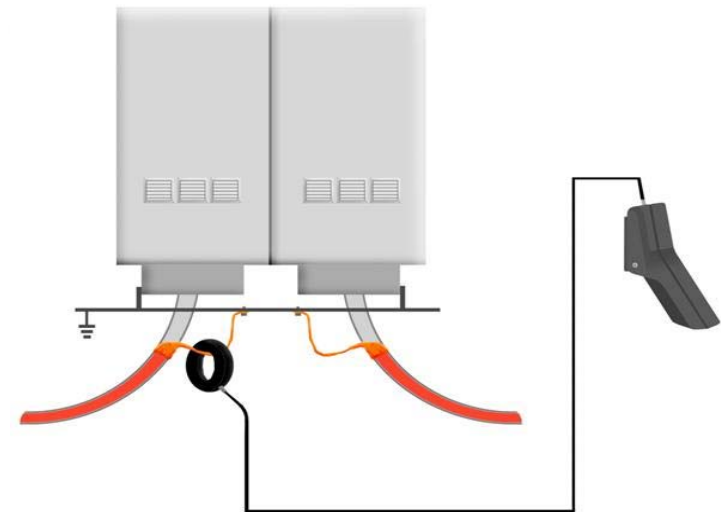
TEV Sensor

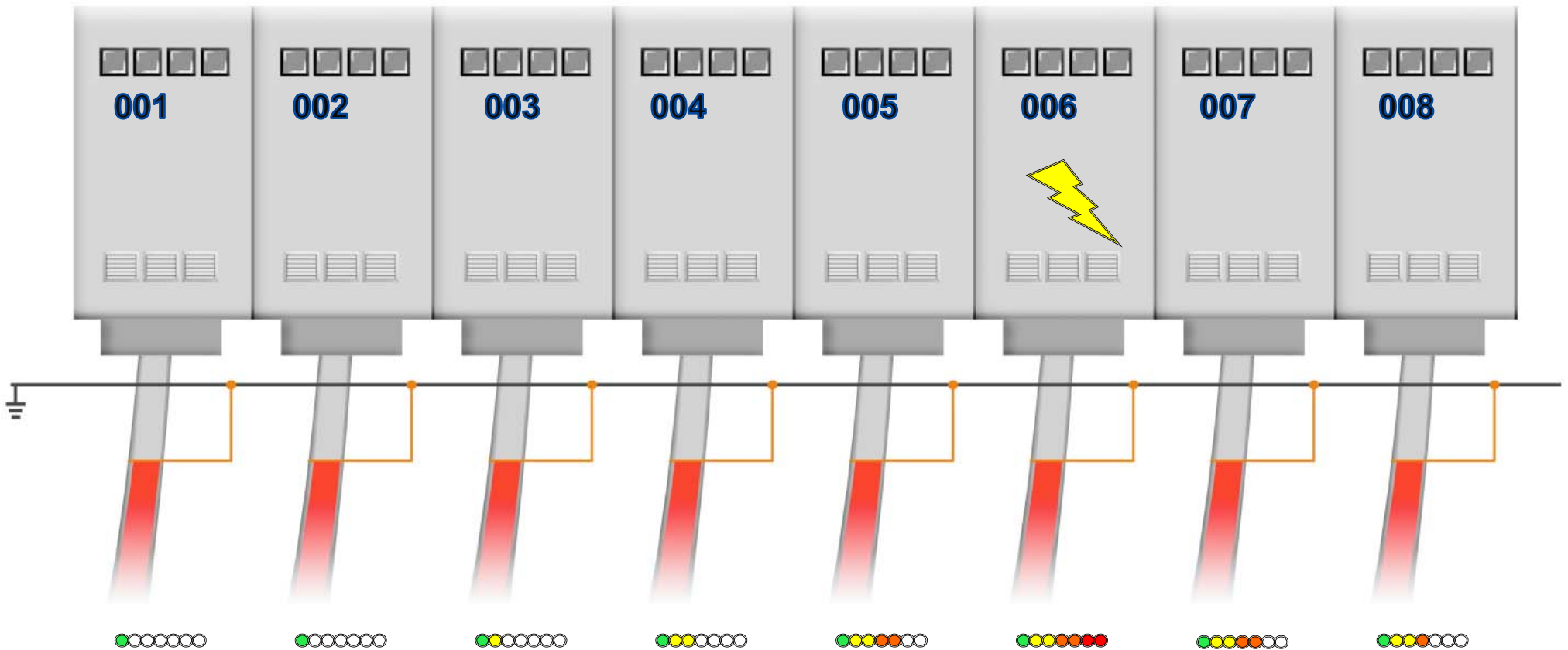


Airborne Acoustic Sensor



HFCT Sensor





**Very High Level Local PD Activity >48 dB (Panel 006)
Further Investigation Recommended**

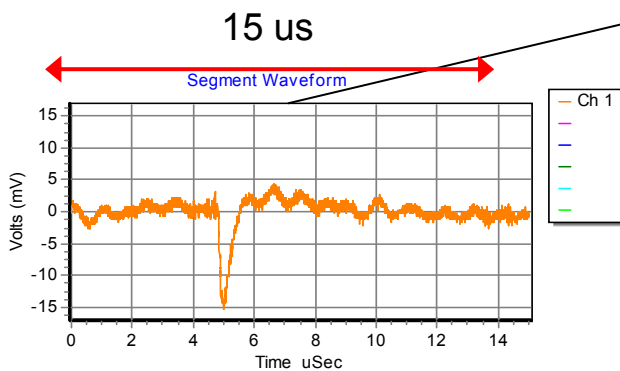
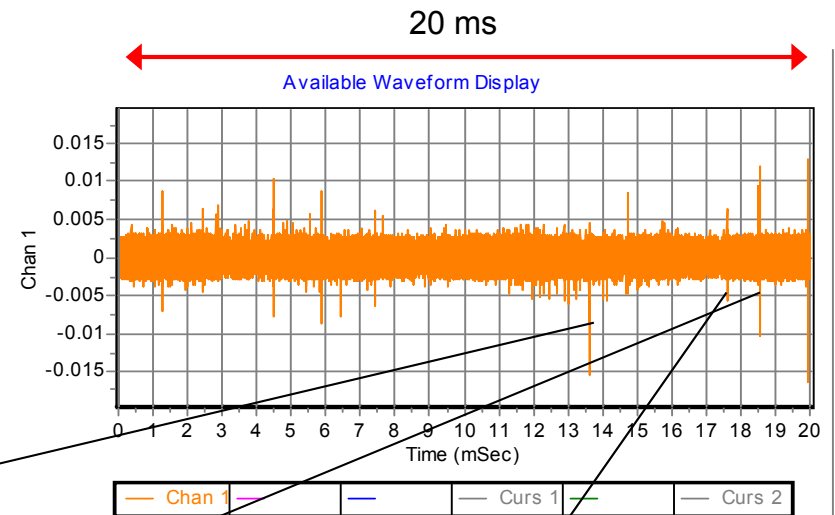


- 4-Channel, synchronous OLPD test unit
- Captures PD activity using very high speed data acquisition capability (100–500 MS/s)
- Diagnostic PDGold© v7 software with unique ‘*Event Recogniser*©’ software modules differentiates between PD activity and any electrical noise and RF interference.
- An automatic, detailed analysis of pulse frequency, waveshape and other signal waveform characteristics.

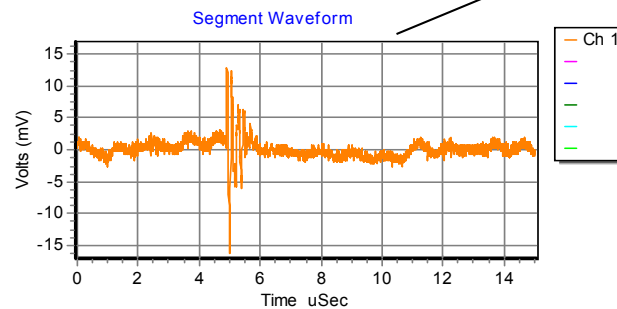


- Impulsive events **extracted and categorised by software** as cable PD, local PD and noise.
- Even amongst noise interference, **PD data can still be extracted.**

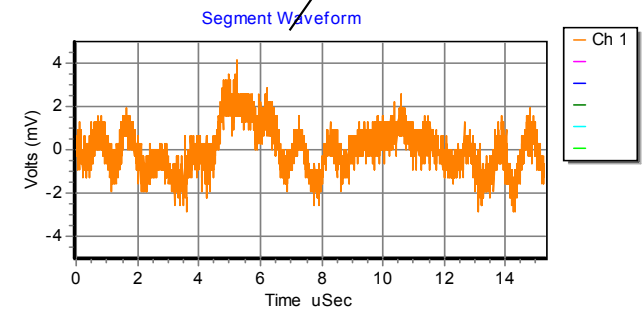
One power cycle of raw data from HFCT sensor



Cable PD Pulse: 16 mV, 1160 pC



Local PD Pulse: 15 mV, 24 dB



Noise Pulse: 6 mV

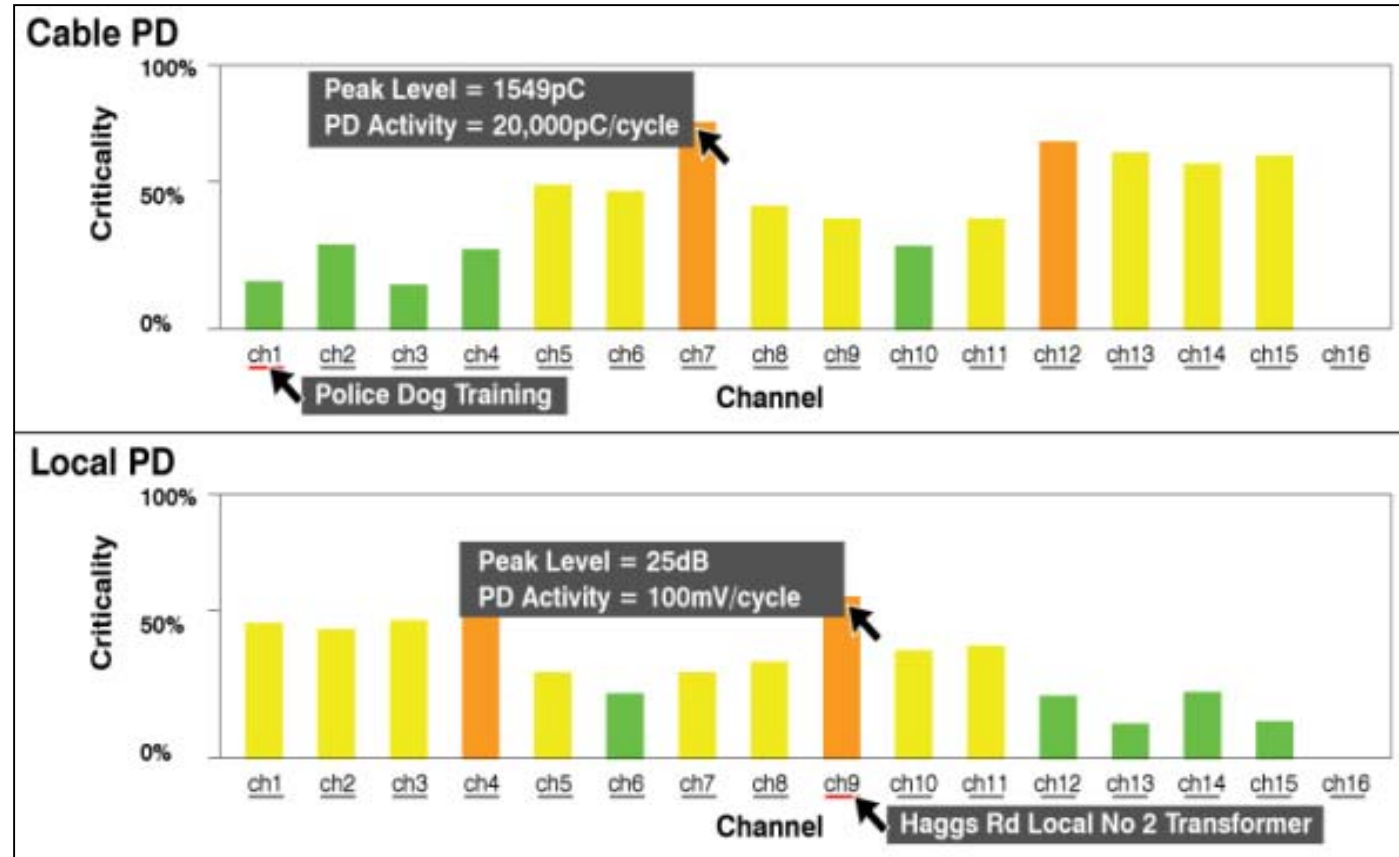


- 24/7 diagnostic portable OLPD monitoring technology for MV and HV Plant
- Measures, analyses and logs Cable PD, Local PD and Noise
- 'Knowledge-Rule' based PD criticality measurement (0–100)
- Remote access connection via LAN/Modem
- 16-Channel (HFCT/TEV/HVCC) with optional add-on 32x channel AA sensor modules



- Criticality league table
- Highlights most critical circuits
- Updated every 24 hours
- Link to data graphs
- Criticality algorithm, specific to plant

- Small PD-activity
- Moderate PD-activity
- Intensive PD-activity
- Critical PD-activity



- Criticality league table
- Highlights most critical circuits
- Updated every 24 hours
- Link to data graphs
- Criticality algorithm, specific to plant

Cable Local

Circuit	Sensor	PD Peak (pC)	PD Activity (pC/cycle)	Criticality
Police Dog Training	HFCT	2671	4523	
Haggs Rd Local No 1 Transformer	HFCT	5375	9119	
Shawhom Crescent	HFCT	2546	2647	
Pollockshaws commercial centre	HFCT	1994	4924	
Rossendale Rd South	HFCT	1977	11990	
Green Park	HFCT	2286	3873	
145 Shawhill Rd tee Shawhill Rd	HFCT	2837	5202	
Craigholme School	HFCT	2046	2120	
Haggs Rd Local No 2 Transformer	HFCT	4200	4333	
Millwood Street	HFCT	4898	4898	
Shawmoss Rd	HFCT	697.4	922.9	
Wellgreen Court	HFCT	1094	1285	
Shawbridge Street South	HFCT	740.6	858.1	
Shawbridge Street	HFCT	1338	1455	
Rossendale Rd	HFCT	491	688.1	

Last 24hrs Last Week Last Month Entire Test Monitoring Period: 2/07/09 12:00pm - 3/07/09 12:00pm

- Small PD-activity
- Moderate PD-activity
- Intensive PD-activity
- Critical PD-activity

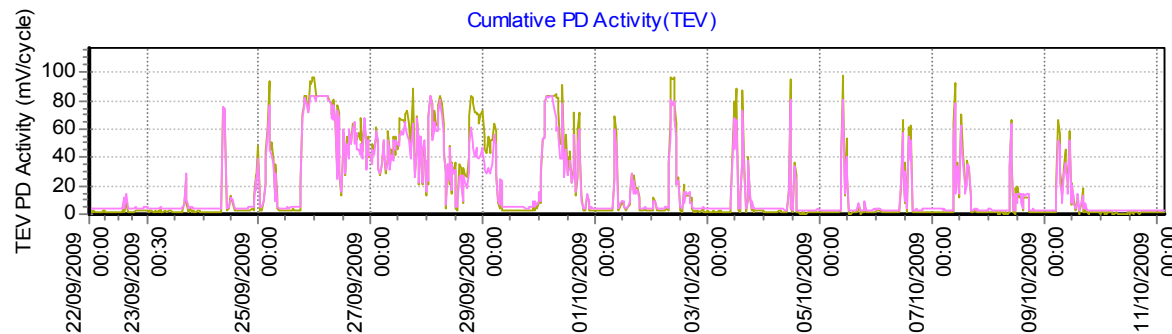
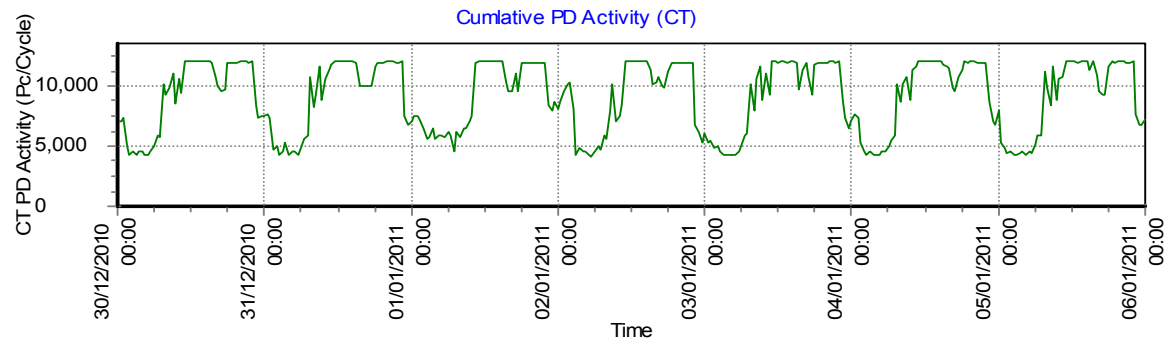


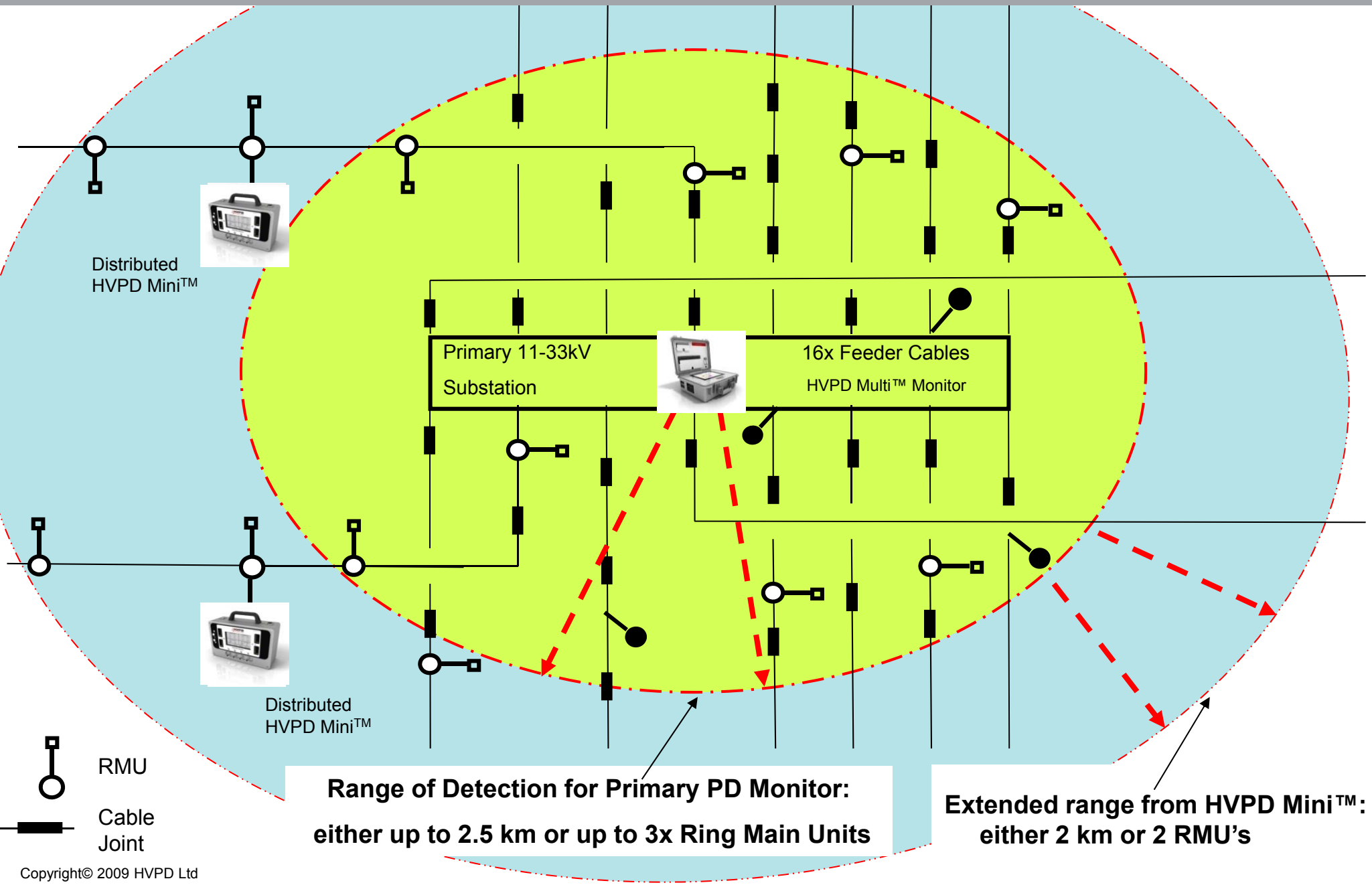
- Low-cost 24/7 PD monitoring technology for MV cables, switchgear & other plant
- Incorporates up to 4x portable PD sensors
- Measures and logs both cable PD and local PD (PD magnitude & 'count' – no. of pulses)
- Stores up to 12 months of data on local flash memory
- Uploads PD data to server every 24 hours via GSM/GPRS Modem
- Compact, lightweight and easy to set up unit for portable installations





- Provides an early warning against incipient faults to be indicated through changes in PD activity over time.
- PD activity can vary in relation to load, local temperature and humidity.
- Distributed temperature and humidity modules monitor these variations in the substation.

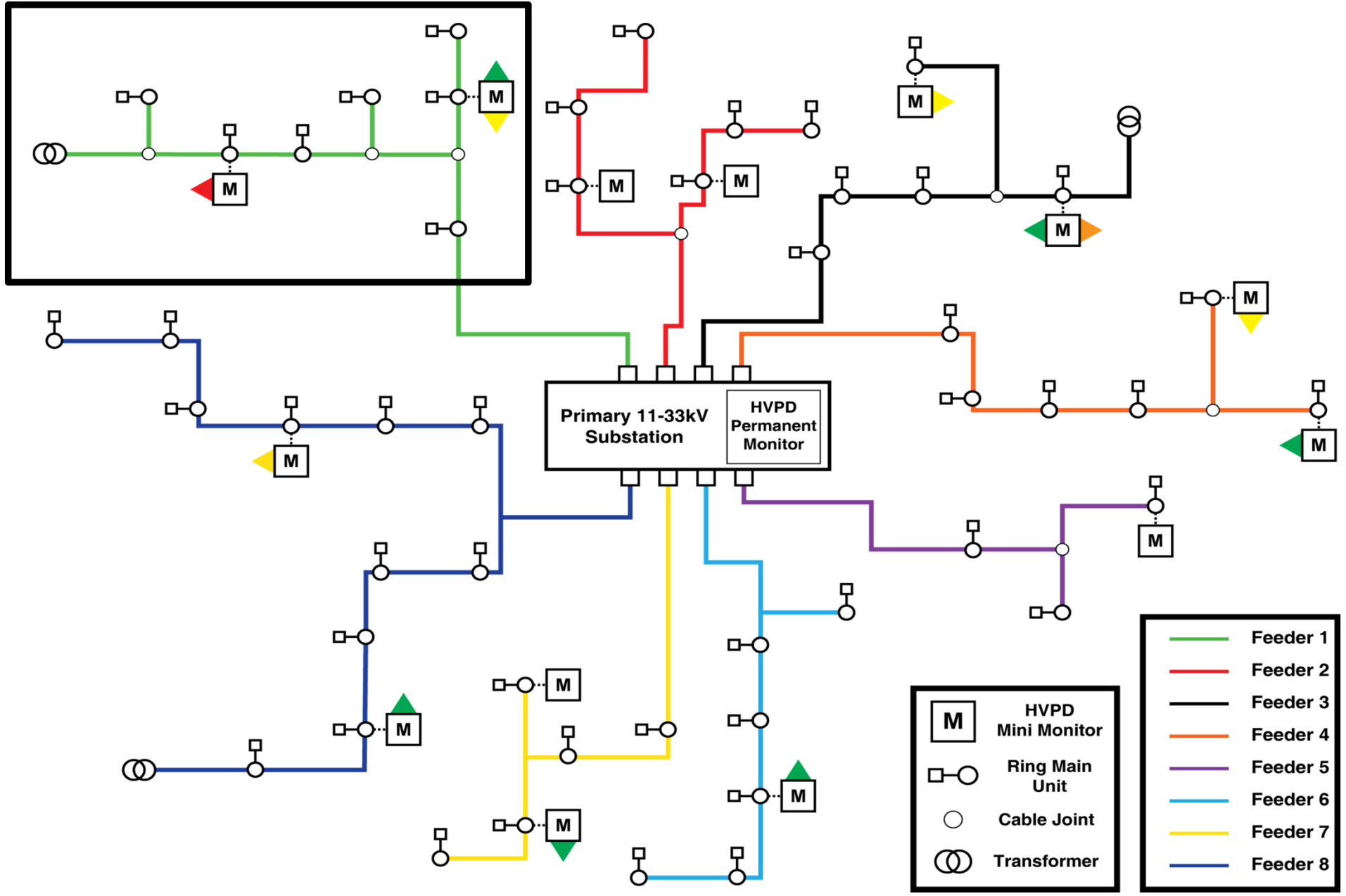


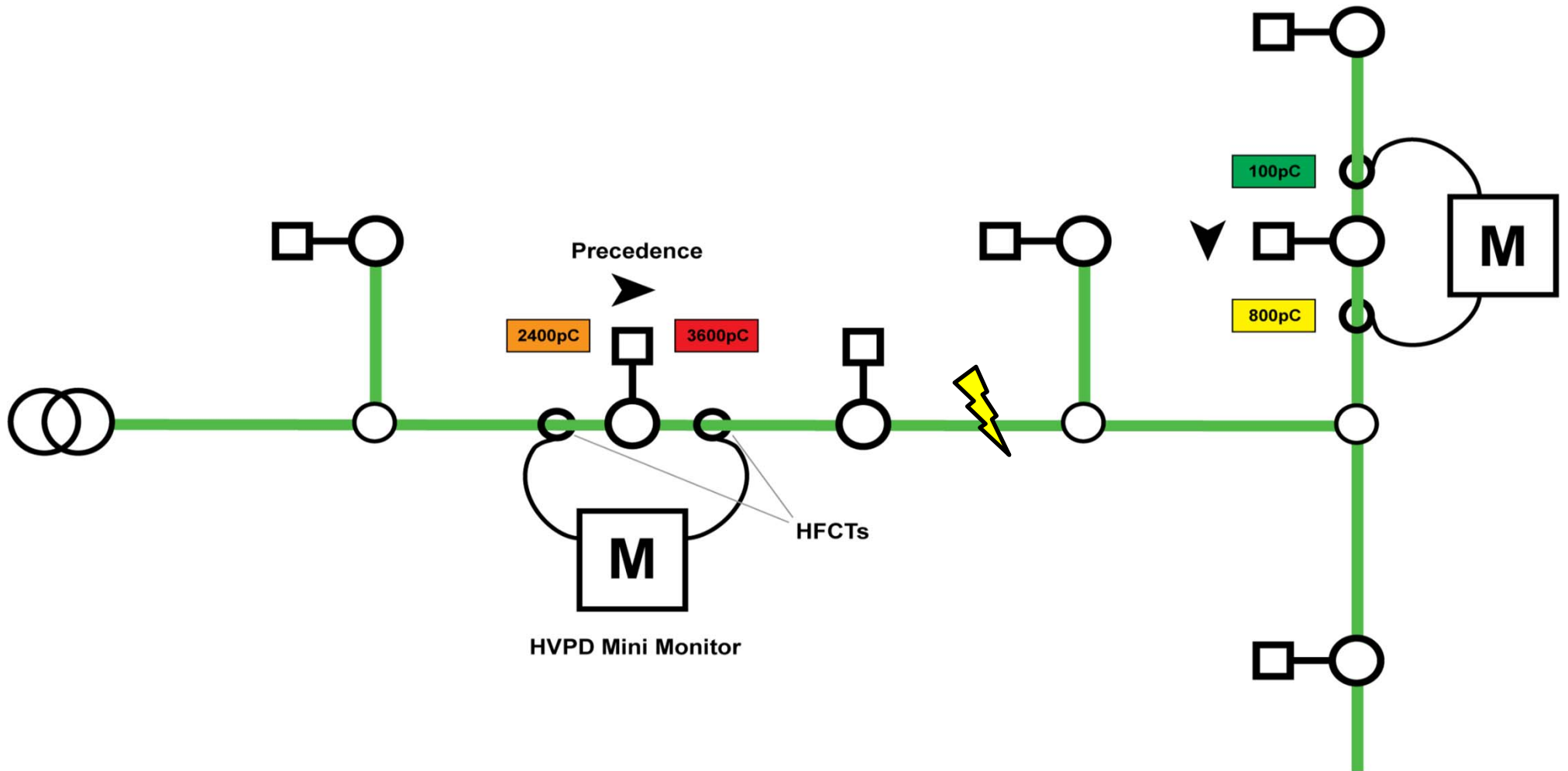




Combined OLPD Monitoring Solution

Primary Substation Monitor plus Distributed HVPD Mini™ Monitors







- 24/7 monitoring of PD in switchgear, cables and rotating HV machines
- Non-intrusive, inductive sensors
- Remotely accessible with GPRS/3G modem
- Onboard automatic analysis software provides differentiation of all PD pulses from noise
- Can monitor up to 4x rotating HV machines



- The HVPD-Multi™ Monitor does not provide automated alarms but provide '*flags*' for further engineer investigation
- These '*flags*' can signal an increase in either PD level or PD activity but can also be caused as a result of network switching
- Each '*flag*' is investigated by HVPD engineers before a diagnostic decision is made regarding preventative maintenance interventions.



**Increase within
acceptable limits**

**Some
concern -
monitor
closely**

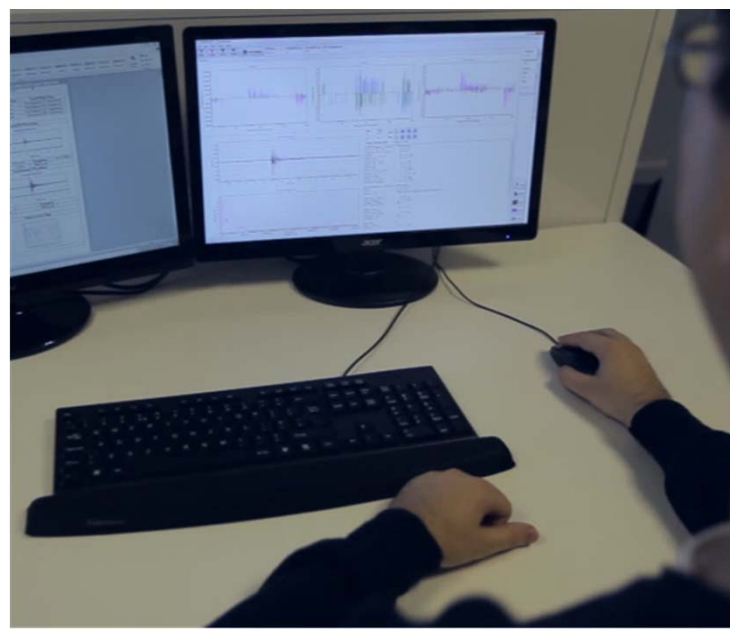
**Major
concern -
intervention**

INSTALLATION



DAY 1

DATA ANALYSIS

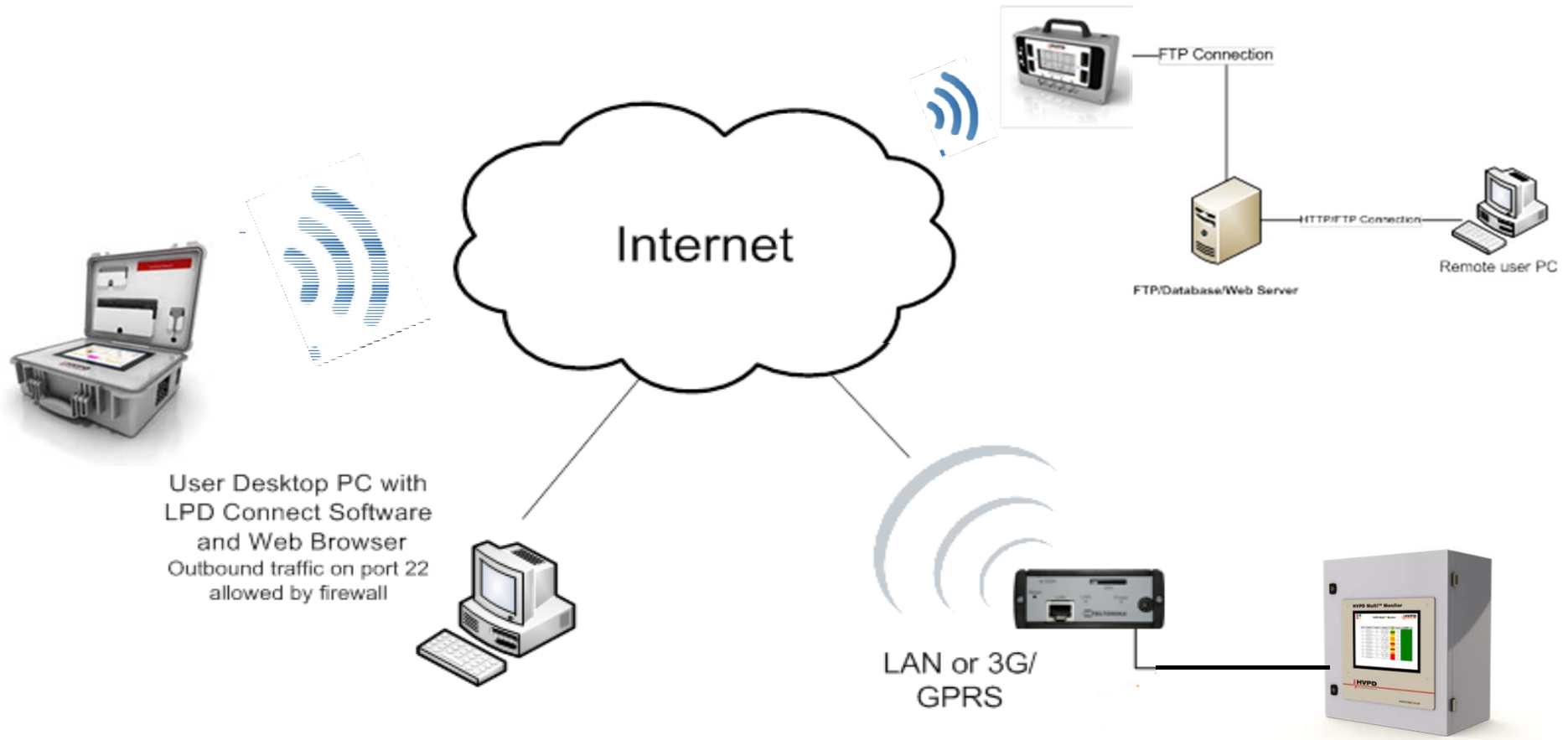


DAILY DATA ANALYSIS

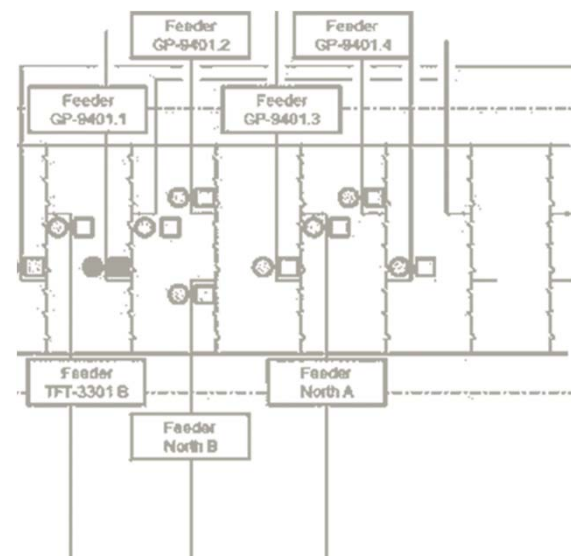
ADJUSTMENT

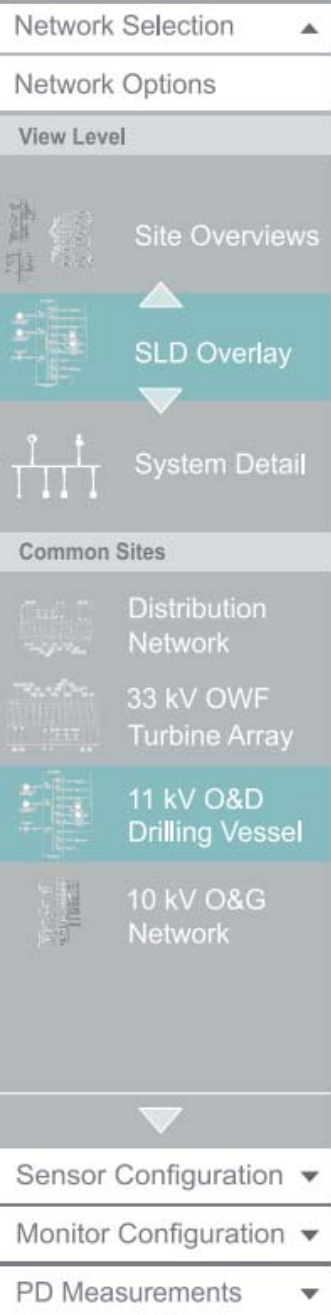


DAY 30



EXAMPLE OF HV NETWORK OLPD MONITORING SYSTEM USER INTERFACE BASED ON THE CLIENT'S HV NETWORK SINGLE-LINE DIAGRAM (SLD)





Presents data hierarchically using a 3-level interface:

- 1st level: all sites/vessels
- 2nd level: one site/vessel (entire SLD)
- 3rd level: one switchroom

Analysis / Reports

Local Area Network Criticality League Table

Site
DRILLING VESSEL 1
DRILLING VESSEL 2
DRILLING VESSEL 3
DRILLING VESSEL 4



Network Selection

View Level

- Site Overviews
- SLD Overlay
- System Detail

Sites

- Drilling Vessel 1
- Drilling Vessel 2
- Drilling Vessel 3
- Drilling Vessel 4

Sensor Configuration

Manual Configuration

PD Measurements

Analysis / Reports Substation : HV SWBD 1

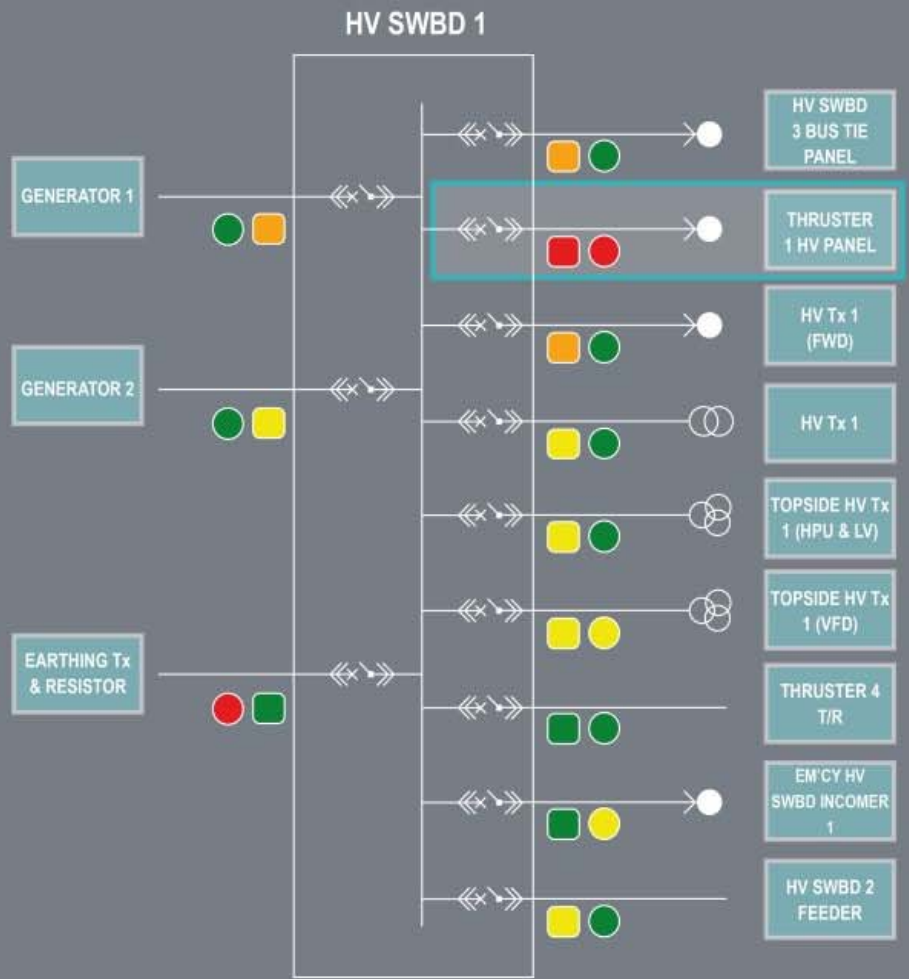
Local Area Network Criticality League Table

Locations	Criticality (0-100)	
	Cable	Local
THRUSTER 1 HV PANEL	95	99
EARTHING Tx & RESISTOR	77	100
GENERATOR 1	13	74
HV Tx 1 (FWD)	18	70
HV SWBD 3 BUS TIE PANEL	13	65
TOPSIDE HV Tx 1 (HPU & LV)	39	39
GENERATOR 2	18	38
TOPSIDE HV Tx 1 (VFD)	36	44
HV SWBD 2 FEEDER	09	26
EM'CY HV SWBD INCOMER 1	25	21
THRUSTER 4 T/R	20	12

Condition/Action Guideline	Criticality (0-100)
High PD / Diagnostic	76 - 100
Moderate to High PD / Investigate	51 - 75
Moderate PD / Monitor	26 - 50
Plant OK / No Action	0 - 25

Key
● Cable / Machine PD Activity
● Local PD Activity

Monitoring Period
 Last Hour Last 24 Hours
 Last Week Last Month



Network Options

- View Level
- GEO : Overview
 - SLD : Overview
 - Substation : HV SWBD 1
 - Location : select

Overview Substations

- Distribution Network
- 33 kV OW Turbine Array
- 11 kV O&D Drilling Vessel
- 10 kV O&G Network

- Sensor Configuration
- Manual Configuration
- PD Measurements

Analysis / Reports

Substation : HV SWBD 1

Local Area Network Criticality League Table

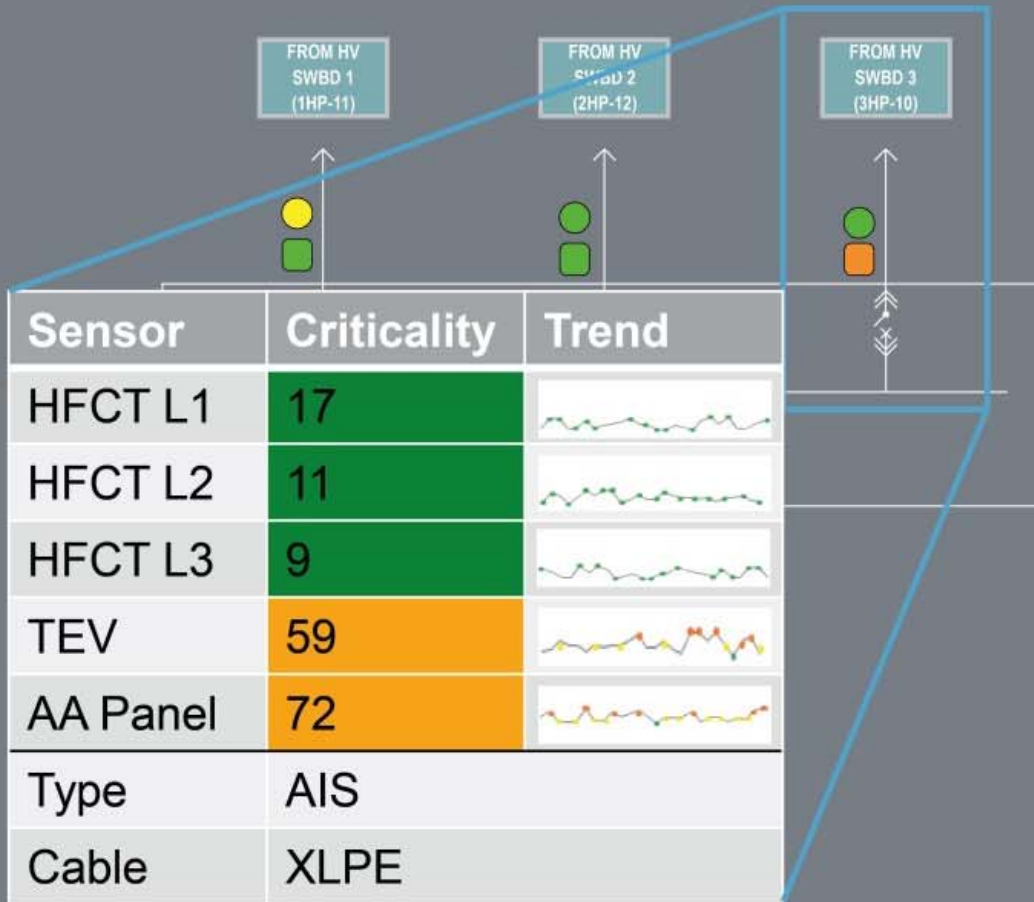
Locations	Criticality (0-100)	
	Cable	Local
FROM HV SWBD 3 (3HP-10)	17	72
FROM HV SWBD 1 (1HP-11)	43	08
EM'CY HV Tx	27	58
FROM HV SWBD 2 (2HP-12)	30	18

Condition/Action Guideline	Criticality (0-100)
High PD / Diagnostic	76 - 100
Moderate to High PD / Investigate	51 - 75
Moderate PD / Monitor	26 - 50
Plant OK / No Action	0 - 25

Key
● Cable / Machine PD Activity
■ Local PD Activity

Monitoring Period

- Last Hour
- Last 24 Hours
- Last Week
- Last Month



Network Options

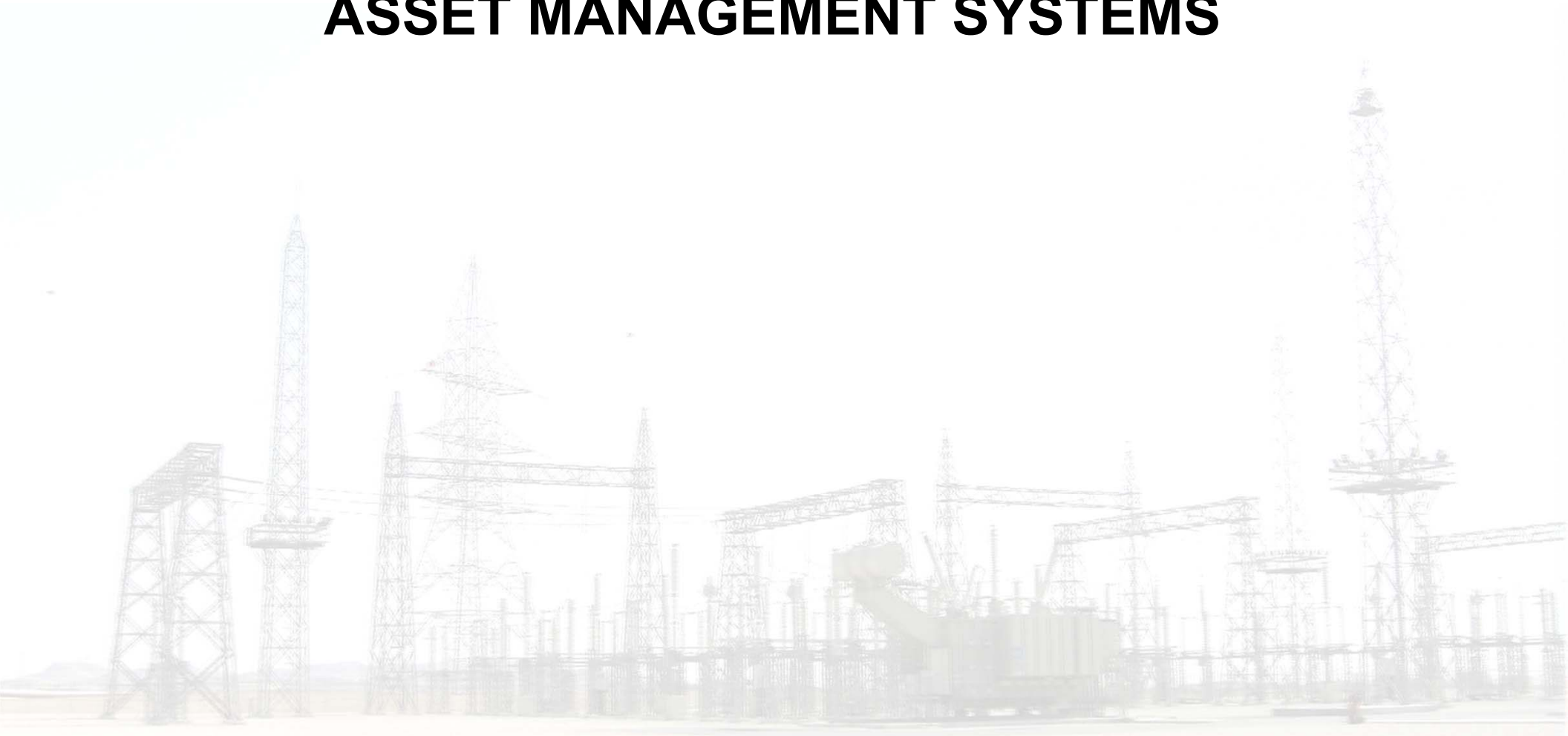
- View Level
- GEO : Overview
 - SLD : Overview
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- Overview Substations
- Distribution Network
 - 33 kV OW Turbine Array
 - 11 kV O&D Drilling Vessel
 - 10 kV O&G Network

- Sensor Configuration
- Manual Configuration
- PD Measurements



EXAMPLES OF DEPLOYMENT OF PD TESTING IN ASSET MANAGEMENT SYSTEMS





**CASE STUDY 2: OLPD TEST AND MONITORING
PROJECT ON 11 KV AND 33 KV
'WORST PERFORMING CIRCUITS'**



- 'Worst Performing Circuits List' focuses on replacing cable sections with the highest number of faults.
- Due to budget, it is only possible to replace a small percentage of circuits a year.
- Limited monitoring budgets need to be used on circuits with the highest risk of failure.

- Network A 11 kV: 6.91 faults per 100 km per annum
- Network B 11 kV: 13.66 faults per 100 km per annum
- Network A & Network B 33 kV: 11.5 faults per 100 km per annum

Summary Data of 11 kV Worst Performing Circuits in Networks A & B (2004-2008)

No. of Circuits	Total Length	Average Circuit Length	Average faults per annum (Av. 5 years 2004 to 2008)	Faults per 100 km p.a.
Network B - 86	530 km	6.160 km	72.4	13.66
Network A -122	970 km	7.950 km	67.0	6.91
Total - 208	1500 km	7.210 km	139.4	9.30

Summary Data of 33 kV Worst Performing Circuits in Networks A & B (2002-2008)

No. of Circuits	Total Length (est.)	Average Circuit Length (est.)	Average faults per annum (Av. 7 years 2002 to 2008)	Faults per 100 km p.a.
Network B- 51	357 km	7.000 km	42.1	11.80
Network A - 62	434 km	7.000 km	48.6	11.19
Total - 113	791 km	7.000 km	90.7	11.47



- The suitability of cable terminations for the attachment of the HFCT sensors is the main restriction on the widespread application of the OLPD technology.
- Only around 40% of the terminations on the customer's networks can be considered as 'suitable'.
- For future testing, it has been suggested that the customer modify solidly bonded terminations.

- OLPD tests were carried out at substations with worst historical failure rates.
- HVPD Mini™ Portable was installed at a number of substations.
- The spot testing was carried out using HVPD's OLPD test technology.



10% of all of 39x 33kV cable circuits tested are the **Red Condition Category**.

No. of Circuits	Condition	%
26	Discharge within acceptable limits	66
7	Some concern, monitoring recommended	18
2	Some concern, regular monitoring recommended	5
4	Major concern, locate PD and then repair or replace	10

4% of all 25x 11kV circuits tested in this project are in the **Red Condition Category**.

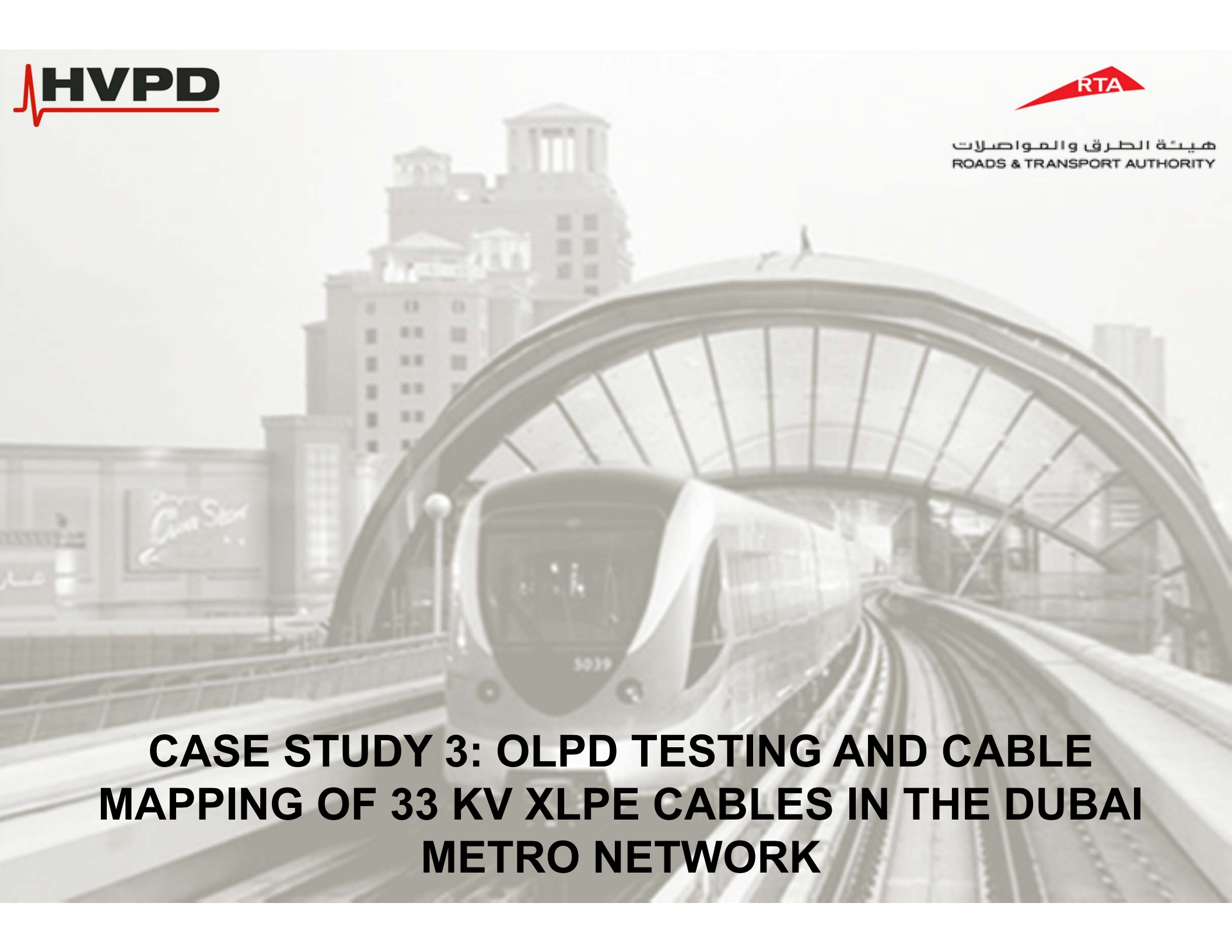
No. of Circuits	Condition	%
18	Discharge within acceptable limits	72
4	Some concern, monitoring recommended	16
2	Some concern, regular monitoring recommended	8
1	Major concern, locate PD and then repair or replace	4



Case Study: Worst Performing Circuits

Criticality Number	Circuit	Comments	Peak PD Value	Cumulative PD Level	OLPD Criticality (%)	Maintenance Action
1.	Circuit 18	Large PD on this circuit	3600pC	195 nC/Cycle	83.2	Major concern, locate PD and then repair or replace.
2.	Circuit 62	Large cable PD	4000pC Cable Box PD	62nC/Cycle 1.2V/Cycle	79.7	
3.	Circuit 28	No cable PD Local PD is 36dB	36dB	1.1 V/Cycle	78.3	
4.	Circuit 26	No cable PD Local PD 35dB	35dB	1.4 V/Cycle	76.4	
5.	Circuit 14	Some outdoor PD	25dB Local PD	24.6 V/Cycle	*Outdoor Survey*	
6.	Circuit 32	No Cable PD Local 34dB	34dB	1.0 V/Cycle	73.3	Some concern, repeat test and regular monitoring recommended.
7.	Circuit 50	Cable box PD TEV levels at 35dB	1600pC & 35dB	4.2 nC/Cycle 0.7 V/Cycle	70.1	
8.	Circuit 63	Cable PD & Cable Box, 30dB	1200pC 30dB Cable Box	<10 nC/Cycle 1.5V/Cycle	62.2	
9.	Circuit 36	No Cable PD Local 27dB	27dB	1.6 V/Cycle	57.7	
10.	Circuit 21	Large PD on this circuit	3800pC	21 nC/Cycle	56.3	Some concern, re-test within 6 months.
11.	Circuit 61	Low-Medium Level Cable PD	1600pC	52nC/cycle	55.8	
12.	Circuit 40	Medium-High Cable PD	4000pC	<10 nC/Cycle	55.5	
13.	Circuit 37	No Cable PD Local 23dB	23dB	1.1 V/Cycle	46.6	
14.	Circuit 31	No Cable PD Local 25dB	25dB	0.6 V/Cycle	45.7	
15.	Circuit 46	Medium Cable PD	2500pC	<10 nC/Cycle	38.2	
16.	Circuit 27	No cable PD Local PD 20dB	20dB	0.8 V/Cycle	37.4	
17.	Circuit 43	Medium-High Cable PD	3500pC	<10 nC/Cycle	37.1	
18.	Circuit 12	Incipient PD of 2000pC measured at Circuit 12	2000pC	<10 nC/Cycle	29.1	
19.	Circuit 11	PD on circuit, no location	1000pC	40.4 nC/Cycle	28.0	
20.	Circuit 22	Bad phase is the source	1400pC	<10 nC/Cycle	25.2	

- Continuous OLPD monitoring of the medium and high PD sites (the highest risk of failure).
- Retesting of all of the 'TOP 20' circuits within the next 3-6 months.
- Deploy monitoring units at the worst performing substations over an initial 3-month monitoring period.
- For the 44x circuits which have lower, a repeat 'spot' test within 12 months would be prudent.
- A larger survey of a minimum 100x 11 kV and 100x 33 kV feeders should be carried out to provide a more statistically valid data set.



**CASE STUDY 3: OLPD TESTING AND CABLE
MAPPING OF 33 KV XLPE CABLES IN THE DUBAI
METRO NETWORK**

- OLPD testing was carried out in response to a number recent faults* of 33 kV cable joints within the customer's network.
- The faults led to disruption of the power supply to the Metropolitan rail system.
- The purpose of the testing was to measure and locate any PD activity within the cables with particular focus on the cable joints.

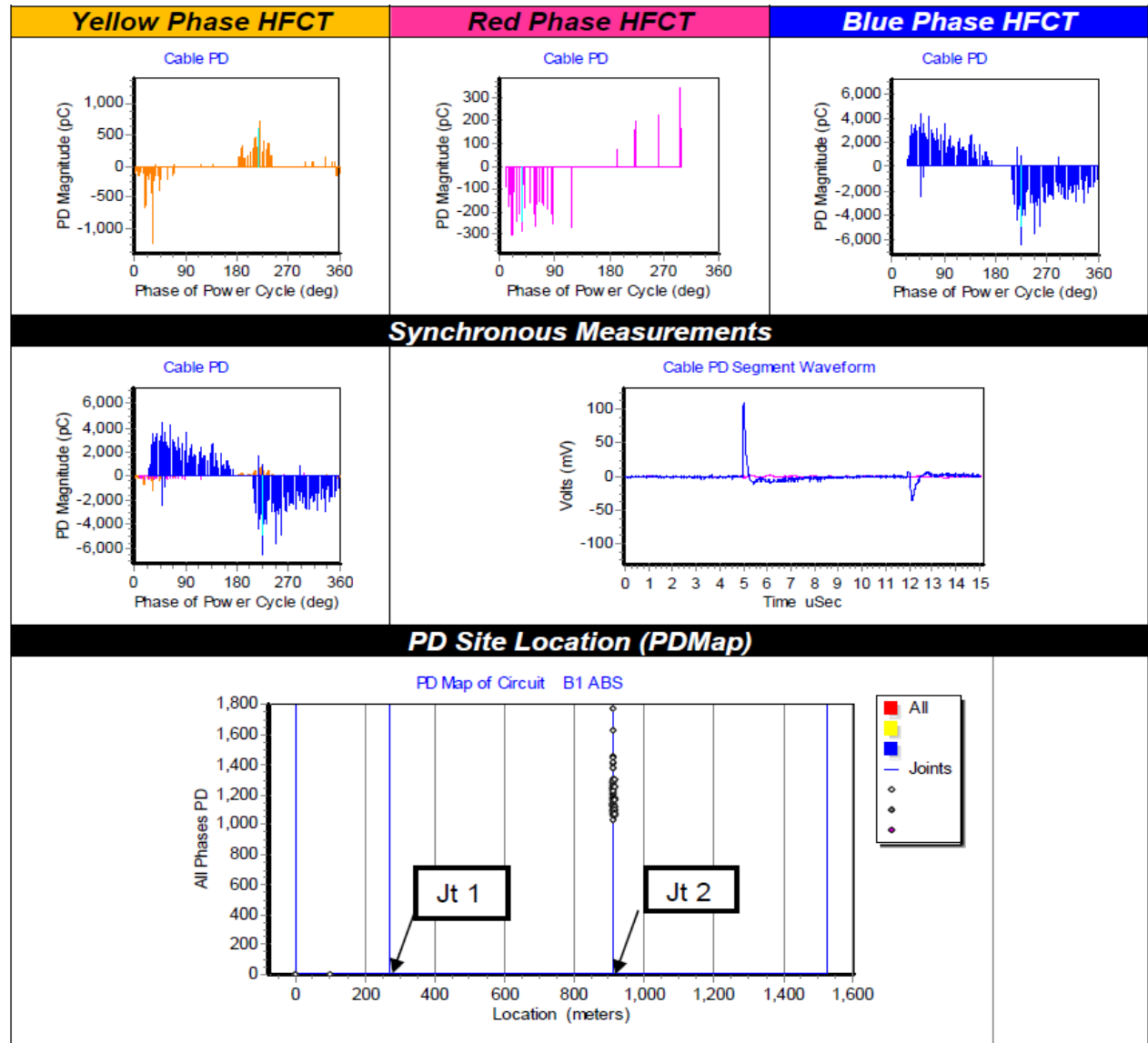


** It should be noted that this was a newly installed cable system that had been in-service for just over 12 months before the faults started to occur.*



- On-line Cable PD Mapping using the HVPD Longshot™ test unit and Portable transponder.
- Tests started with calibration testing with pulse injection HFCTs.

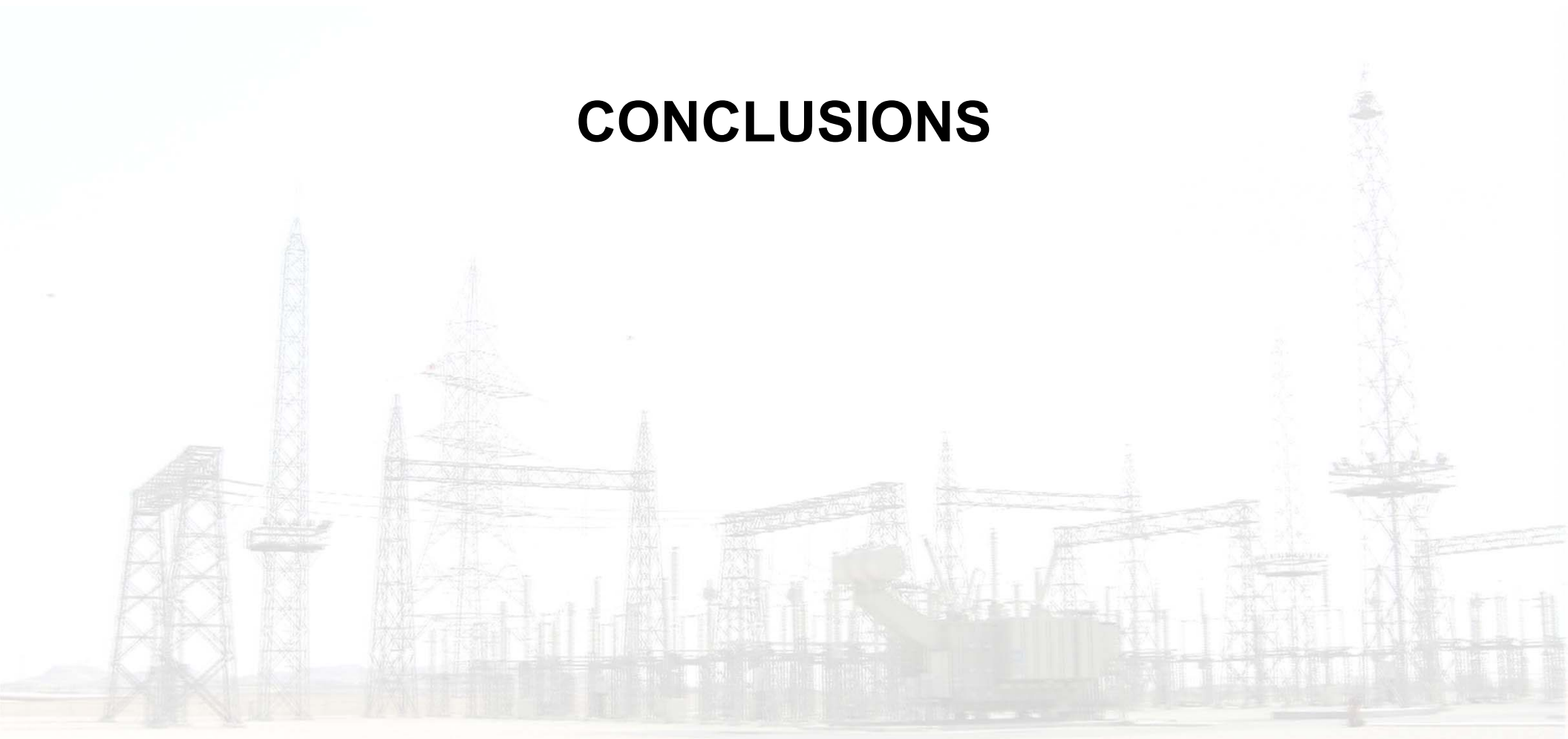
- Cable PD signals have been detected on Blue Phase with cross-talk (lower magnitude) on Red and Yellow phases.
- The source of PD was located to Joint Number 2 (Jt2) using the on-line PD mapping technique.
- The faulty joint on this cable was replaced and re-tested using the HVPD Longshot™ test unit to verify the repair was good



- Out of the 50+ circuits tested, Major PD was detected within cable accessories on the three of the circuits (6%) as shown in RED in the Table below.
- The levels of discharges detected put these 33 kV cables into RED category, “Major concern, locate PD and then repair or replace”.

Criticality Number	Circuit	Comments	Peak Cable PD Level (pC)	Local PD Level (dB)	Cumulative Cable PD Level (nC/cycle)	OLPD Criticality (%)	Maintenance Action
1.	DUB to MPS1 C2	B Phase	25888	<10	247	97.4	Major concern, locate PD and then repair or replace.
2.	ABS to AH C2	B / Y Phase	9729	<10	120	90.3	
3.	BUR to HCC C2	B / Y Phase	3781	<10	12.3	78.7	
4.	BUR to HCC C1	B / Y Phase	3245	<10	7.9	78.1	
5.	ABS to AH C1	B / Y Phase	2920	<10	14.4	77.4	
6.	NHD to QYD C2	R Phase	2849	<10	15.0	76.2	
7.	ALQ to AHS C2	B Phase	1733	<10	4.6	70.6	Some concern, repeat test and regular monitoring recommended.
8.	MPS3 to BNS C2	R / B Phase	1337	<10	6.4	65.5	
9.	NHD to QYD C1	R Phase	887	<10	8.8	47.8	
10.	HCC to CRK C1	Y / B Phase	759	<10	2.5	39.2	
11.	AHS to SLD	Y / R Phase	705	<10	3.1	38.5	
12.	STD to ABH	Y Phase	238	<10	1.0	24.1	Re-test in 12 months.
13.	ALR to BNS C1	B Phase	184	<10	0.9	18.6	
14.	ALR to BRJ	No PD detected	0	<10	0	0	
15.	ALG to PMD	No PD detected	0	<10	0	0	
16.	ALG to KBW	No PD detected	0	<10	0	0	
17.	AQD to AQ2	No PD detected	0	<10	0	0	
18.	JDD to CRK	No PD detected	0	<10	0	0	
19.	ODM to JDF C1	No PD detected	0	<10	0	0	
20.	ODM to JDF C2	No PD detected	0	<10	0	0	

CONCLUSIONS



- A combination of both on-line and off-line partial discharge testing and OLPD monitoring systems for in-service plant helps produce 'risk-of-failure' indices that support condition-based asset management decisions
- By replacing or repairing cables or plant that has high levels of OLPD activity (and therefore a higher risk of failure) the MV and HV plant owner can target their maintenance budgets to those assets in most need whilst simultaneously reducing the risk of HV insulation faults on their network
- With the advent of recent developments in wideband OLPD monitoring, such as with the HVPD Complete HV Network Monitoring Solution, the entire installed HV network, including switchgear, cables and remotely connected HV plant can be assessed under normal working conditions, without the need for an outage
- Real-time condition monitoring (CM) such as this, combined with a proactive, preventative maintenance intervention strategy can help reduce the risk of unplanned outages caused by HV insulation failure



End of Presentation

Thank you for your time

Q&A?

